

# Supporting Information

## A Novel [Os(1,10-phenanthroline-5,6-dione)<sub>2</sub>(PVP)<sub>4</sub>Cl]Cl Redox Polymer for Electrocatalytic Oxidation of NADH and its Application to the Construction of Reagentless $\beta$ -D-glucose Biosensors

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### EXPERIMENTAL SECTION

**Materials.**  $\beta$ -Dihyronicotinamide adenine dinucleotide (NADH),  $\beta$ -nicotinamide adenine dinucleotide (NAD<sup>+</sup>), were purchased from Sigma (Madrid, Spain). Glucose dehydrogenase (GDH) (EC 1.1.1.47) from *Bacillus megaterium* (220 U/mg protein) was obtained from Merck (Darmstadt, Germany). Sodium phosphate salts, sodium chloride and dimethylformamide were from Aldrich (Madrid, Spain). Ethylene glycol and  $\beta$ -D-glucose were purchased from Panreac (Madrid, Spain). Poly(ethylene glycol) diglycidyl ether (PEGDGE) and poly(4-vinyl pyridine) (PVP) were obtained from Polysciences Inc. (Warrington, PA, USA). Spectrographic graphite rods were acquired from Carbone of America Corp. Ultra Carbon Division (Bay City, MI, USA). Fine emery paper was from Buehler Ltd. (Lake Bluff, IL, USA). All other reagents were of analytical grade. Water was produced in a Mili-Q<sup>TM</sup> system (Millipore Corp., Bedford, MA, USA). [Os(1,10-phenanthroline-5,6-dione)<sub>2</sub>Cl<sub>2</sub>] was synthesized according to an earlier published modified method.<sup>28,31</sup> The <sup>1</sup>H NMR investigation performed in (CD<sub>3</sub>)<sub>2</sub>SO with a tetramethylsilane standard demonstrated following shifts  $\delta_{\text{H}}$ : 8.1 ppm (2H dd), 7.53 ppm (2H dd), and 7.15 ppm (2H dd). Poly(4-vinyl pyridine) was derivatized with bromoethylamine as reported elsewhere<sup>62</sup> to yield the “binder” polymer.

**Synthesis of Os-phendione-PVP.** 80 mg of [Os(1,10-phenanthroline-5,6-dione)<sub>2</sub>Cl<sub>2</sub>] and 50 mg of poly(4-vinylpyridine) were mixed in 3 mL ethylene glycol. The mixture was deaerated with argon during 10 min and refluxed under argon in darkness during 1 h, the temperature of the oil bath being maintained below 220°C, next the reaction mixture was cooled to room temperature and added dropwise to

100 mL of aqueous 1 M sodium chloride solution during 15 min. The resulting mixture was left to stay overnight at 4°C, the precipitate was filtered off, washed with water and air-dried. The synthesis route and the suggested structure of the resulting redox polymer is shown in Figure 1. [Anal. Calcd. For n=4: C, 61.52%; H, 1.76%; N, 10.99%. Found: C, 61.71%; H, 1.70%; N, 10.7%.

**Preparation of electrodes modified with Os-phendione-PVP.** Spectrographic graphite rods of 3 mm diameter were fixed inside heat shrunk PVC tubes. Before use they were wet polished on fine (grit 400 and 600) emery paper to produce graphite electrodes having a flat circular surface.

Modification of the surface of electrodes was carried out by spreading of 1 µL on an electrode of 1.8 mg/mL Os-phendione-PVP solution in ethylene glycol. The polymer solution was left on the electrode surface for 3 min, the surface was washed with 2-3 drops of ethylene glycol and deionised water. The surface coverage was determined at pH 5.0 from the areas under the peak of cyclic voltammograms of phendione ligands at 10 mV s<sup>-1</sup> assuming that four electrons were exchanged.

**Preparation of β-D-glucose biosensors.** A mixture containing 8.5 mg/mL “binder” polymer, 34 mg/mL NAD<sup>+</sup>, 1 mg/mL PEGDGE, and 28 U/mL glucose dehydrogenase in 0.04 M sodium phosphate buffer (pH 7.6) was composed. Next 5 µL of the resulting mixture were placed on an Os-phendione-PVP modified electrode and dried under vacuum during 12 h.

**Electrochemical measurements.** For both amperometry and cyclic voltammetry a three-electrode conventional thermostabilised cell (3 mL) equipped with a Ag/AgCl/KCl<sub>sat</sub> reference electrode, and a platinum auxiliary electrode was used, a graphite electrode, modified according to one of the above mentioned procedures, being the working electrode. The buffer, pH 6.0 (0.1 M sodium phosphate and 0.15 M sodium chloride) served as supporting electrolyte. The pH was adjusted using concentrated NaOH or H<sub>3</sub>PO<sub>4</sub>. A computer-controlled BAS CV-50W voltammetric analyser (Bioanalytical Systems Inc., West Lafayette, IN, USA) was employed in cyclic voltammetry and steady state rotating electrode measurements. The rotating disk electrode, having the same spectrographic graphite as disk material, was operated by a modulated speed rotator AMSFRX (Pine Instruments Co., Grove City, PA, USA). The response to successive additions of stock β-D-glucose was registered as the steady state current with a computer controlled three-electrode potentiostat AUTOLAB PGSTAT 10 (Eco Chemie BV, The Netherlands). The working potential was 150 mV vs. Ag/AgCl/KCl<sub>sat</sub> and the temperature of the thoroughly stirred solution was 25°C unless indicated otherwise.

**Electrochemical Conversion Experiments.** Electrodes were prepared by fixing spectrographic graphite rods having diameter of 6 mm inside a heat shrunk PVC. They were wet polished on fine (grit 400 and 600) emery paper, cleaned by sonication, air-dried and modified with 4 µL of 1.8 mg/mL Os-phendione-PVP solution according to the above mentioned procedure. Next they were immersed into 2 mL of 18 µM NADH solution in 0.1 M phosphate buffer (pH 6.0) deaerated with argon, and poised at 150 mV vs. Ag/AgCl/KCl<sub>sat</sub> with stirring in a three-electrode electrochemical cell at 25 °C. Spectrophotometrical measurements of absorbance at 340 nm (A<sub>340</sub>) were used to determine the depletion of the NADH concentration during 1 hour (A<sub>340</sub> changed from 0.1117 in the beginning to 0.0540 at the end of experiment, RSD 5%). Then, 1 mL of the resulting solution was mixed with 30 µL of a mixture

containing glucose dehydrogenase and 50 fold excess of glucose and the recovery of NADH concentration was monitored spectrophotometrically until reaching the end point ( $A_{340}$  equal to 0.0867). These values were corrected for the  $\Delta A_{340}$  (from 0.1117 to 0.0902, RSD 6%) of a controlled solution of NADH during 1 hour which was not subjected to electrolysis in order to quantify the spontaneous decomposition of NADH. The area under the chronoamperometric plots was assessed to find the charge passed through the circuit during the electrocatalytic NADH oxidation which was equal to  $(2.3 \pm 0.3)$  mC.

## STEADY-STATE KINETIC MODEL OF BIOSENSORS

Figure 8S illustrates the kinetic scheme for the operation of reagentless biosensors based on a dehydrogenase enzyme (E) catalyzing the reaction of  $\text{NAD}^+$  (A) with a substrate (B) to give NADH (P) and a product (Q). Then a mediator (M), which has reduced ( $M_{\text{red}}$ ) and oxidized ( $M_{\text{ox}}$ ) forms, immobilized on the electrode surface, catalyzes the electrochemical conversion of P back to A.  $A_{\text{im}}$  and  $P_{\text{im}}$  are the concentrations of immobilized A and P.  $B_0$  and  $Q_0$  are the concentrations of the substrate and the product inside of the hydrogel.  $B_\infty$  and  $Q_\infty$  are the concentrations of the substrate and the product in the external medium.  $k'_B$  and  $k'_Q$  are mass transfer constants of the substrate and the product ( $\text{cm s}^{-1}$ ), respectively.  $L$  is the thickness of the hydrogel layer. The following expressions for the flux of P to the electrode surface ( $j_{\text{el}}$ ), which determines the current density of a biosensor ( $j$ ) through the expression  $j = nFj_{\text{el}}$ , where  $n$  is the number of exchanged electrons and  $F$  is the Faraday's constant, can be obtained:

$$j_{\text{el}} = k'_B(B_\infty - B_0) \quad (1S)$$

$$j_{\text{el}} = L(k_3 A_{\text{im}} [E] - k_{-3} [E \cdot A]) \quad (2S)$$

$$j_{\text{el}} = L(k_4 B_0 [E \cdot A] - k_{-4} [E \cdot A \cdot B]) \quad (3S)$$

$$j_{\text{el}} = L(k_5 [E \cdot A \cdot B] - k_{-5} [E \cdot P \cdot Q]) \quad (4S)$$

$$j_{\text{el}} = L(k_6 [E \cdot P \cdot Q] - k_{-6} [E \cdot P] Q_0) \quad (5S)$$

$$j_{\text{el}} = L(k_7 [E \cdot P] - k_{-7} [E] P_{\text{im}}) \quad (6S)$$

$$j_{\text{el}} = k'_Q Q_0 \quad (7S)$$

$$j_{\text{el}} = k_1 P_{\text{im}} \Gamma_{\text{Mox}} - k_{-1} \Gamma_{\text{M} \cdot \text{P}} \quad (8S)$$

$$j_{\text{el}} = k_2 \Gamma_{\text{M} \cdot \text{P}} \quad (9S)$$

$$j_{\text{el}} = k_3 \Gamma_{\text{Mred}} \quad (10S)$$

$$E_t = [E] + [E \cdot A] + [E \cdot A \cdot B] + [E \cdot P \cdot Q] + [E \cdot P] \quad (11S)$$

$$\Gamma = \Gamma_{\text{M} \cdot \text{P}} + \Gamma_{\text{Mox}} + \Gamma_{\text{Mred}} \quad (12S)$$

$$A_t = A_{\text{im}} + P_{\text{im}} \quad (13S)$$

Where  $\Gamma_{\text{Mox}}$  and  $\Gamma_{\text{Mred}}$  are surface coverages of the mediator in oxidized and reduced forms, respectively.  $\Gamma$  is the total mediator surface coverage.  $\Gamma_{\text{M} \cdot \text{P}}$  is the surface coverage of the intermediate complex between the mediator and NADH.  $A_t$  and  $E_t$  are the total concentrations of the cofactor and the enzyme immobilized in the hydrogel, respectively.  $A_{\text{im}}$  and  $P_{\text{im}}$  are the concentrations of  $\text{NAD}^+$  and NADH in the hydrogel respectively. The equations(2S-6S, 11S) yield the equation (14S) describing the enzyme kinetics.

$$j_{el} = \frac{E_t L(k_3 k_4 k_5 k_6 k_7 A_{im} B_o - k_{-3} k_{-4} k_{-5} k_{-6} k_{-7} P_{im} Q_o)}{K_6 k_7 k_{-3} k_{-4} + k_{-3} k_5 k_6 k_7 + k_7 k_{-3} k_{-4} k_{-5} + (k_3 k_6 k_7 k_{-4} + k_3 k_5 k_6 k_7 + k_3 k_7 k_{-4} k_{-5}) A_{im} + k_4 k_5 k_6 k_7 B_o + (k_3 k_4 k_6 k_7 + k_3 k_4 k_7 k_{-5} + k_3 k_4 k_5 k_7 + k_3 k_4 k_5 k_6) A_{im} B_o + (k_6 k_{-3} k_{-4} k_{-7} + k_5 k_6 k_{-3} k_{-7} + k_{-3} k_{-4} k_{-5} k_{-7}) P_{im} + k_{-3} k_{-4} k_{-5} k_{-6} Q_o + (k_{-4} k_{-5} k_{-6} k_{-7} + k_{-3} k_{-5} k_{-6} k_{-7} + k_{-3} k_{-4} k_{-6} k_{-7} + k_5 k_{-3} k_{-6} k_{-7}) P_{im} Q_o + k_3 k_{-4} k_{-5} k_{-6} A_{im} Q_o + (k_4 k_{-5} k_{-6} k_{-7} + k_4 k_5 k_{-6} k_{-7}) B_o P_{im} Q_o + (k_3 k_4 k_{-5} k_{-6} + k_3 k_4 k_5 k_{-6}) A_{im} B_o Q_o + k_4 k_5 k_6 k_{-7} B_o P_{im}} \quad (14S)$$

When numerator and denominator of this rate equation are multiplied by the factor  $(k_{-3} k_{-4} k_{-5} k_{-6} k_{-7}) / ((k_3 k_4 k_6 k_7 + k_3 k_4 k_7 k_{-5} + k_3 k_4 k_5 k_7 + k_3 k_4 k_5 k_6)(k_{-4} k_{-5} k_{-6} k_{-7} + k_{-3} k_{-5} k_{-6} k_{-7} + k_{-3} k_{-4} k_{-6} k_{-7} + k_5 k_{-3} k_{-6} k_{-7}))$  the following equation can be obtained:

$$j_{el} = \frac{L(V_1 V_2 A_{im} B_o - (V_1 V_2 P_{im} Q_o) / K_{eq})}{K_{AB} V_2 + K_B V_2 A_{im} + K_A V_2 B_o + V_2 A_{im} B_o + K_Q V_1 P_{im} / K_{eq} + K_P V_1 Q_o / K_{eq} + V_1 P_{im} Q_o / K_{eq} + K_P V_1 A_{im} Q_o / (K_{iA} K_{eq}) + K_A V_2 B_o P_{im} Q_o / (K_{iP} K_{iQ}) + K_P V_1 A_{im} B_o Q_o / (K_{iA} K_{iB} K_{eq}) + K_A V_2 B_o P_{im} / K_{iP}} \quad (15S)$$

Where  $V_1 = E_t(k_4 k_5 k_6 k_7) / (k_4 k_6 k_7 + k_4 k_7 k_{-5} + k_4 k_5 k_7 + k_4 k_5 k_6)$  and  $V_2 = E_t(k_{-3} k_{-4} k_{-5} k_{-6}) / (k_{-4} k_{-5} k_{-6} + k_{-3} k_{-5} k_{-6} + k_{-3} k_{-4} k_{-6} + k_5 k_{-3} k_{-6})$  are the maximum velocities in forward and reverse directions, the equilibrium constant  $K_{eq} = (k_3 k_4 k_5 k_6 k_7) / (k_{-3} k_{-4} k_{-5} k_{-6} k_{-7})$ , Michaelis constants for A, B, P, Q are  $K_A = (k_5 k_6 k_7) / (k_3 k_6 k_7 + k_3 k_7 k_{-5} + k_3 k_5 k_7 + k_3 k_5 k_6)$ ,  $K_B = (k_6 k_7 k_{-4} + k_5 k_6 k_7 + k_7 k_{-4} k_{-5}) / (k_4 k_6 k_7 + k_4 k_7 k_{-5} + k_4 k_5 k_7 + k_4 k_5 k_6)$ ,  $K_P = (k_{-3} k_{-4} k_{-5}) / (k_{-4} k_{-5} k_{-7} + k_{-3} k_{-5} k_{-7} + k_{-3} k_{-4} k_{-7} + k_5 k_{-3} k_{-7})$ ,  $K_Q = (k_6 k_{-3} k_{-4} + k_5 k_6 k_{-3} + k_{-3} k_{-4} k_{-5}) / (k_{-4} k_{-5} k_{-6} + k_{-3} k_{-5} k_{-6} + k_{-3} k_{-4} k_{-6} + k_5 k_{-3} k_{-6})$ , the inhibition constants for A, B, P, Q are  $K_{iA} = k_{-3} / k_3$ ,  $K_{iB} = (k_{-4} k_{-5} k_{-6} + k_{-3} k_{-5} k_{-6} + k_{-3} k_{-4} k_{-6} + k_5 k_{-3} k_{-6}) / (k_4 k_{-5} k_{-6} + k_4 k_5 k_{-6})$ ,  $K_{iP} = k_7 / k_{-7}$ ,  $K_{iQ} = (k_5 k_6) / (k_{-5} k_{-6} + k_5 k_{-6})$  and  $K_{AB} = (k_6 k_7 k_{-3} k_{-4} + k_{-3} k_5 k_6 k_7 + k_7 k_{-3} k_{-4} k_{-5}) / (k_3 k_4 k_6 k_7 + k_3 k_4 k_7 k_{-5} + k_3 k_4 k_5 k_7 + k_3 k_4 k_5 k_6) = K_B K_{iA}$ ,  $K_{PQ} = (k_6 k_7 k_{-3} k_{-4} + k_{-3} k_5 k_6 k_7 + k_7 k_{-3} k_{-4} k_{-5}) / (k_{-4} k_{-5} k_{-6} k_{-7} + k_{-3} k_{-5} k_{-6} k_{-7} + k_{-3} k_{-4} k_{-6} k_{-7} + k_5 k_{-3} k_{-6} k_{-7}) = K_Q K_{iP}$

Dividing numerator and denominator of (15S) by  $V_2$  and taking into account that  $V_1 / (V_2 K_{eq}) = (K_B K_{iA}) / (K_Q K_{iP})$  one can derive the equation (16S):

$$j_{el} = \frac{L(V_1 A_{im} B_o - (V_1 P_{im} Q_o) / K_{eq})}{K_{AB} + K_B A_{im} + K_A B_o + A_{im} B_o + K_B K_{iA} P_{im} / K_{iP} + K_P K_B K_{iA} Q_o / (K_Q K_{iP}) + K_B K_{iA} P_{im} Q_o / (K_Q K_{iP}) + K_P K_B K_{iA} A_{im} Q_o / (K_Q K_{iA} K_{iP}) + K_A B_o P_{im} Q_o / (K_{iP} K_{iQ}) + K_B K_P A_{im} B_o Q_o / (K_Q K_{iB} K_{iP}) + K_A B_o P_{im} / K_{iP}} \quad (16S)$$

The equations (8S-10S, 12S) give the equation (17S) which governs the kinetics of NADH oxidation at the electrode surface modified with the mediator

$$j_{el} = \frac{\Gamma k_1 k_2 k_S P_{im}}{k_2 k_S + k_{-1} k_S + (k_1 k_2 + k_1 k_S) P_{im}} = \frac{\Gamma P_{im} k_1 k_2 k_S / (k_1 k_2 + k_1 k_S)}{(k_2 k_S + k_{-1} k_S) / (k_1 k_2 + k_1 k_S) + P_{im}} = \frac{k_{cat} \Gamma P_{im}}{K_M + P_{im}} \quad (17S)$$

where the Michaelis constant for the mediator M is  $K_M = (k_2 k_S + k_{-1} k_S) / (k_1 k_2 + k_1 k_S)$  and  $k_{cat} = k_2 k_S / (k_2 + k_S)$ . Using the equations (13S) and (17S) the concentrations of  $NAD^+$  and  $NADH$  ( $A_{im}$  and  $P_{im}$ ) as well as  $B_o$  and  $Q_o$  from (1S) and (7S) can be found:  $P_{im} = j_{el} K_M / (k_{cat} \Gamma - j_{el})$ ,  $A_{im} = A_t - P_{im} = A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})$ ,  $B_o = B_\infty - j_{el} / k'_B$ ,  $Q_o = j_{el} / k'_Q$ . Substitution of  $A_{im}$ ,  $B_o$ ,  $P_{im}$ ,  $Q_o$  in equation (16S) by their expressions gives following equation:

$$j_{el} = \frac{L(V_1(A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) (B_\infty - j_{el} / k'_B) - (V_1(j_{el} K_M / (k_{cat} \Gamma - j_{el})) (j_{el} / k'_Q)) / K_{eq})}{K_{AB} + K_B(A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) + K_A(B_\infty - j_{el} / k'_B) + (A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) (B_\infty - j_{el} / k'_B) + K_B K_{iA} (j_{el} K_M / (k_{cat} \Gamma - j_{el})) / K_{iP} + K_P K_B K_{iA} (j_{el} / k'_Q) / (K_Q K_{iP}) + K_B K_{iA} (j_{el} K_M / (k_{cat} \Gamma - j_{el})) (j_{el} / k'_Q) / (K_Q K_{iP}) + K_P K_B K_{iA} (A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) (j_{el} / k'_Q) / (K_Q K_{iA} K_{iP}) + K_A (B_\infty - j_{el} / k'_B) (j_{el} K_M / (k_{cat} \Gamma - j_{el})) (j_{el} / k'_Q) / (K_{iP} K_{iQ}) + K_B K_P (A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) (B_\infty - j_{el} / k'_B) (j_{el} / k'_Q) / (K_Q K_{iB} K_{iP}) + K_A (B_\infty - j_{el} / k'_B) (j_{el} K_M / (k_{cat} \Gamma - j_{el})) / K_{iP}} \quad (18S)$$

The latter is transformed into the equation of the fourth order:

$$LV_1 \Gamma k_{cat} A_t B_\infty = j_{el} [K_{AB} \Gamma k_{cat} + K_A \Gamma k_{cat} B_\infty + \Gamma k_{cat} A_t B_\infty + K_B \Gamma k_{cat} A_t + LV_1 ((A_t + K_M) k'_B B_\infty + \Gamma k_{cat} A_t) / k'_B] + j_{el}^2 [V_1 L K_M / (K_{eq} k'_Q) + K_B K_{iA} K_M / K_{iP} + K_P K_B K_{iA} \Gamma k_{cat} / (K_Q K_{iP} k'_Q) + K_P K_B K_{iA} \Gamma k_{cat} A_t / (K_Q K_{iA} K_{iP} k'_Q) + \Gamma k_{cat} A_t B_\infty k'_B K_B K_P / (K_Q K_{iB} K_{iP} k'_B k'_Q) + K_M K_A B_\infty / K_{iP} - LV_1 (A_t + K_M) / k'_B - K_{AB} - K_B (A_t + K_M) - (k'_B B_\infty + \Gamma k_{cat}) K_A / k'_B - (A_t + K_M) B_\infty - \Gamma k_{cat} A_t / k'_B] + j_{el}^3 [K_A / k'_B + (A_t + K_M) / k'_B + K_M K_B K_{iA} / (K_Q K_{iP} k'_Q) + K_M K_A B_\infty / (K_{iP} K_{iQ} k'_Q) - K_P K_B K_{iA} / (K_Q K_{iP} k'_Q) - (A_t + K_M) K_P K_B K_{iA} / (K_Q K_{iA} K_{iP} k'_Q) - K_M K_A / (K_{iP} k'_B) - (\Gamma k_{cat} A_t) K_B K_P / (K_Q K_{iB} K_{iP} k'_B k'_Q) - (A_t + K_M) B_\infty K_B K_P / (K_Q K_{iB} K_{iP} k'_Q)] + j_{el}^4 [(A_t + K_M) K_B K_P / (K_Q K_{iB} K_{iP} k'_B k'_Q) - K_M K_A / (K_{iP} K_{iQ} k'_B k'_Q)] \quad (19S)$$

In some enzymatic reactions, including the reaction catalyzed by GDH, the equilibrium is greatly shifted towards the formation of the reaction products and their concentrations  $P_o$  and  $Q_o$  exert negligible influence on the reaction rate. In this case the equation (16S) can be rewritten as follows:

$$j_{el} = \frac{LV_1 A_{im} B}{K_{AB} + K_B A_{im} + K_A B_o + A_{im} B_o} = \frac{LV_1 (A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) (B_\infty - j_{el} / k'_B)}{K_{AB} + K_B (A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) + K_A (B_\infty - j_{el} / k'_B) + (A_t - j_{el} K_M / (k_{cat} \Gamma - j_{el})) (B_\infty - j_{el} / k'_B)} \quad (20S)$$

or

$$LV_1 \Gamma k_{cat} k'_B A_t B_\infty = j_{el} [K_{AB} k'_B \Gamma k_{cat} + K_B k'_B \Gamma k_{cat} A_t + K_A k'_B \Gamma k_{cat} B_\infty + \Gamma k_{cat} k'_B A_t B_\infty + LV_1 \Gamma k_{cat} A_t + LV_1 k'_B (A_t + K_M) B_\infty] - j_{el}^2 [K_{AB} k'_B + K_B k'_B (A_t + K_M) + K_A k'_B B_\infty + K_A \Gamma k_{cat} + \Gamma k_{cat} A_t + k'_B (A_t + K_M) B_\infty + LV_1 (A_t + K_M)] + j_{el}^3 [K_A + A_t + K_M] \quad (21S)$$

If the concentration of the immobilized cofactor  $A_t$  is so high that it is not a limiting factor of the enzymatic reaction the equation 21S can be simplified to give:

$$LV_1\Gamma k_{\text{cat}}k'_B B_\infty = j_{\text{el}}[K_B k'_B \Gamma k_{\text{cat}} + \Gamma k_{\text{cat}}k'_B B_\infty + LV_1\Gamma k_{\text{cat}} + LV_1k'_B B_\infty] - j_{\text{el}}^2[K_B k'_B + \Gamma k_{\text{cat}} + k'_B B_\infty + LV_1] + j_{\text{el}}^3 \quad (22S)$$

When the concentration of the substrate  $B_\infty$  is infinitely high the latter equation can be rewritten as:

$$LV_1\Gamma k_{\text{cat}}k'_B = j_{\text{el max}}[\Gamma k_{\text{cat}}k'_B + LV_1k'_B] - j_{\text{el max}}^2 k'_B \quad (23S)$$

$$j_{\text{el max}}^2 - j_{\text{el max}}[\Gamma k_{\text{cat}} + LV_1] + LV_1\Gamma k_{\text{cat}} = 0 \quad (24S)$$

$$\text{The roots of this square equation are } j_{\text{el max 1}} = \Gamma k_{\text{cat}} \quad (25S)$$

and

$$j_{\text{el max 2}} = LV_1 \quad (26S)$$

It follows from the equation (24S) that the maximum flux in reagentless biosensors in the presence of saturating concentration of  $\text{NAD}^+$  is equal to  $LV_1$  (the maximum response is limited by the enzymatic reaction) or  $\Gamma k_{\text{cat}}$  (the maximum response is limited by the reaction of the mediated oxidation of NADH at the electrode surface). The value of the maximum flux of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ) was found from calibration curves of the graphite electrodes modified with Os-phendione-PVP according to the Eadie-Hofstee plots. Calibration of these electrodes with NADH was performed to demonstrate the maximum current density of  $492 \mu\text{A cm}^{-2}$  which corresponds to  $\Gamma k_{\text{cat}}$  equal to  $2.55 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ .

Cubic equation (21S), having exact analytical solution, was used to simulate the response of reagentless glucose biosensors. The typical calibration curves and the Eadie-Hofstee plots for glucose biosensors computed at varied loading of  $\text{NAD}^+$  ( $A_t$ ), the infinitely rapid mass transport of glucose ( $k'_B \rightarrow \infty$ ), and the maximum flux of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ) less than the maximum flux of the electrochemical oxidation of NADH ( $\Gamma k_{\text{cat}}$ ) are represented in the Figure 9S. The straight lines of the Eadie-Hofstee plots indicate that under these conditions the response of the biosensors is determined only by the rate of the enzymatic reduction of  $\text{NAD}^+$ . The slope of the Eadie-Hofstee plots which is equal to  $-1/K_{B \text{ app}}$ , where  $K_{B \text{ app}}$  is the apparent Michaelis constant for the substrate B, depends on the loading of  $\text{NAD}^+$ . The intercept of the Eadie-Hofstee plots with the axis of  $j$  which is the apparent maximum current density ( $j_{\text{max app}}$ ) is determined by  $A_t$  too. So, an increase in the loading of  $\text{NAD}^+$  results in a rise in the apparent Michaelis constant and the maximum current density. Only when the  $\text{NAD}^+$  loading reaches a saturating level ( $A_t \rightarrow \infty$ ) the values of the apparent maximum current density ( $j_{\text{max app}}$ ) and the apparent Michaelis constant ( $K_{B \text{ app}}$ ) coincide with those of the product  $LV_1 nF$  and the Michaelis constant ( $K_B$ ) respectively.

The Figure 10S demonstrates the effect of the mass transfer constant of the substrate ( $k'_B$ ) on the calibration curves and the Eadie-Hofstee plots simulated with the saturating loading of  $\text{NAD}^+$  ( $A_t \rightarrow \infty$ ) and the maximum flux of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ) less than the maximum flux of the electrochemical oxidation of NADH ( $\Gamma k_{\text{cat}}$ ). In this case the smaller is the mass transfer constant of the

substrate the greater is the deviation from the straight line in the Eadie-Hofstee plots which is characteristic of the process governed by the enzymatic reaction of the  $\text{NAD}^+$  reduction. The values of the apparent current densities and apparent Michaelis constants obtained by the Eadie-Hofstee plots coincide with the values of  $LV_1nF$  and  $K_B$ , respectively, only if very high concentrations of the substrate ( $B_\infty$ ) are used to build the plots

The Figures 11S-18S show the influence of the maximum flux of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ), maximum flux of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ), and the  $\text{NAD}^+$  loading on calibration curves and the Eadie-Hofstee plots simulated with the infinitively rapid mass transport of glucose ( $k'_B \rightarrow \infty$ ). Clearly, the maximum current density is determined by the maximum flux of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ) when the latter is less than the maximum flux of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ). The maximum flux of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ) limits the maximum current density if  $\Gamma k_{\text{cat}}$  is less than the flux of the enzymatic reduction of  $\text{NAD}^+$  at given  $\text{NAD}^+$  loading ( $A_t$ ). The sharp breaks followed by the horizontal lines in the Figures 11S, 12S, 15S, 16S are due to  $\text{NAD}^+$  depletion caused by rapid enzymatic reaction at the saturating  $\text{NAD}^+$  loading in the steady state model. The decrease in the  $\text{NAD}^+$  loading results in the decrease in the flux of the enzymatic reduction of  $\text{NAD}^+$  (Figures 13S, 17S) making that less or equal to the flux of the electrochemical NADH oxidation at a given value of  $A_t$ . That's why, at low  $\text{NAD}^+$  loading the response of the biosensors is limited by the enzymatic reduction of  $\text{NAD}^+$  even if  $\Gamma k_{\text{cat}}$  is less than  $LV_1$  (Figures 14S, 18S). The Eadie-Hofstee plots show linear parts in the range of low substrate concentrations ( $B_\infty$ ) in the Figures 11S, 12S, 13S, 15S, 16S, 17S and none linear parts in the range of high substrate concentrations. Therefore they can yield correct values of Michaelis constants ( $K_B$ ) and the maximum flux of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ) in the range of low substrate concentrations even if the maximum response of the biosensors is limited by the rate of NADH oxidation at the electrode surface. That is true only if the transport of substrate is not a limiting factor. Certainly, the intercepts of none linear parts of Eadie-Hofstee plots with the axis of  $j$  give the correct values of the maximum response to glucose.

The Figures 19S-22S illustrate the influence of the maximum flux of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ), the  $\text{NAD}^+$  loading ( $A_t$ ), and the mass transfer constant of the substrate ( $k'_B$ ) on response of biosensors. The smaller are the  $\text{NAD}^+$  loading and the maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  in comparison with the maximum flux of the electrochemical NADH oxidation, the straighter are the Eadie-Hofstee plots. At lower concentrations of the substrate ( $B_\infty$ ) the slopes of the Eadie-Hofstee plots and hence the apparent Michaelis constants depend very much on  $k'_B$ . The effect of this factor on the apparent Michaelis constant is less pronounced at high values of  $B_\infty$ .

## GLOSSARY

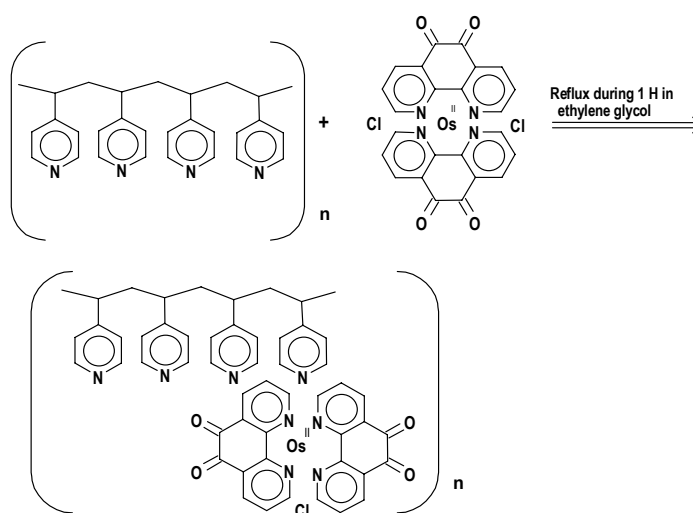
$j_{\text{el}}$	flux of reactants ( $\text{mol cm}^{-2} \text{s}^{-1}$ )
$j$	current density ( $\text{A cm}^{-2}$ )

$k_3, k_4, k_5, k_6, k_7$	rate constants of the elemental enzymatic reactions in forward direction ( $M^{-1} s^{-1}, M^{-1} s^{-1}, s^{-1}, s^{-1}, s^{-1}$ , respectively)
$k_{-3}, k_{-4}, k_{-5}, k_{-6}, k_{-7}$	rate constants of the elemental enzymatic reactions in backward direction ( $s^{-1}, s^{-1}, s^{-1}, M^{-1} s^{-1},$ and $M^{-1} s^{-1}$ , respectively)
$k_B^?$	mass transfer rate coefficient for the substrate ( $cm s^{-1}$ )
$k_Q^?$	mass transfer rate coefficient for the product ( $cm s^{-1}$ )
$L$	thickness of a hydrogel layer (cm)
$P_{im}$	concentration of NADH immobilized in the hydrogel (M)
$V_1$	maximum velocity of the enzymatic reaction in forward direction ( $s^{-1}$ )
$V_2$	maximum velocity of the enzymatic reaction in reverse direction ( $s^{-1}$ )

*Greek letters*

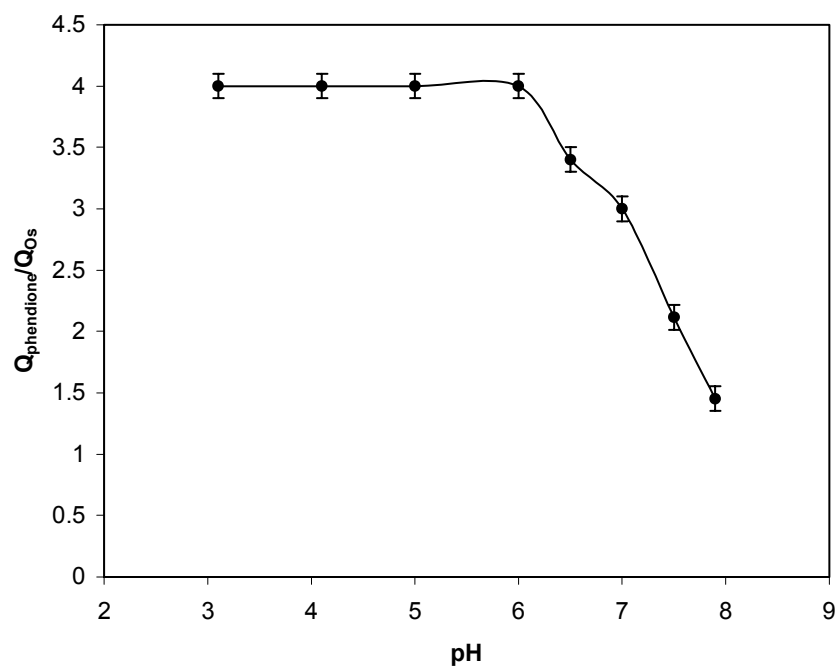
$\Gamma$	total surface coverage of Os-phendione-PVP ( $mol\ cm^{-2}$ )
$\Gamma_{Mox}$	surface coverage of the mediator in the oxidized form ( $mol\ cm^{-2}$ )
$\Gamma_{Mred}$	surface coverage of the mediator in the reduced form ( $mol\ cm^{-2}$ )
$\Gamma_{M \cdot P}$	surface coverage of the intermediate complex between Os-phendione-PVP and NADH ( $mol\ cm^{-2}$ )

**FIGURES AND FIGURE LEGENDS**

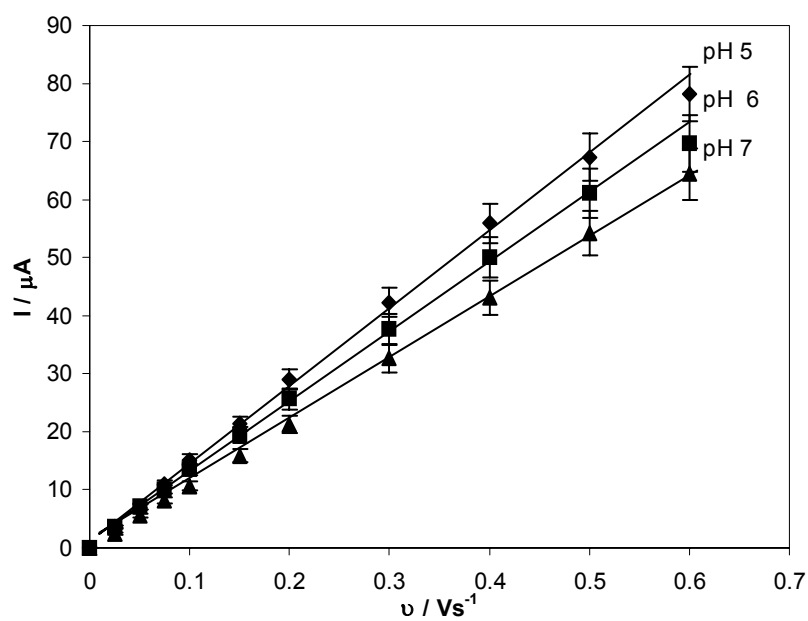


**Figure 1S.** The synthetic route to Os-phendione-PVP.

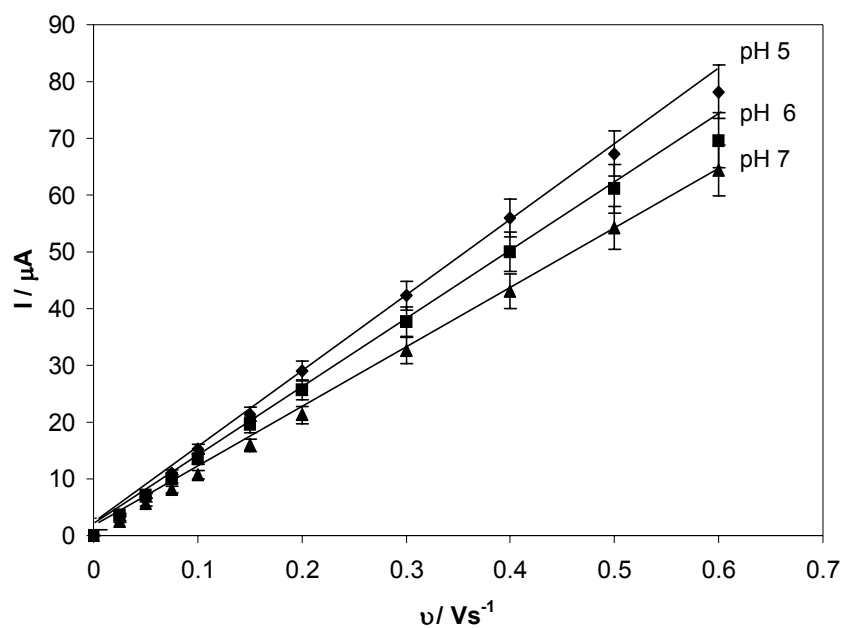




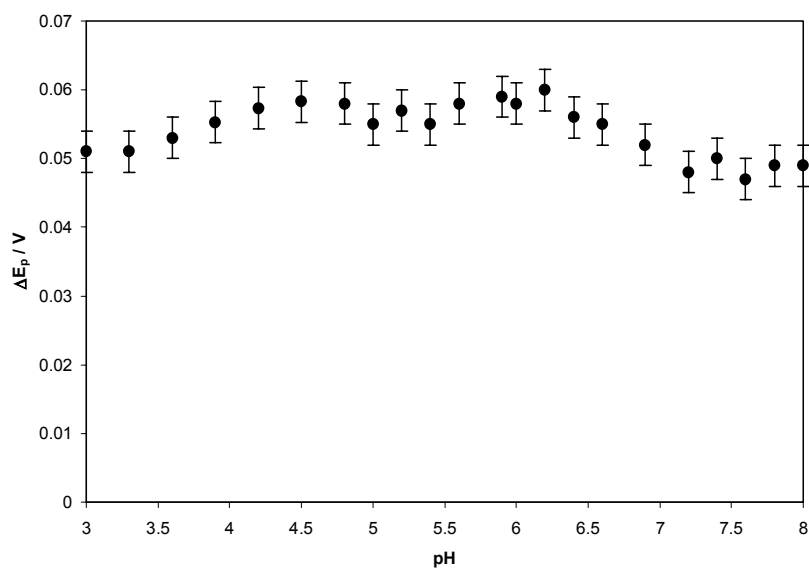
**Figure 2S.** The effect of pH on the ratio of phendione peak area to that of osmium atom in cyclic voltammetry.



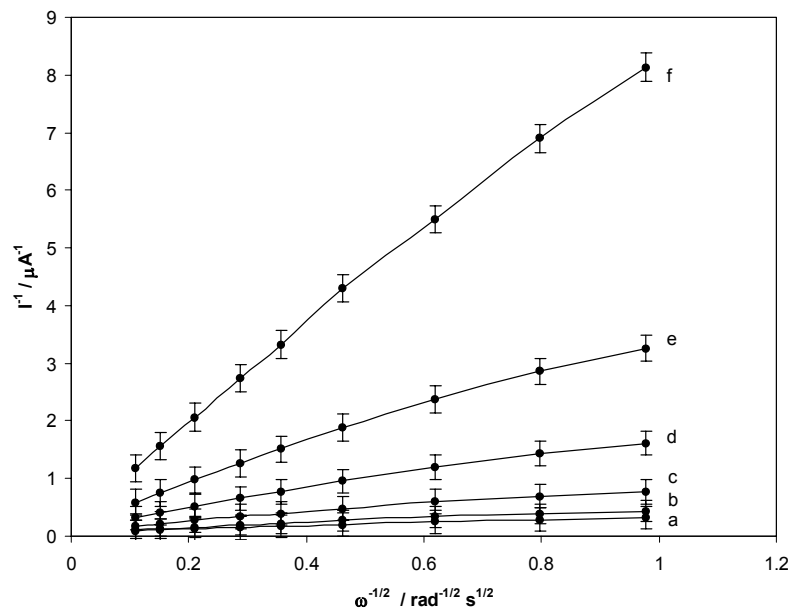
**Figure 3S.** The effect of scan rate on the anodic peak current of phendione. Experimental conditions: Os-phendione-PVP coverage  $(6.7 \pm 0.5) \times 10^{-10} \text{ mol cm}^{-2}$ , 0.1 M phosphate buffer.



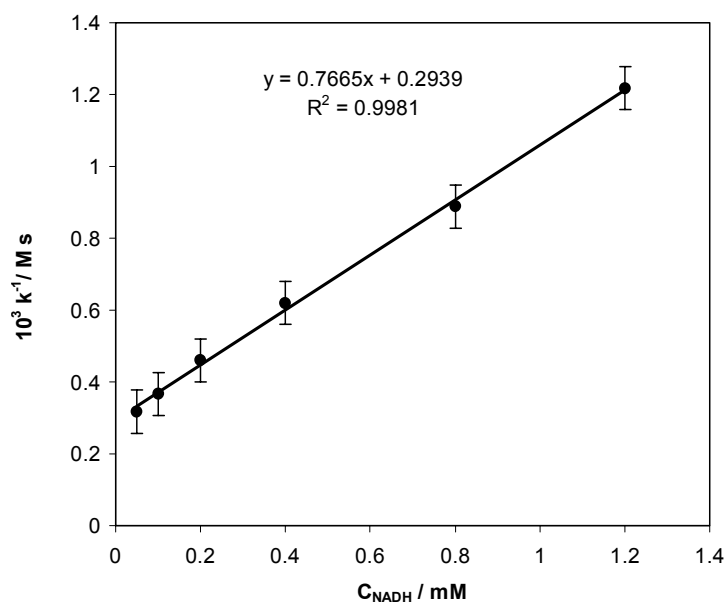
**Figure 4S.** The effect of scan rate on the cathodic peak current of phendione. Experimental conditions are the same as in Figure 3S.



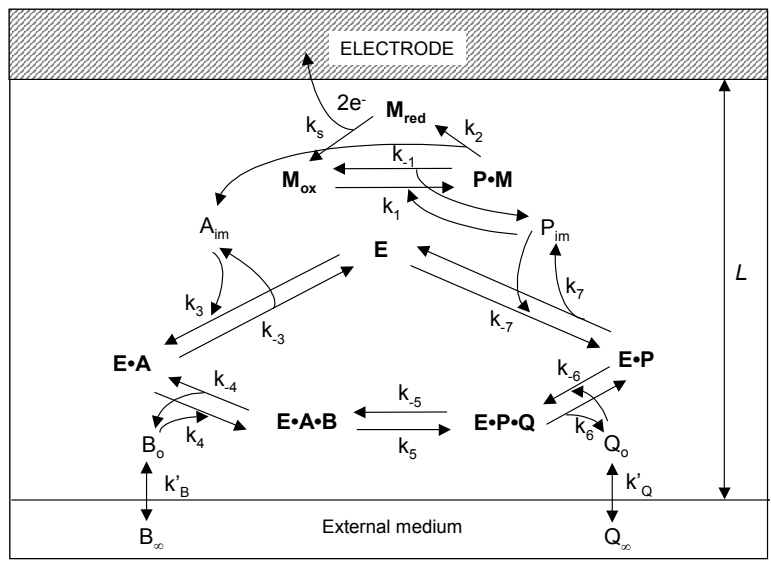
**Figure 5S.** Variation of  $\Delta E_p$  as a function of pH. Experimental conditions are the same as in Figure 2.



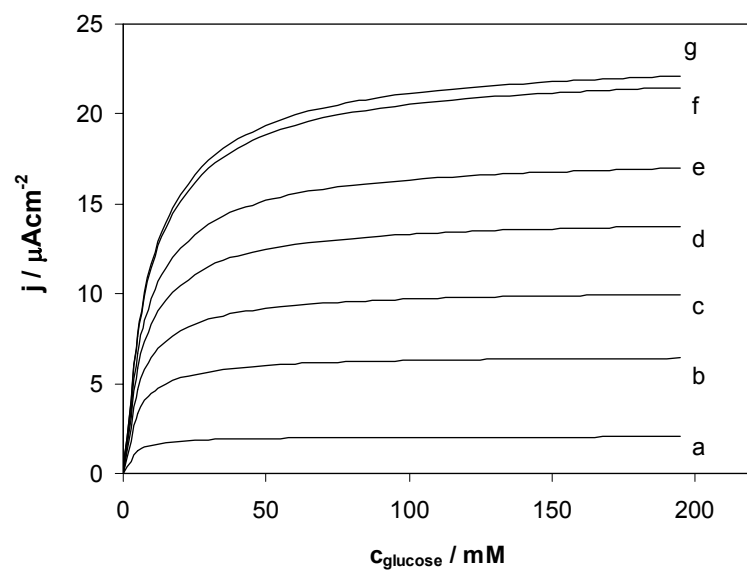
**Figure 6S.** Koutecky-Levich plot of steady state electrocatalytic response for an Os-phenidone-PVP modified graphite RDE at different NADH concentrations: a) 0.05 mM; b) 0.1 mM; c) 0.2 mM; d) 0.4 mM; e) 0.8 mM; f) 1.2 mM. Experimental conditions: Os-phenidone-PVP coverage  $(7.3 \pm 0.3) \times 10^{-10}$  mol cm<sup>-2</sup>; applied potential 200 mV vs. Ag/AgCl/KCl<sub>sat</sub>, 0.1 M phosphate buffer, pH 5.0, deaerated with argon.



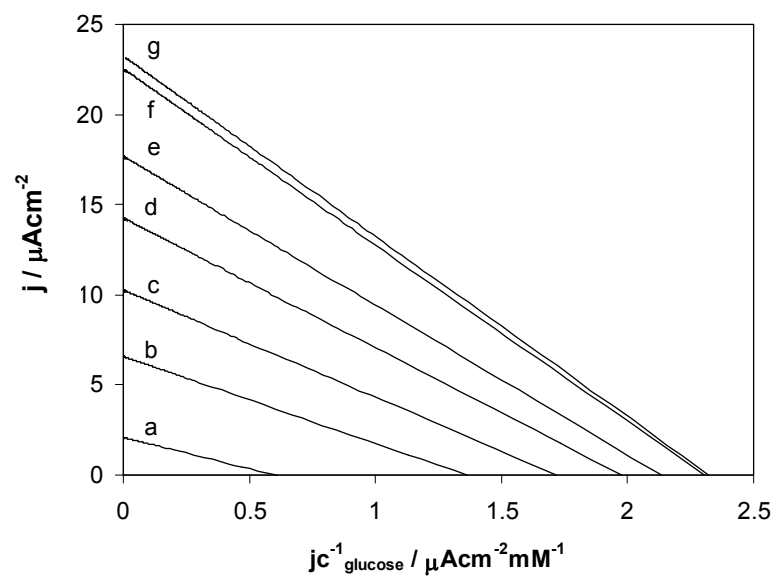
**Figure 7S.** Plot of  $k^{-1}$  vs. concentration of NADH for the electrooxidation of NADH at Os-phenidone-PVP modified electrodes. Experimental conditions are the same as in Figure 6S.



**Figure 8S.** Reaction scheme for a reagentless glucose biosensor.

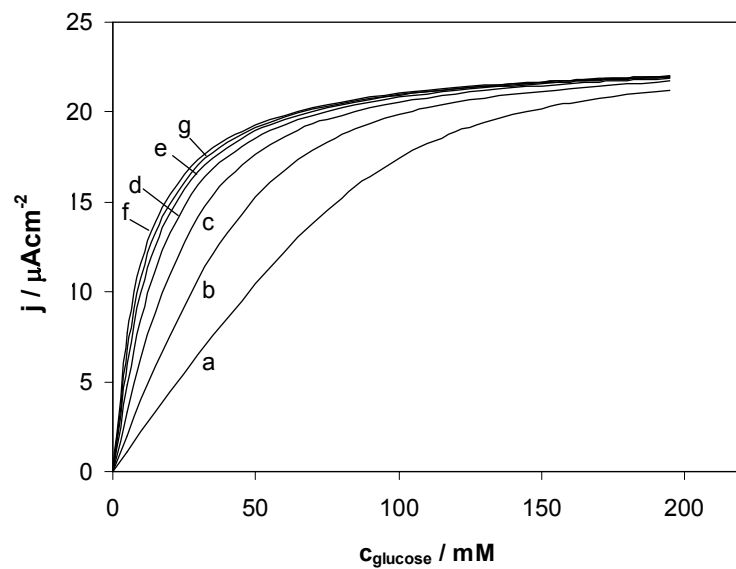


(A)

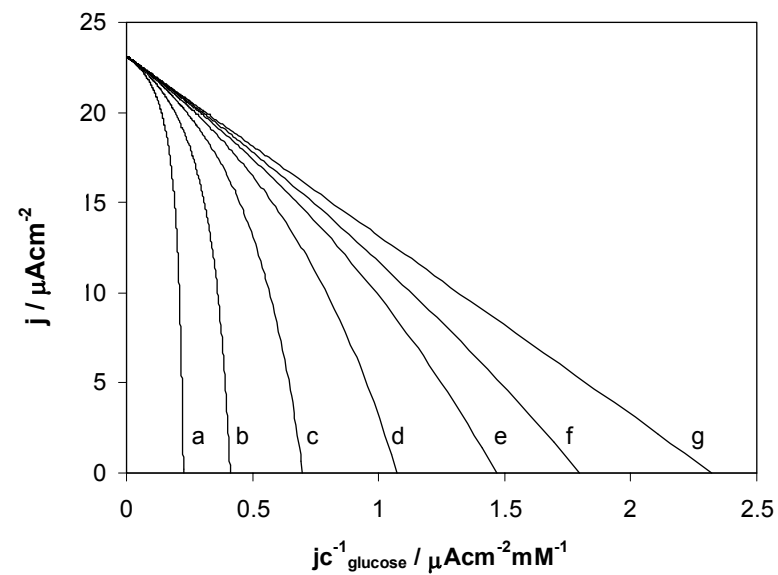


(B)

**Figure 9S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors with varying loading of  $\text{NAD}^+$  in the hydrogel ( $A_i$ ): a) 0.2 mM; b) 0.8 mM; c) 1.6 mM; d) 3.2 mM; e) 6.4 mM; f) 64 mM; g)  $\infty$ . The values of other parameters are:  $\Gamma k_{\text{cat}} = 2.55 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $LV_1 = 1.2046 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $k'_{\text{B} \rightarrow} \rightarrow \infty$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .

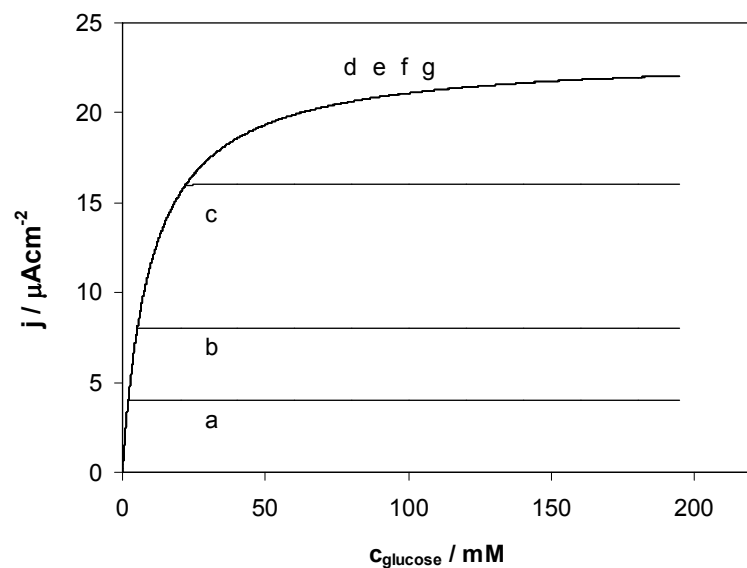


**(A)**

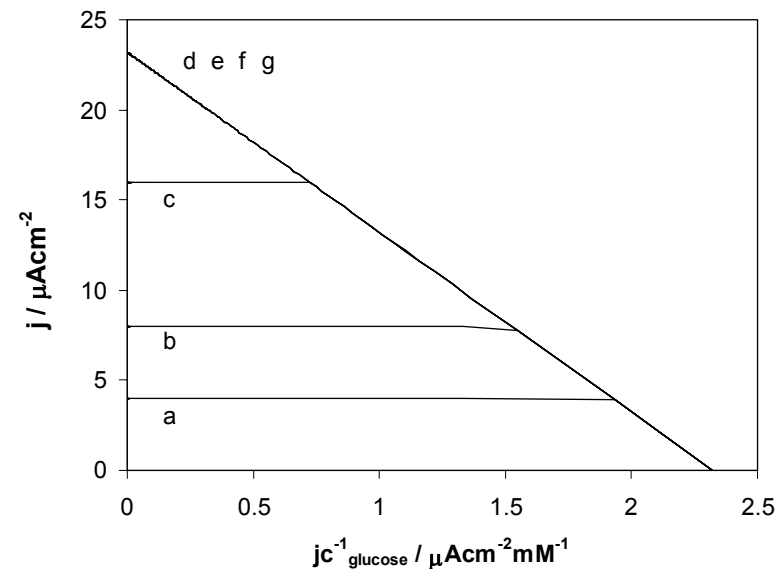


**(B)**

**Figure 10S.** Simulation of calibration curves **(A)** and Eadie-Hofstee plots **(B)** for the reagentless glucose biosensors with varying mass transfer coefficient ( $k'_B$ ): a)  $1.3 \times 10^{-12} \text{ cm s}^{-1}$ ; b)  $2.6 \times 10^{-12} \text{ cm s}^{-1}$ ; c)  $5.18 \times 10^{-12} \text{ cm s}^{-1}$ ; d)  $1.04 \times 10^{-11} \text{ cm s}^{-1}$ ; e)  $2.07 \times 10^{-11} \text{ cm s}^{-1}$ ; f)  $4.15 \times 10^{-11} \text{ cm s}^{-1}$ ; g)  $\infty$ . The values of other parameters are:  $A_t \rightarrow \infty$ ;  $\Gamma k_{\text{cat}} = 2.55 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $LV_1 = 1.2046 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .

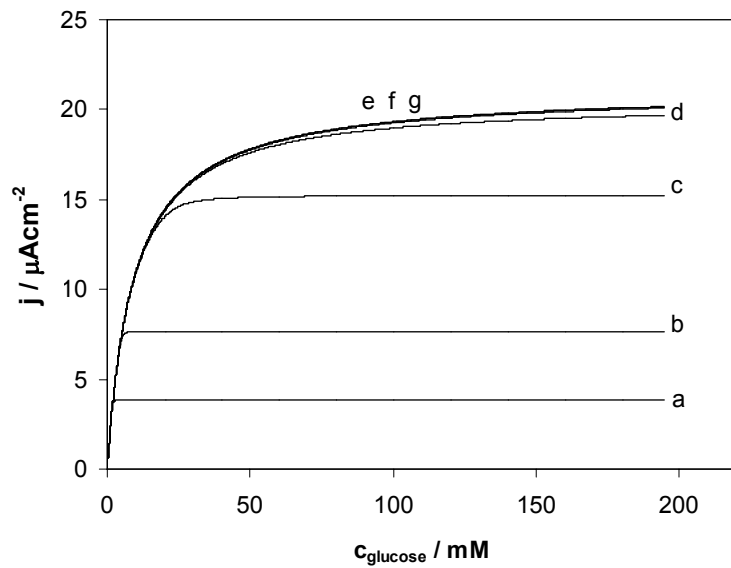


(A)

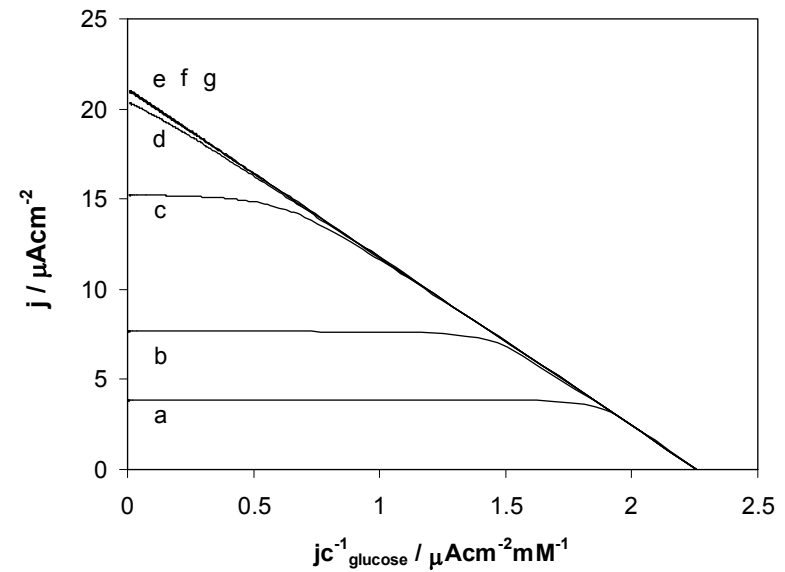


(B)

**Figure 11S.** Simulation of calibration curves **(A)** and Eadie-Hofstee plots **(B)** for the reagentless glucose biosensors at  $A_t \rightarrow \infty$  with varying maximum fluxes of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ): a)  $2.073 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $4.145 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $8.291 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.073 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.145 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $\infty$ . The values of other parameters are:  $k_{\text{B}}^{\rightarrow} \rightarrow \infty$ ;  $LV_1 = 1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_{\text{A}} = 2 \text{ mM}$ ;  $K_{\text{B}} = 10 \text{ mM}$ ;  $K_{\text{AB}} = 5.6 \text{ mM}^2$ ;  $K_{\text{M}} = 0.8 \text{ mM}$ .



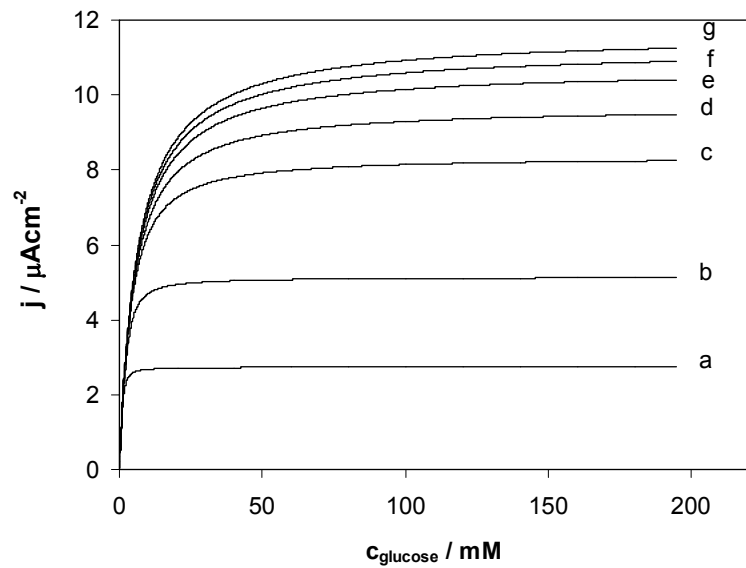
(A)



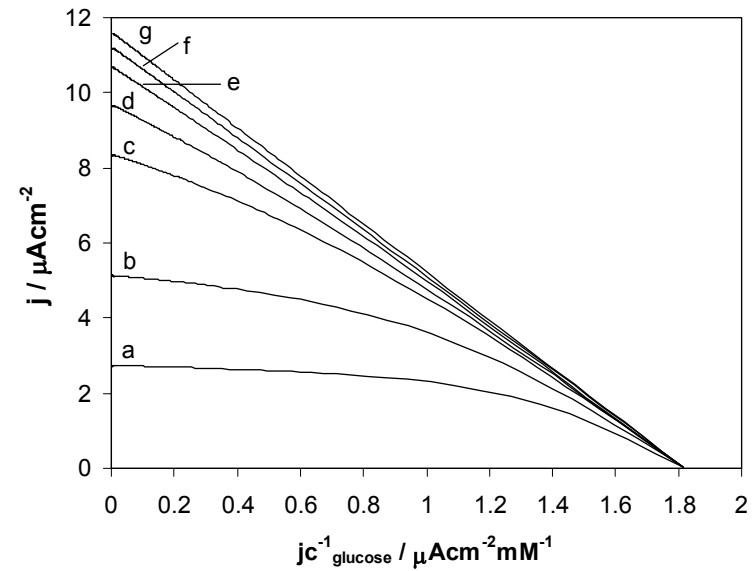
(B)

**Figure 12S.** Simulation of calibration curves **(A)** and Eadie-Hofstee plots **(B)** for the reagentless glucose biosensors at  $A_t$  equal to 20 mM with varying maximum fluxes of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ): a)  $2.073 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $4.145 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $8.291 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.073 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.145 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $\infty$ . The values of other parameters are:  $k'_B \rightarrow \infty$ ;  $LV_1 = 1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .



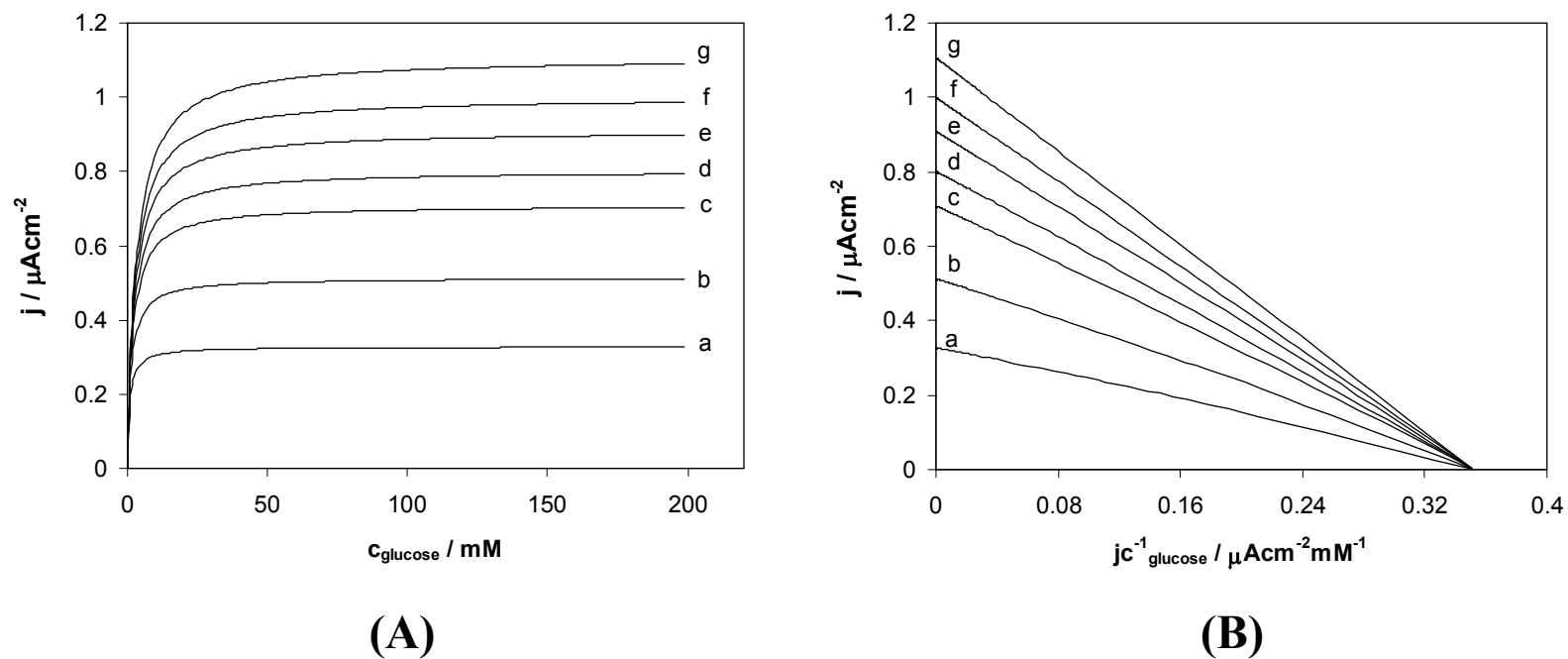


(A)

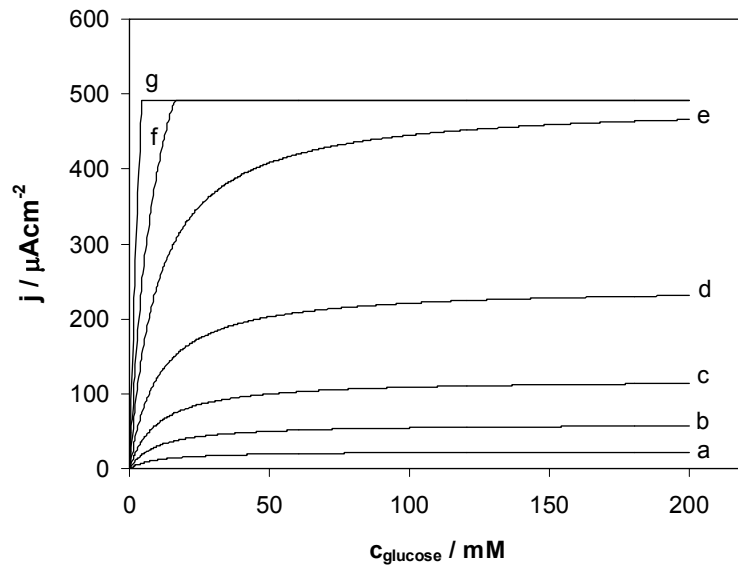


(B)

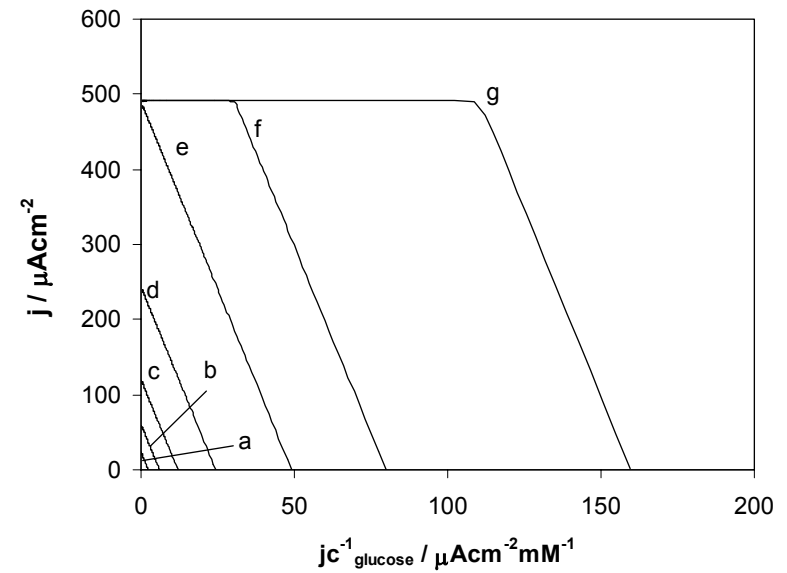
**Figure 13S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors at  $A_t$  equal to 2 mM with varying maximum fluxes of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ): a)  $2.073 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $4.145 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $8.291 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.073 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.145 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $\infty$ . The values of other parameters are:  $k'_{\text{B}} \rightarrow \infty$ ;  $LV_1 = 1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .



**Figure 14S.** Simulation of calibration curves **(A)** and Eadie-Hofstee plots **(B)** for the reagentless glucose biosensors at  $A_i$  equal to 0.1 mM with varying maximum fluxes of the electrochemical NADH oxidation ( $\Gamma k_{\text{cat}}$ ): a)  $2.073 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $4.145 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $8.291 \times 10^{-11} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.073 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.145 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $\infty$ . The values of other parameters are:  $k'_{\text{B}} \rightarrow \infty$ ;  $LV_1 = 1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_{\text{A}} = 2 \text{ mM}$ ;  $K_{\text{B}} = 10 \text{ mM}$ ;  $K_{\text{AB}} = 5.6 \text{ mM}^2$ ;  $K_{\text{M}} = 0.8 \text{ mM}$ .

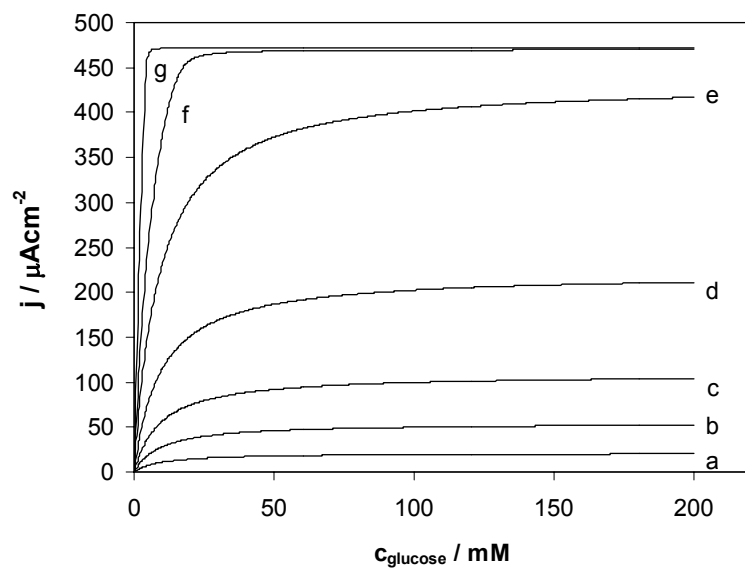


(A)

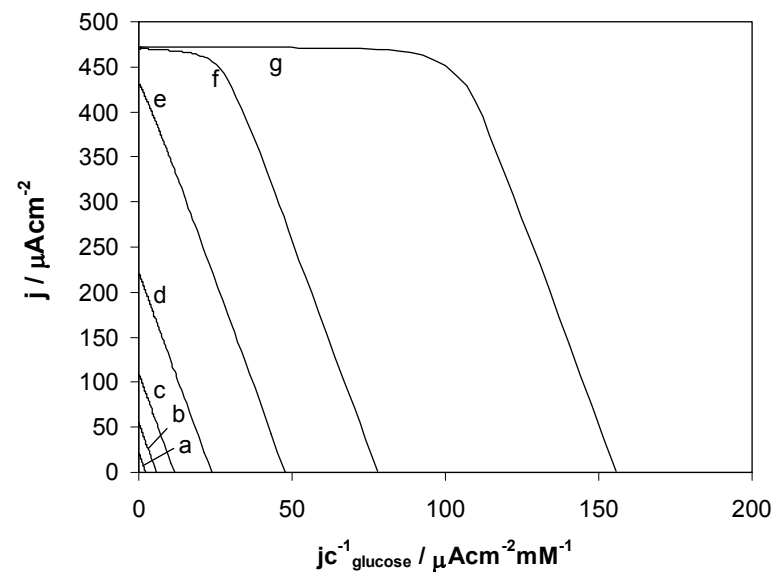


(B)

**Figure 15S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors at  $A_t \rightarrow \infty$  with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $k'_{B \rightarrow \infty}$ ;  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$

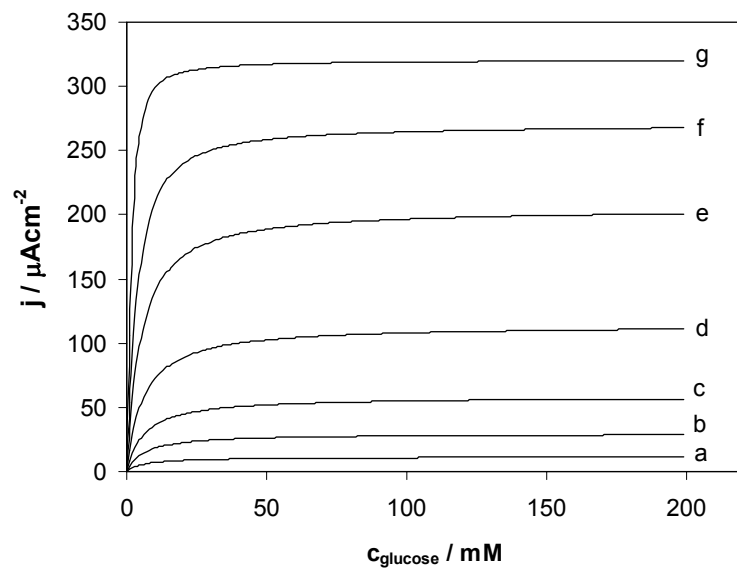


(A)

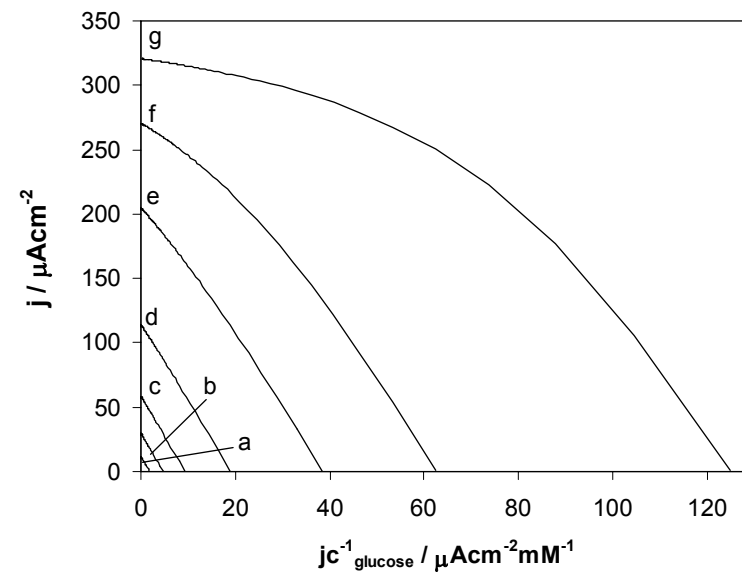


(B)

**Figure 16S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors at  $A_i$  equal to 20 mM with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $k'_{B \rightarrow \infty}$ ;  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .

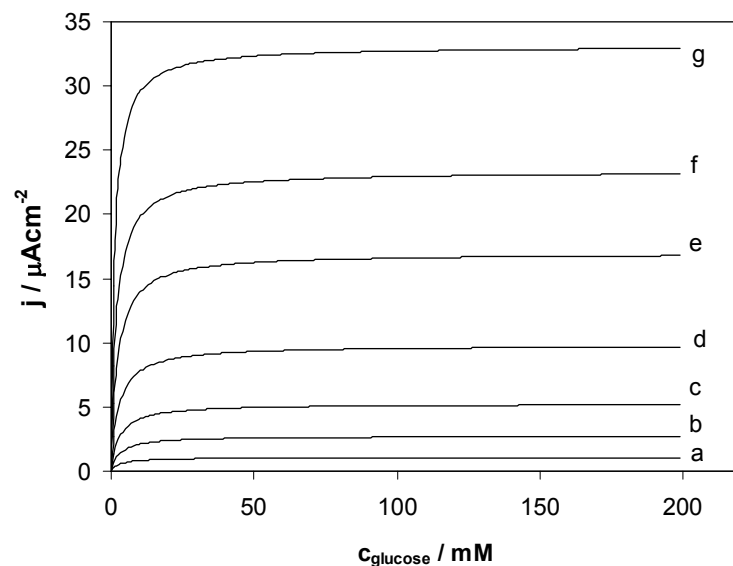


(A)

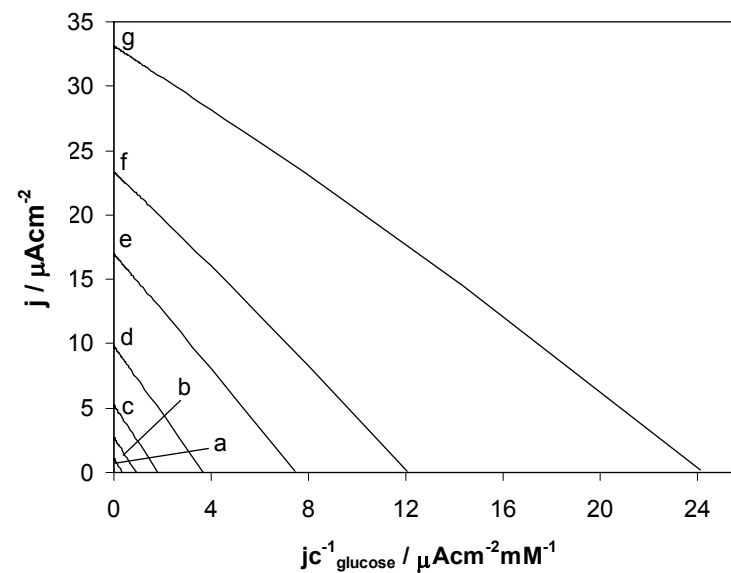


(B)

**Figure 17S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors at  $A_t$  equal to 2.0 mM with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $k_{B \rightarrow \infty}^2$ ;  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$

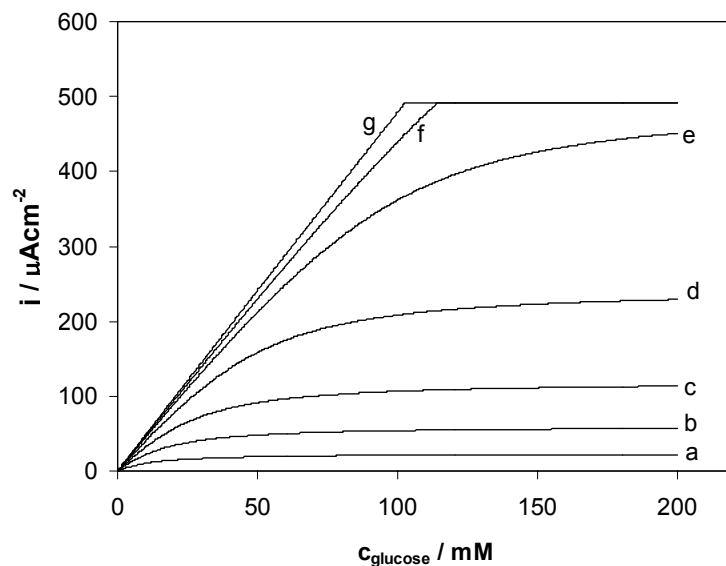


(A)

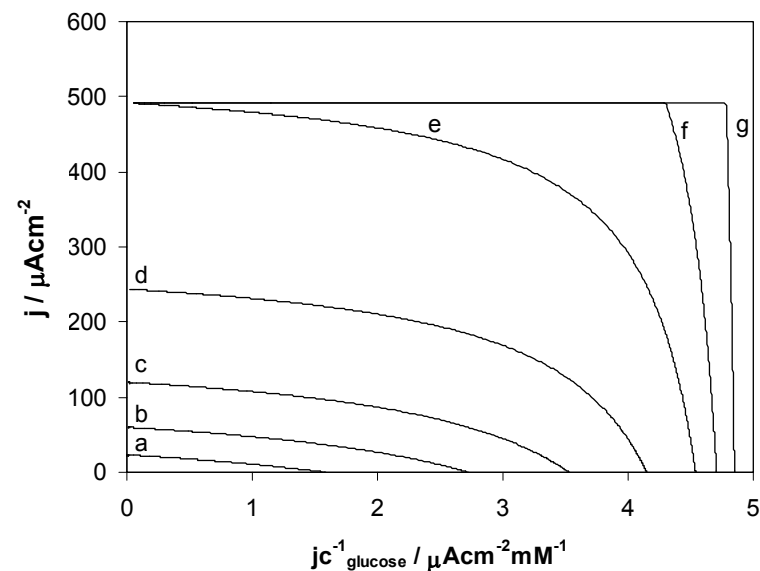


(B)

**Figure 18S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors at  $A_t$  equal to 0.1 mM with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $k_B^2 \rightarrow \infty$ ;  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .

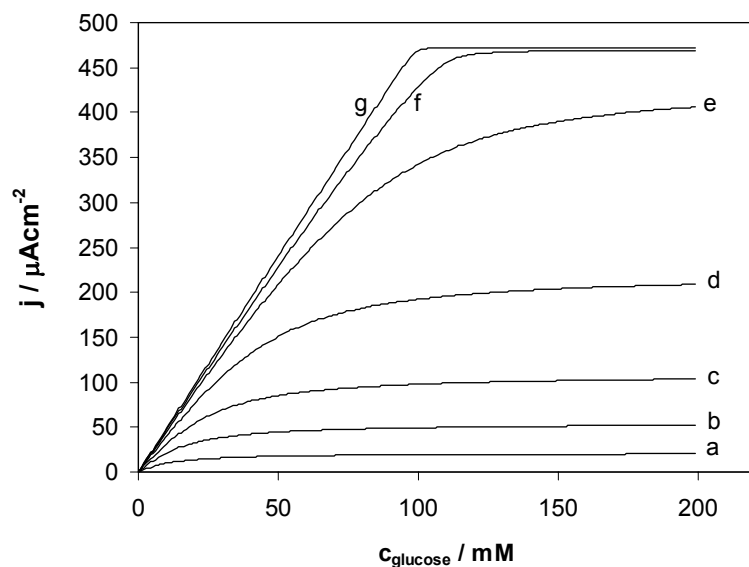


**(A)**

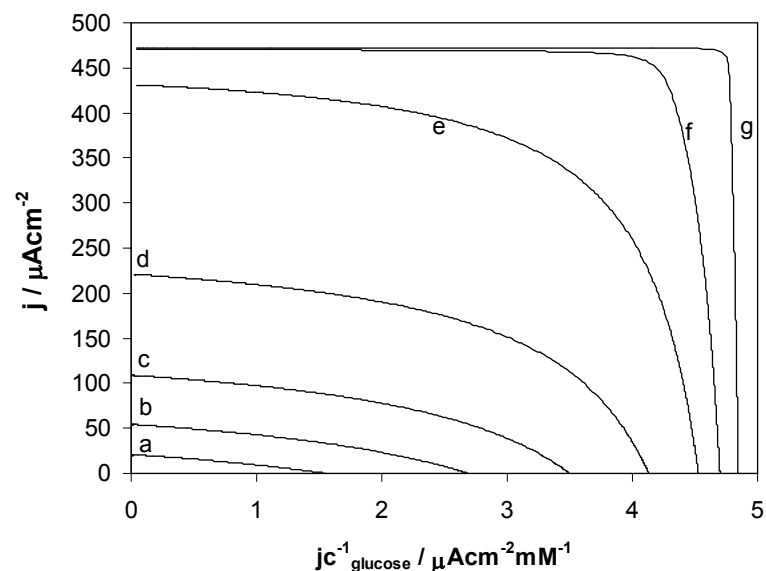


**(B)**

**Figure 19S.** Simulation of calibration curves **(A)** and Eadie-Hofstee plots **(B)** for the reagentless glucose biosensors at  $k_B^2$  equal to  $2.591 \times 10^{-11} \text{ cm s}^{-1}$  and  $A_t \rightarrow \infty$  with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .



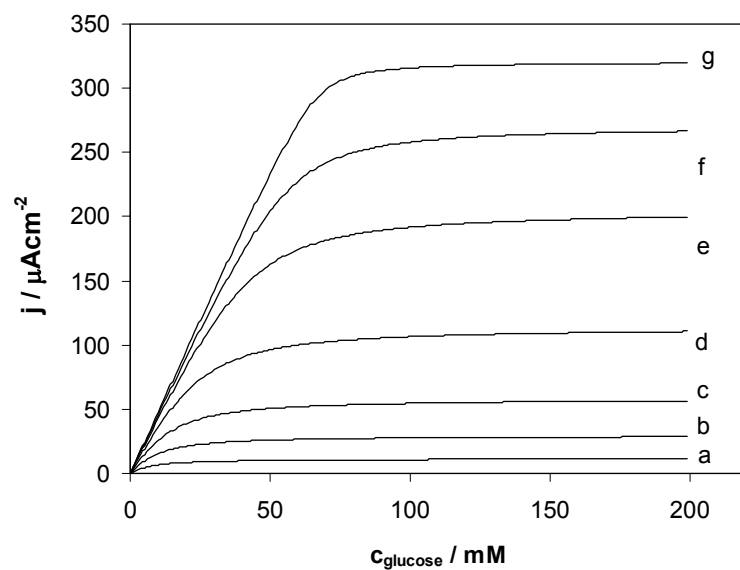
(A)



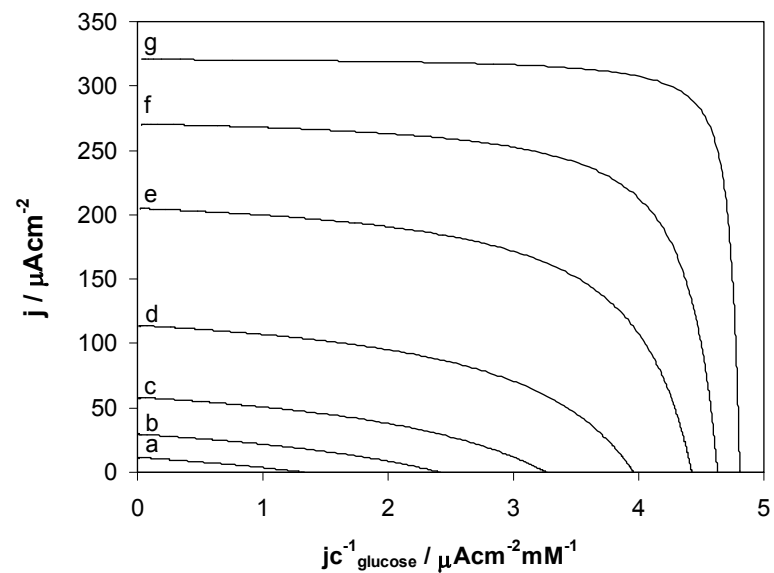
(B)

**Figure 20S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors at  $k'_B$  equal to  $2.591 \times 10^{-11} \text{ cm s}^{-1}$  and  $A_i$  equal to 20 mM with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .



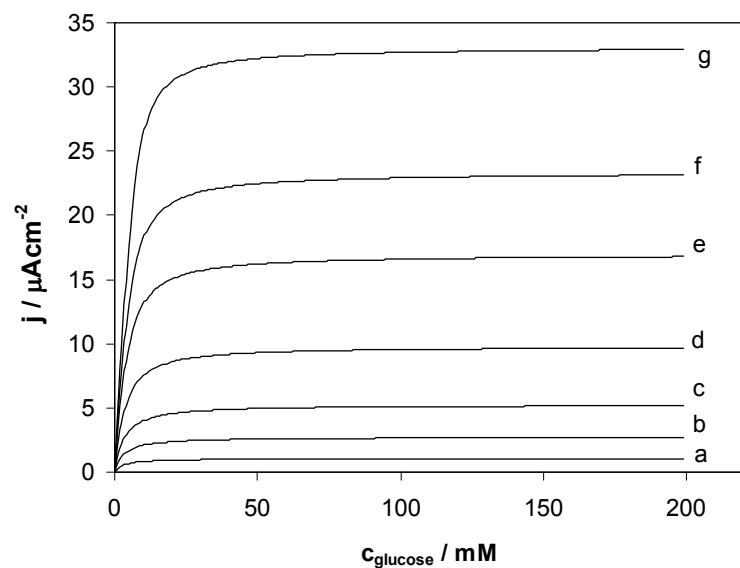


(A)

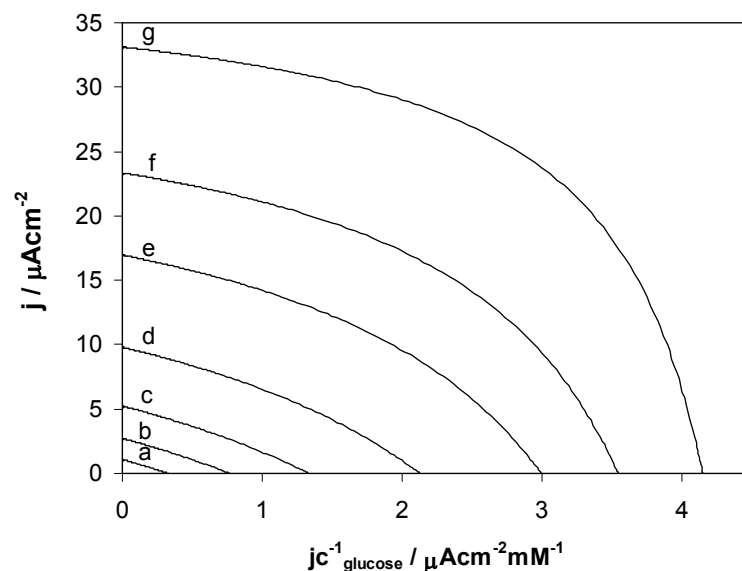


(B)

**Figure 21S.** Simulation of calibration curves **(A)** and Eadie-Hofstee plots **(B)** for the reagentless glucose biosensors at  $k'_B$  equal to  $2.591 \times 10^{-11} \text{ cm s}^{-1}$  and  $A_i$  equal to 2.0 mM with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .

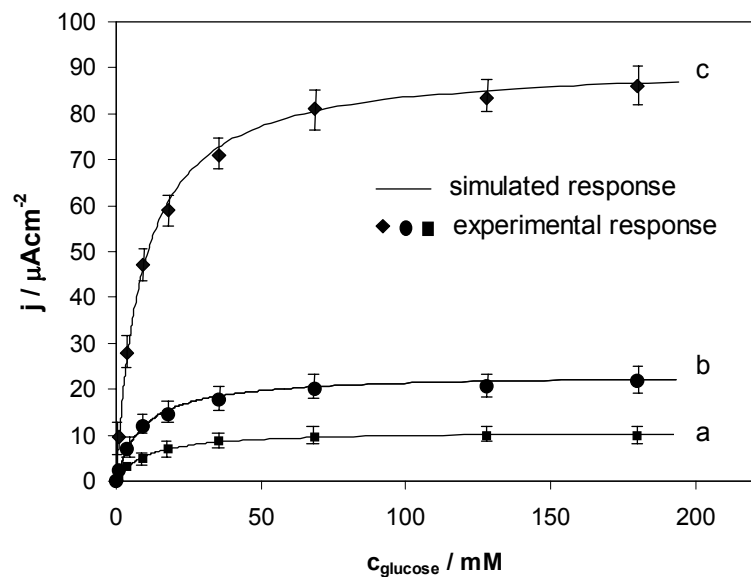


(A)

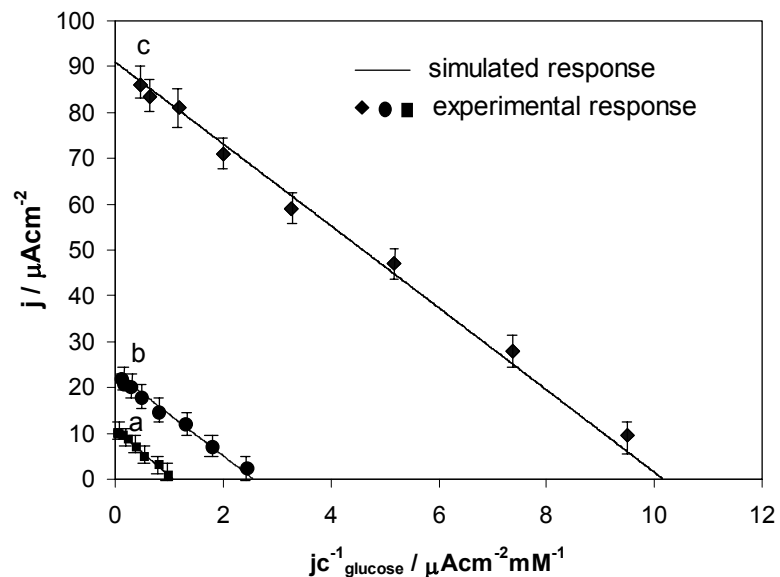


(B)

**Figure 22S.** Simulation of calibration curves (A) and Eadie-Hofstee plots (B) for the reagentless glucose biosensors at  $k_B^*$  equal to  $2.591 \times 10^{-11} \text{ cm s}^{-1}$  and  $A_t$  equal to  $0.1 \text{ mM}$  with varying maximum fluxes of the enzymatic reduction of  $\text{NAD}^+$  ( $LV_1$ ): a)  $1.204 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; b)  $3.109 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; c)  $6.218 \times 10^{-10} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; d)  $1.264 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; e)  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; f)  $4.146 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ; g)  $8.281 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of other parameters are:  $\Gamma k_{\text{cat}} = 2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ ;  $K_A = 2 \text{ mM}$ ;  $K_B = 10 \text{ mM}$ ;  $K_{AB} = 5.6 \text{ mM}^2$ ;  $K_M = 0.8 \text{ mM}$ .

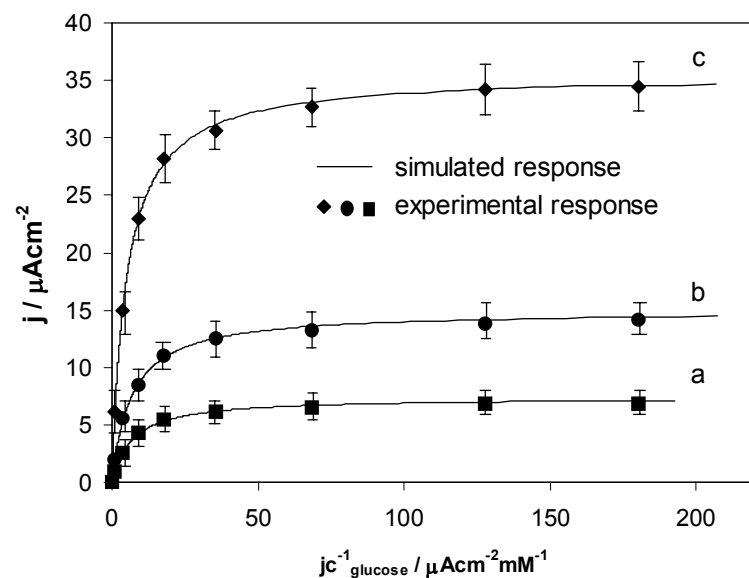


(A)

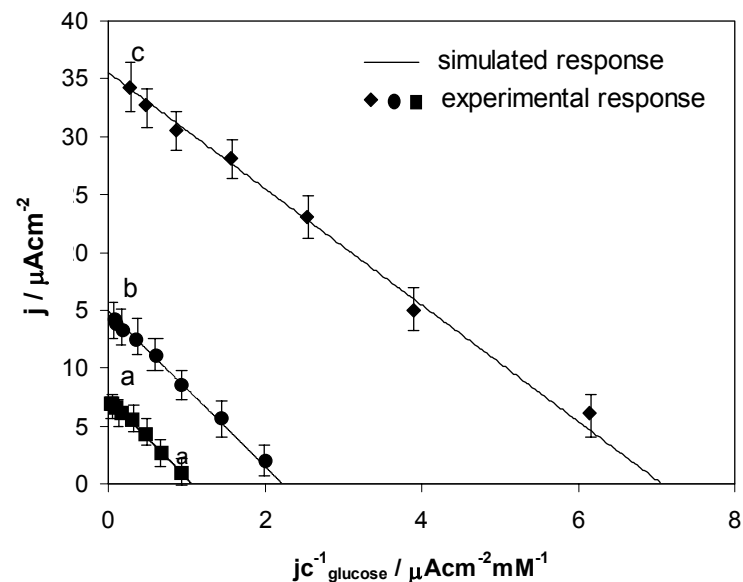


(B)

**Figure 23S.** Simulated and experimental calibration curves (A) and Eadie-Hofstee plots (B) for the biosensors prepared using varied loading of GDH per electrode: a) 0.135 U; b) 0.027 U; c) 0.0135 U. Experimental conditions: temperature 25°C, applied potential 150 mV vs. Ag/AgCl/KCl<sub>sat</sub>, 0.1 M phosphate buffer, pH 7.0, containing 26 mM NAD<sup>+</sup>. The value of  $\Gamma k_{\text{cat}}$  employed for fitting and simulation was  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$ . The values of  $K_B$ ,  $LV_1$ , and  $k_B'$  found by fitting and employed for simulation are listed in Table III.



(A)



(B)

**Figure 24S.** Simulated and experimental calibration curves (A) and Eadie-Hofstee plots (B) for the biosensors operating in the reagentless mode prepared using varied loading of GDH per electrode: a) 0.135 U; b) 0.027; c) 0.0135 U. Experimental conditions: temperature 25°C, applied potential 150 mV vs. Ag/AgCl/KCl<sub>sat</sub>, 0.1 M phosphate buffer, pH 7.0. The values of  $\Gamma k_{\text{cat}}$  and  $K_M$  employed for fitting and simulation were  $2.549 \times 10^{-9} \text{ mol s}^{-1} \text{ cm}^{-2}$  and 0.8 mM respectively. The values of  $k'_B$ ,  $K_A$ ,  $K_{AB}$ ,  $K_B$ ,  $LV_1$ , and  $A_i$  found by fitting and employed for simulation are listed in Tables III and IV.