

TOMO II: APENDICES.

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APENDICE A : Respuesta inversa de una central hidroeléctrica.

Este efecto de fase no mínima es consecuencia de las variaciones de presión derivadas del "golpe de ariete", y depende del diseño concreto de las tuberías, por lo que no siempre tendrá igual importancia. Esto se puede ver de una forma sencilla: la potencia N generada por una turbina puede expresarse como

$$N = K p Q$$

donde p y Q son, respectivamente, la presión y el caudal, y K es una constante que depende del diseño. Por otro lado,

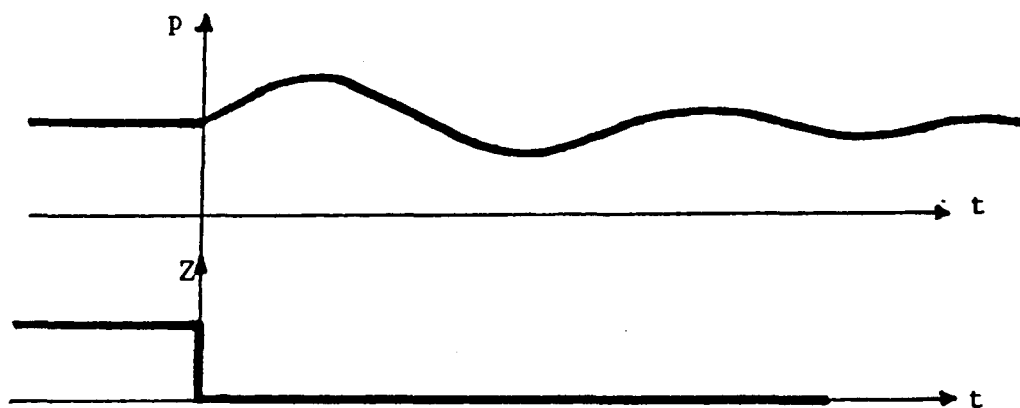
$$Q = Z \sqrt{p}$$

siendo Z la apertura del distribuidor.

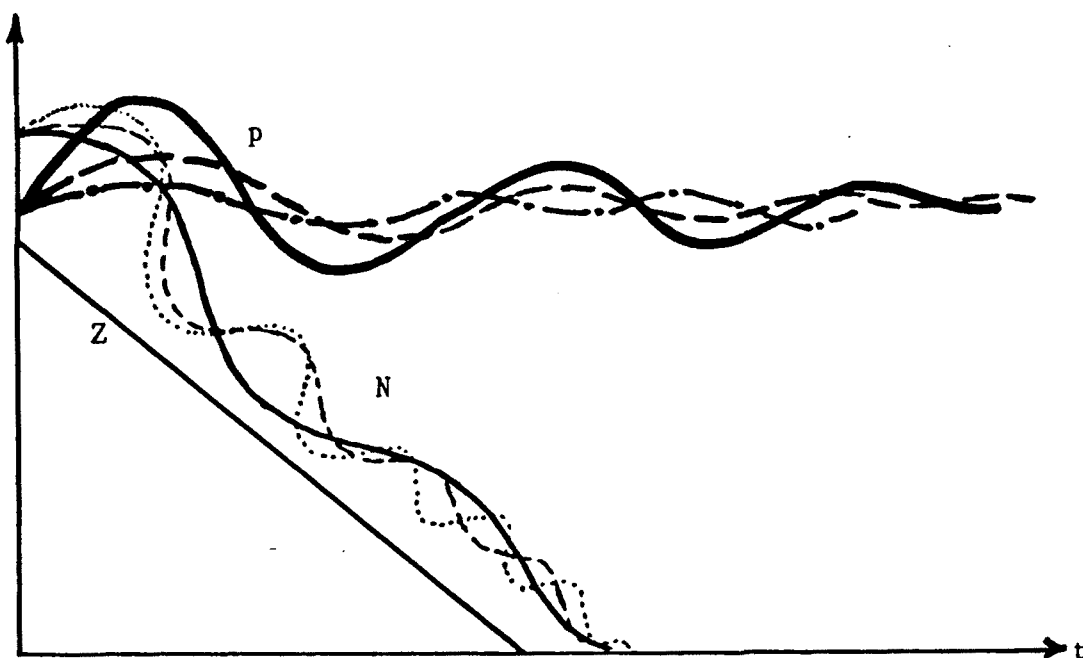
Combinando ambas fórmulas tenemos:

$$N = K Z p^{3/2}$$

Ante una modificación de Z , el efecto del golpe de ariete hace oscilar el nivel de la presa, con las correspondientes variaciones de p .



Considerando la expresión anterior ($N = KZp^{3/2}$), podemos ver, con ayuda del siguiente gráfico:

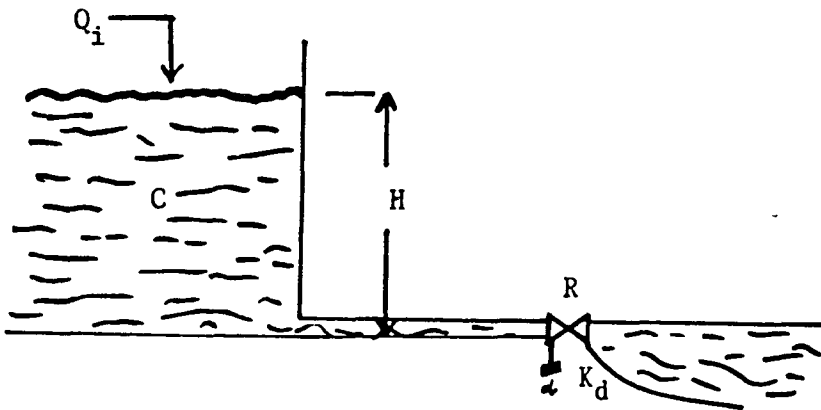


que la variación de la potencia N asociada a una disminución de apertura del distribuidor puede pasar, transitoriamente, por valores superiores a los que tenía antes de modificarse el valor de Z . Ello supondría que, al disminuir Z con el objetivo de disminuir el nivel de potencia generada en una central, el sistema empezara respondiendo con un aumento de potencia (podríamos obtener unas conclusiones duales ante un aumento de Z).

El estudio de este primer transitorio es especialmente importante en el modelado conjunto de los sistemas de regulación de velocidad y de tensión. Si bien para el análisis y diseño de RFP no es tan importante, no por ello puede ser menospreciado, dados los efectos desestabilizadores de la respuesta inversa del sistema.

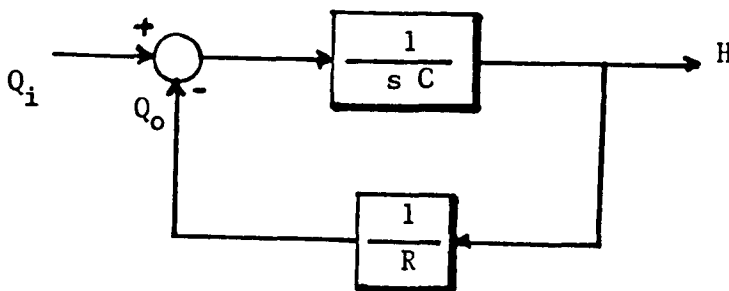
APENDICE B: Ajuste del parámetro T_w .

Hay formas sencillas y bien conocidas [100] para obtener el valor del parámetro T_w de modelo clásico. Sin embargo, los valores de T_w obtenidos de este modo sólo son válidos para cotas y niveles de carga elevados. A fin de disponer de unos criterios adicionales a los de Smith et al. y a los de Woodward para la corrección del valor T_w , se ha elaborado un estudio que nos ha llevado a la obtención de la fig. AB.1, en la que se muestra la evolución de la constante de tiempo de la turbina en función de la apertura del distribuidor (Z) y de la cota (h). Para ello se ha usado, en primer lugar, el modelo de Jasmin et al., sobre el que hemos obtenido, via simulación, el valor de la constante de tiempo dominante del conjunto tubería-turbina para diferentes valores de h y de Z . En segundo lugar lo hemos comparado con un modelo simple, deducido de forma sencilla:

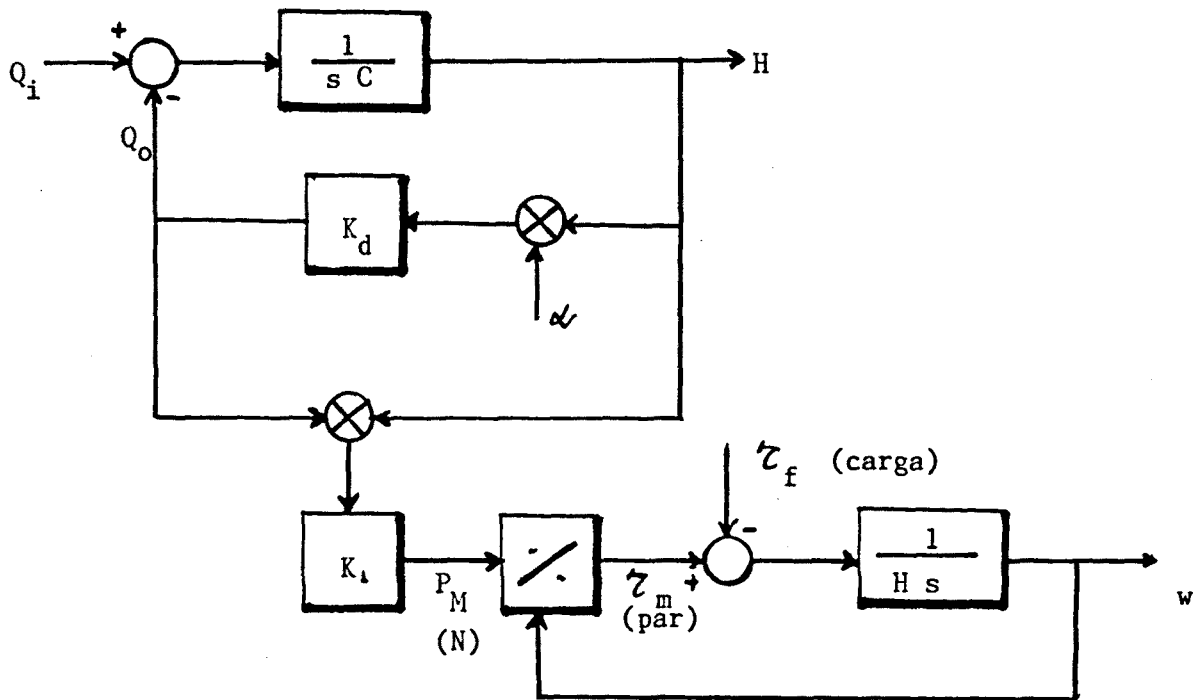


$$R = K_d \cdot \alpha$$

$$\alpha = \% \text{ apertura.}$$



$$\frac{Q_o}{Q_i} = \frac{1}{1 + sRC} \quad , \quad RC = \tau_H$$



Como se desprende de la fig. AB.1, la velocidad de respuesta del circuito hidráulico es más sensible a la apertura (Z ó α) del distribuidor que a la cota h de la presa. Para niveles de apertura elevados, una variación relativa de la apertura modifica poco la velocidad de respuesta, mientras que para aperturas reducidas la dinámica es muy sensible al grado de apertura. Por otro lado, la variación de la cota (manteniéndose fija la apertura) modifica menos la dinámica del conjunto hidráulico.

Otra conclusión que se desprende de la figura es la validez del modelo teórico simplificado para este estudio, lo que evita la complejidad de simulación asociada a modelos tales como los de Jasmin et al.

La validez de estas curvas no ha podido ser rigurosamente evaluada. Sin embargo, dada la bondad de las previsiones del modelo de Jasmin et al. (demostrada en su artículo), extrapolamos una buena fiabilidad en la información cualitativa de las curvas de la fig. AB.1.

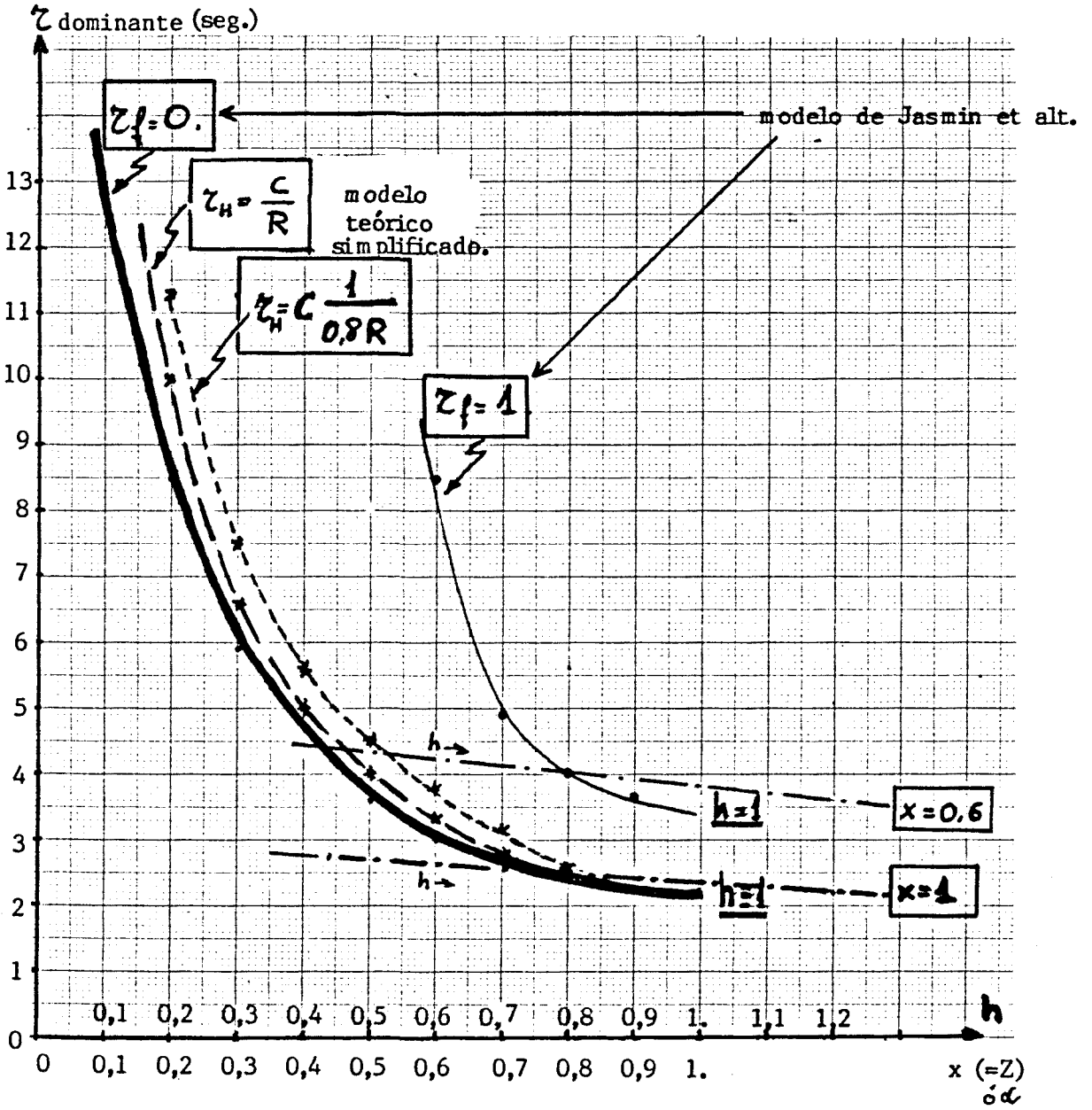
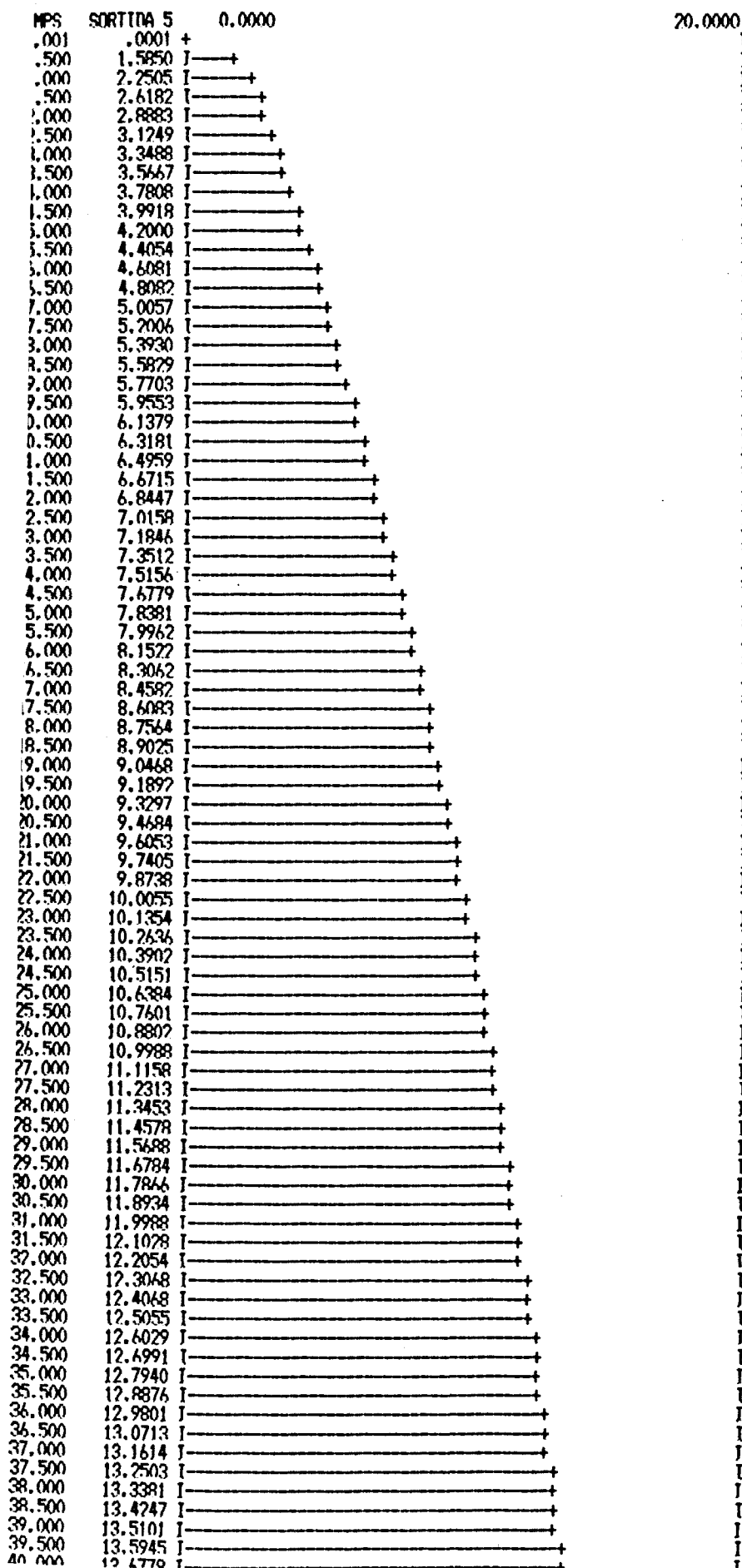


Fig. AB.1

APENDICE C :Resultados de simulación correspondientes al Capítulo 2.Gráficas:

- RSR-1 a RSR-21 : Respuesta de la apertura de los distribuidores de diferentes reguladores de velocidad de centrales hidroeléctricas.
- RS-1 a RS-9 : Elaboración del modelo reducido equivalente del Area 1.
- RS-17 a RS-23 : Funcionamiento primario del Area 1.
- RS-24 a RS-38 : Simulación del comportamiento del Area 1 acoplada al modelo de la carga del Area 2 para diferentes ganancias en la interconexión (T_{ie}).
- RS-39 a RS-60 : Simulación del funcionamiento primario de las dos áreas interconectadas.
- RS-61 a RS-62 : Modelo de simulación.
- RS-63 a RS-69 : Inclusión de alinealidades en los detectores de velocidad.

LOC FIX Y (5) MINIM (0.0000) MAXIM (20.0000)



RSR-1 (Ilvey)

LOC EIX Y (5) MINIM (0.0000) MAXIM (25.0000)

WPS	SORTIDA 5	0.0000	25.0000
.001	.0001	+	I
.500	1.6855	I → +	I
1.000	2.4709	I → +	I
1.500	2.9112	I → +	I
2.000	3.2184	I → +	I
2.500	3.4734	I → +	I
3.000	3.7069	I → +	I
3.500	3.9309	I → +	I
4.000	4.1499	I → +	I
4.500	4.3655	I → +	I
5.000	4.5786	I → +	I
5.500	4.7892	I → +	I
6.000	4.9977	I → +	I
6.500	5.2040	I → +	I
7.000	5.4081	I → +	I
7.500	5.6101	I → +	I
8.000	5.8101	I → +	I
8.500	6.0080	I → +	I
9.000	6.2038	I → +	I
9.500	6.3977	I → +	I
10.000	6.5895	I → +	I
10.500	6.7793	I → +	I
11.000	6.9672	I → +	I
11.500	7.1532	I → +	I
12.000	7.3372	I → +	I
12.500	7.5194	I → +	I
13.000	7.6996	I → +	I
13.500	7.8780	I → +	I
14.000	8.0546	I → +	I
14.500	8.2293	I → +	I
15.000	8.4023	I → +	I
15.500	8.5734	I → +	I
16.000	8.7428	I → +	I
16.500	8.9104	I → +	I
17.000	9.0764	I → +	I
17.500	9.2406	I → +	I
18.000	9.4031	I → +	I
18.500	9.5639	I → +	I
19.000	9.7231	I → +	I
19.500	9.8806	I → +	I
20.000	10.0365	I → +	I
20.500	10.1908	I → +	I
21.000	10.3435	I → +	I
21.500	10.4947	I → +	I
22.000	10.6443	I → +	I
22.500	10.7923	I → +	I
23.000	10.9388	I → +	I
23.500	11.0838	I → +	I
24.000	11.2273	I → +	I
24.500	11.3693	I → +	I
25.000	11.5099	I → +	I
25.500	11.6490	I → +	I
26.000	11.7867	I → +	I
26.500	11.9229	I → +	I
27.000	12.0578	I → +	I
27.500	12.1912	I → +	I
28.000	12.3233	I → +	I
28.500	12.4540	I → +	I
29.000	12.5834	I → +	I
29.500	12.7115	I → +	I
30.000	12.8382	I → +	I
30.500	12.9636	I → +	I
31.000	13.0877	I → +	I
31.500	13.2105	I → +	I
32.000	13.3321	I → +	I
32.500	13.4524	I → +	I
33.000	13.5715	I → +	I
33.500	13.6894	I → +	I
34.000	13.8060	I → +	I
34.500	13.9214	I → +	I
35.000	14.0357	I → +	I
35.500	14.1487	I → +	I
36.000	14.2606	I → +	I
36.500	14.3714	I → +	I
37.000	14.4810	I → +	I
37.500	14.5894	I → +	I
38.000	14.6968	I → +	I
38.500	14.8030	I → +	I
39.000	14.9082	I → +	I
39.500	15.0122	I → +	I

RSR-2 (Ramey)

0.000 15.1152 |-----+ |

BLOC FIX Y (5) MINIM (0.0000) MAXIM (25.0000)

FMP5	SORTIDA 5	0.0000	25.0000
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10.500	15.2172	-----+	
11.000	15.3180	-----+	
11.500	15.4179	-----+	
12.000	15.5167	-----+	
12.500	15.6145	-----+	
13.000	15.7113	-----+	
13.500	15.8070	-----+	
14.000	15.9018	-----+	
14.500	15.9957	-----+	
15.000	16.0885	-----+	
15.500	16.1803	-----+	
16.000	16.2713	-----+	
16.500	16.3613	-----+	
17.000	16.4503	-----+	
17.500	16.5385	-----+	
18.000	16.6257	-----+	
18.500	16.7121	-----+	
19.000	16.7975	-----+	
19.500	16.8821	-----+	
20.000	16.9658	-----+	
20.500	17.0486	-----+	
21.000	17.1305	-----+	
21.500	17.2116	-----+	
22.000	17.2919	-----+	
22.500	17.3713	-----+	
23.000	17.4499	-----+	
23.500	17.5277	-----+	
24.000	17.6047	-----+	
24.500	17.6809	-----+	
25.000	17.7563	-----+	
25.500	17.8309	-----+	
26.000	17.9047	-----+	
26.500	17.9778	-----+	
27.000	18.0502	-----+	
27.500	18.1218	-----+	
28.000	18.1927	-----+	
28.500	18.2628	-----+	
29.000	18.3322	-----+	
29.500	18.4009	-----+	
30.000	18.4689	-----+	
30.500	18.5361	-----+	
31.000	18.6027	-----+	
31.500	18.6687	-----+	
32.000	18.7339	-----+	
32.500	18.7984	-----+	
33.000	18.8624	-----+	
33.500	18.9256	-----+	
34.000	18.9881	-----+	
34.500	19.0501	-----+	
35.000	19.1114	-----+	
35.500	19.1720	-----+	
36.000	19.2320	-----+	
36.500	19.2915	-----+	
37.000	19.3503	-----+	
37.500	19.4084	-----+	
38.000	19.4660	-----+	
38.500	19.5230	-----+	
39.000	19.5794	-----+	
39.500	19.6353	-----+	
40.000	19.6905	-----+	
40.500	19.7452	-----+	
41.000	19.7993	-----+	
41.500	19.8529	-----+	
42.000	19.9059	-----+	
42.500	19.9584	-----+	
43.000	20.0103	-----+	
43.500	20.0617	-----+	
44.000	20.1125	-----+	
44.500	20.1628	-----+	
45.000	20.2127	-----+	
45.500	20.2620	-----+	
46.000	20.3108	-----+	
46.500	20.3591	-----+	
47.000	20.4069	-----+	

RSR-3 (Ramey, contn.)

.OC EIX Y (5) MINIM (0.0000) MAXIM (20.0000)

WPS	SOBTIDA 5	0.0000	20.0000
.001	.0001	+	I
.500	.7648	I+	I
.000	1.3105	I→+	I
.500	1.7129	I→+	I
.000	2.0715	I→+	I
.500	2.2685	I→+	I
.000	2.4751	I→+	I
.500	2.6549	I→+	I
.000	2.8169	I→+	I
.500	2.9669	I→+	I
.000	3.1089	I→+	I
.500	3.2452	I→+	I
.000	3.3775	I→+	I
.500	3.5069	I→+	I
.000	3.6340	I→+	I
.500	3.7593	I→+	I
.000	3.8832	I→+	I
.500	4.0057	I→+	I
.000	4.1272	I→+	I
.500	4.2475	I→+	I
.000	4.3668	I→+	I
.500	4.4852	I→+	I
.000	4.6026	I→+	I
.500	4.7191	I→+	I
.000	4.8347	I→+	I
.500	4.9495	I→+	I
.000	5.0633	I→+	I
.500	5.1763	I→+	I
.000	5.2884	I→+	I
.500	5.3997	I→+	I
.000	5.5101	I→+	I
.500	5.6197	I→+	I
.000	5.7285	I→+	I
.500	5.8364	I→+	I
.000	5.9436	I→+	I
.500	6.0499	I→+	I
.000	6.1554	I→+	I
.500	6.2601	I→+	I
.000	6.3640	I→+	I
.500	6.4672	I→+	I
.000	6.5695	I→+	I
.500	6.6711	I→+	I
.000	6.7719	I→+	I
.500	6.8720	I→+	I
.000	6.9713	I→+	I
.500	7.0698	I→+	I
.000	7.1676	I→+	I
.500	7.2647	I→+	I
.000	7.3610	I→+	I
.500	7.4566	I→+	I
.000	7.5515	I→+	I
.500	7.6456	I→+	I
.000	7.7391	I→+	I
.500	7.8318	I→+	I
.000	7.9239	I→+	I
.500	8.0152	I→+	I
.000	8.1058	I→+	I
.500	8.1958	I→+	I
.000	8.2851	I→+	I
.500	8.3737	I→+	I
.000	8.4616	I→+	I
.500	8.5489	I→+	I
.000	8.6355	I→+	I
.500	8.7215	I→+	I
.000	8.8068	I→+	I
.500	8.8914	I→+	I
.000	8.9755	I→+	I
.500	9.0588	I→+	I
.000	9.1416	I→+	I
.500	9.2237	I→+	I
.000	9.3052	I→+	I
.500	9.3861	I→+	I
.000	9.4664	I→+	I
.500	9.5461	I→+	I
.000	9.6251	I→+	I
.500	9.7036	I→+	I
.000	9.7815	I→+	I
.500	9.8588	I→+	I
.000	9.9355	I→+	I
.500	10.0116	I→+	I
.000	10.0871	I→+	I

RSR-4 (Glover)

1.000	10.0871	I	-----+	I
1.500	10.1621	I	-----+	I
1.000	10.2365	I	-----+	I
1.500	10.3104	I	-----+	I
2.000	10.3837	I	-----+	I
2.500	10.4564	I	-----+	I
3.000	10.5286	I	-----+	I
3.500	10.6002	I	-----+	I
4.000	10.6713	I	-----+	I
4.500	10.7419	I	-----+	I
5.000	10.8119	I	-----+	I
5.500	10.8814	I	-----+	I
6.000	10.9504	I	-----+	I
6.500	11.0189	I	-----+	I
7.000	11.0867	I	-----+	I
7.500	11.1541	I	-----+	I
8.000	11.2210	I	-----+	I
8.500	11.2874	I	-----+	I
9.000	11.3533	I	-----+	I
9.500	11.4187	I	-----+	I
10.000	11.4836	I	-----+	I
10.500	11.5481	I	-----+	I
11.000	11.6120	I	-----+	I
11.500	11.6754	I	-----+	I
12.000	11.7384	I	-----+	I
12.500	11.8009	I	-----+	I
13.000	11.8629	I	-----+	I
13.500	11.9244	I	-----+	I
14.000	11.9855	I	-----+	I
14.500	12.0461	I	-----+	I
15.000	12.1063	I	-----+	I
15.500	12.1660	I	-----+	I
16.000	12.2252	I	-----+	I
16.500	12.2840	I	-----+	I
17.000	12.3424	I	-----+	I
17.500	12.4003	I	-----+	I
18.000	12.4578	I	-----+	I
18.500	12.5148	I	-----+	I
19.000	12.5715	I	-----+	I
19.500	12.6276	I	-----+	I
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20.500	12.7387	I	-----+	I
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21.500	12.8482	I	-----+	I
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25.500	13.2696	I	-----+	I
26.000	13.3205	I	-----+	I
26.500	13.3710	I	-----+	I
27.000	13.4212	I	-----+	I
27.500	13.4709	I	-----+	I
28.000	13.5203	I	-----+	I
28.500	13.5693	I	-----+	I
29.000	13.6180	I	-----+	I
29.500	13.6662	I	-----+	I
30.000	13.7141	I	-----+	I
30.500	13.7617	I	-----+	I
31.000	13.8089	I	-----+	I
31.500	13.8557	I	-----+	I
32.000	13.9022	I	-----+	I
32.500	13.9483	I	-----+	I
33.000	13.9940	I	-----+	I
33.500	14.0395	I	-----+	I
34.000	14.0845	I	-----+	I
34.500	14.1293	I	-----+	I
35.000	14.1737	I	-----+	I
35.500	14.2178	I	-----+	I
36.000	14.2615	I	-----+	I
36.500	14.3049	I	-----+	I
37.000	14.3480	I	-----+	I
37.500	14.3907	I	-----+	I
38.000	14.4331	I	-----+	I
38.500	14.4752	I	-----+	I
39.000	14.5170	I	-----+	I
39.500	14.5585	I	-----+	I
40.000	14.5996	I	-----+	I

RSR-5 (Glover, contin.)

LOC FIX Y (5) MINIM (0.0000) MAXIM (20.0000)

MPS	SORTIDA 5	0.0000	20.0000
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1.000	2.7160	I	I
1.500	3.1593	I	I
2.000	3.5804	I	I
2.500	3.9899	I	I
3.000	4.3892	I	I
3.500	4.7785	I	I
4.000	5.1581	I	I
4.500	5.5283	I	I
5.000	5.8892	I	I
5.500	6.2411	I	I
6.000	6.5842	I	I
6.500	6.9188	I	I
7.000	7.2450	I	I
7.500	7.5631	I	I
8.000	7.8733	I	I
8.500	8.1757	I	I
9.000	8.4706	I	I
9.500	8.7581	I	I
10.000	9.0385	I	I
10.500	9.3118	I	I
1.000	9.5784	I	I
1.500	9.8383	I	I
2.000	10.0917	I	I
2.500	10.3388	I	I
3.000	10.5797	I	I
3.500	10.8146	I	I
4.000	11.0437	I	I
4.500	11.2671	I	I
5.000	11.4849	I	I
5.500	11.6972	I	I
6.000	11.9043	I	I
6.500	12.1062	I	I
7.000	12.3030	I	I
7.500	12.4950	I	I
8.000	12.6821	I	I
8.500	12.8646	I	I
9.000	13.0426	I	I
9.500	13.2161	I	I
20.000	13.3853	I	I
20.500	13.5502	I	I
21.000	13.7111	I	I
21.500	13.8679	I	I
22.000	14.0208	I	I
22.500	14.1699	I	I
23.000	14.3153	I	I
23.500	14.4571	I	I
24.000	14.5953	I	I
24.500	14.7301	I	I
25.000	14.8615	I	I
25.500	14.9897	I	I
26.000	15.1146	I	I
26.500	15.2365	I	I
27.000	15.3553	I	I
27.500	15.4711	I	I
28.000	15.5840	I	I
28.500	15.6942	I	I
29.000	15.8015	I	I
29.500	15.9062	I	I
30.000	16.0083	I	I
30.500	16.1078	I	I
31.000	16.2049	I	I
31.500	16.2995	I	I
32.000	16.3918	I	I
32.500	16.4818	I	I
33.000	16.5694	I	I
33.500	16.6549	I	I
34.000	16.7383	I	I
34.500	16.8195	I	I
35.000	16.8988	I	I
35.500	16.9761	I	I
36.000	17.0514	I	I
36.500	17.1249	I	I
37.000	17.1965	I	I
37.500	17.2664	I	I
38.000	17.3345	I	I
38.500	17.4009	I	I
39.000	17.4656	I	I
39.500	17.5287	I	I
40.000	17.5903	I	I

RSR-6 (Calović)

LOC FIX Y (5) MINIM (0.0000) MAXIM (20.0000)

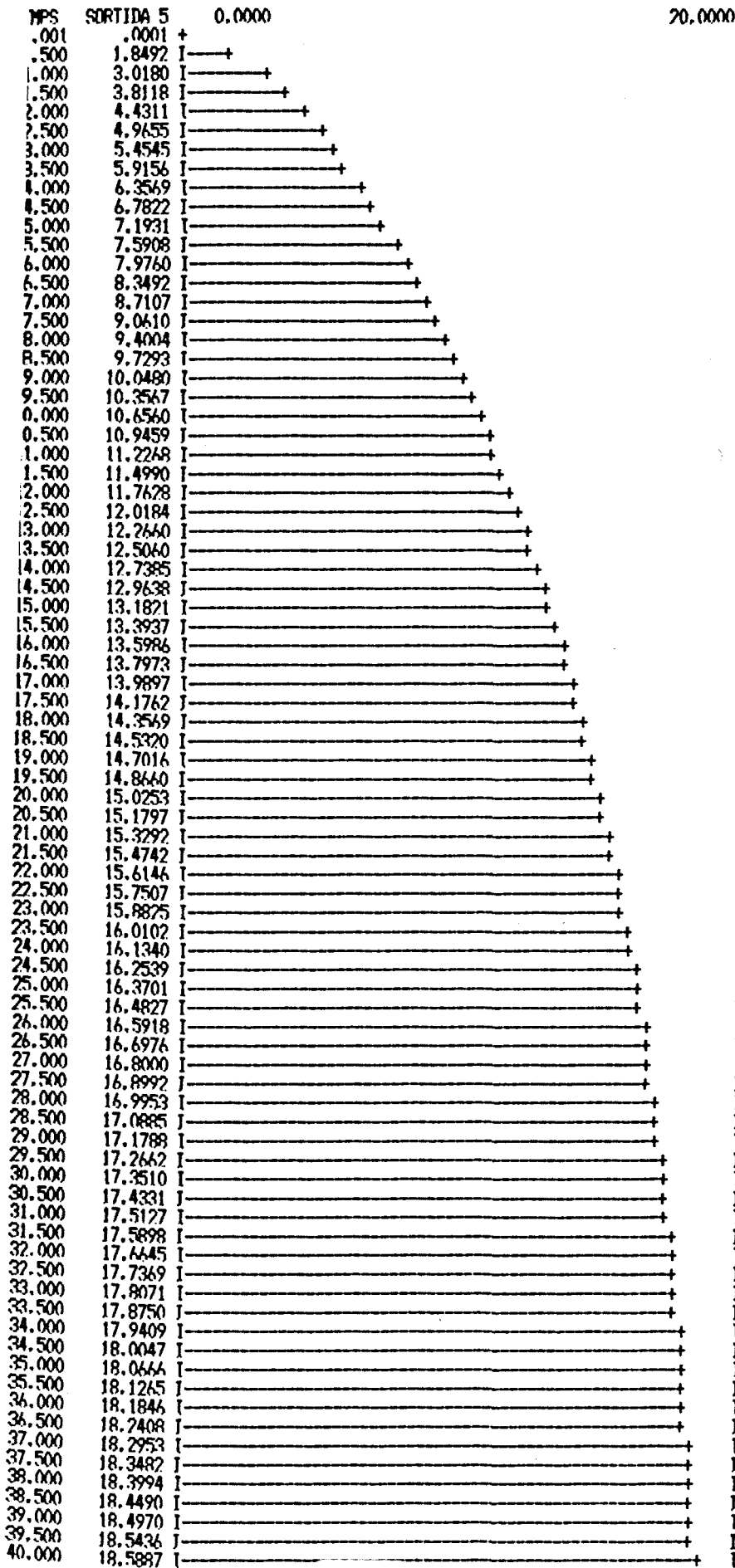
MPS	SORTIDA 5	0.0000	20.0000
.001	.0001	+	I
.500	1.6625	I-----+	I
1.000	2.4848	I-----+	I
1.500	2.9181	I-----+	I
2.000	3.2119	I-----+	I
2.500	3.4545	I-----+	I
3.000	3.6773	I-----+	I
3.500	3.8912	I-----+	I
4.000	4.1004	I-----+	I
4.500	4.3060	I-----+	I
5.000	4.5088	I-----+	I
5.500	4.7088	I-----+	I
6.000	4.9062	I-----+	I
6.500	5.1011	I-----+	I
7.000	5.2934	I-----+	I
7.500	5.4833	I-----+	I
8.000	5.6707	I-----+	I
8.500	5.8556	I-----+	I
9.000	6.0382	I-----+	I
9.500	6.2185	I-----+	I
10.000	6.3964	I-----+	I
10.500	6.5720	I-----+	I
11.000	6.7454	I-----+	I
11.500	6.9165	I-----+	I
12.000	7.0854	I-----+	I
12.500	7.2521	I-----+	I
13.000	7.4167	I-----+	I
13.500	7.5791	I-----+	I
14.000	7.7394	I-----+	I
14.500	7.8977	I-----+	I
15.000	8.0540	I-----+	I
15.500	8.2082	I-----+	I
16.000	8.3604	I-----+	I
16.500	8.5107	I-----+	I
17.000	8.6590	I-----+	I
17.500	8.8054	I-----+	I
18.000	8.9499	I-----+	I
18.500	9.0925	I-----+	I
19.000	9.2334	I-----+	I
19.500	9.3723	I-----+	I
20.000	9.5095	I-----+	I
20.500	9.6450	I-----+	I
21.000	9.7786	I-----+	I
21.500	9.9106	I-----+	I
22.000	10.0408	I-----+	I
22.500	10.1694	I-----+	I
23.000	10.2963	I-----+	I
23.500	10.4216	I-----+	I
24.000	10.5452	I-----+	I
24.500	10.6673	I-----+	I
25.000	10.7878	I-----+	I
25.500	10.9067	I-----+	I
26.000	11.0241	I-----+	I
26.500	11.1399	I-----+	I
27.000	11.2543	I-----+	I
27.500	11.3672	I-----+	I
28.000	11.4787	I-----+	I
28.500	11.5887	I-----+	I
29.000	11.6973	I-----+	I
29.500	11.8044	I-----+	I
30.000	11.9102	I-----+	I
30.500	12.0147	I-----+	I
31.000	12.1178	I-----+	I
31.500	12.2195	I-----+	I
32.000	12.3199	I-----+	I
32.500	12.4191	I-----+	I
33.000	12.5170	I-----+	I
33.500	12.6136	I-----+	I
34.000	12.7089	I-----+	I
34.500	12.8030	I-----+	I
35.000	12.8959	I-----+	I
35.500	12.9876	I-----+	I
36.000	13.0782	I-----+	I
36.500	13.1675	I-----+	I
37.000	13.2557	I-----+	I
37.500	13.3428	I-----+	I
38.000	13.4287	I-----+	I
38.500	13.5136	I-----+	I
39.000	13.5973	I-----+	I
39.500	13.6799	I-----+	I
40.000	13.7615	I-----+	I

RSR-7 (IEEE, valores típicos)

13.500	13.8421	I	+
13.000	13.9216	I	+
13.500	14.0000	I	+
14.000	14.0775	I	+
14.500	14.1539	I	+
15.000	14.2294	I	+
15.500	14.3039	I	+
16.000	14.3774	I	+
16.500	14.4500	I	+
17.000	14.5216	I	+
17.500	14.5924	I	+
18.000	14.6622	I	+
18.500	14.7311	I	+
19.000	14.7991	I	+
19.500	14.8662	I	+
20.000	14.9325	I	+
20.500	14.9979	I	+
21.000	15.0625	I	+
21.500	15.1262	I	+
22.000	15.1892	I	+
22.500	15.2513	I	+
23.000	15.3126	I	+
23.500	15.3731	I	+
24.000	15.4328	I	+
24.500	15.4918	I	+
25.000	15.5499	I	+
25.500	15.6074	I	+
26.000	15.6641	I	+
26.500	15.7201	I	+
27.000	15.7753	I	+
27.500	15.8299	I	+
28.000	15.8837	I	+
28.500	15.9368	I	+
29.000	15.9893	I	+
29.500	16.0410	I	+
30.000	16.0921	I	+
30.500	16.1425	I	+
31.000	16.1923	I	+
31.500	16.2415	I	+
32.000	16.2900	I	+
32.500	16.3378	I	+
33.000	16.3851	I	+
33.500	16.4318	I	+
34.000	16.4778	I	+
34.500	16.5233	I	+
35.000	16.5681	I	+
35.500	16.6124	I	+
36.000	16.6561	I	+
36.500	16.6992	I	+
37.000	16.7417	I	+
37.500	16.7837	I	+
38.000	16.8251	I	+
38.500	16.8661	I	+
39.000	16.9065	I	+
39.500	16.9463	I	+
40.000	16.9857	I	+
40.500	17.0245	I	+
41.000	17.0629	I	+
41.500	17.1008	I	+
42.000	17.1381	I	+
42.500	17.1750	I	+
43.000	17.2114	I	+
43.500	17.2473	I	+
44.000	17.2828	I	+
44.500	17.3178	I	+
45.000	17.3524	I	+
45.500	17.3865	I	+
46.000	17.4201	I	+
46.500	17.4534	I	+
47.000	17.4862	I	+

RSR-8 (IEEE, contin.)

LOC FIX Y (5) MINIM (0.0000) MAXIM (20.0000)



RSR-9 (IEEE, valores de
dinámica más rápida)

LOC. FIX Y (5) MINIM (0.0000) MAXIM (20.0000)

MPS	SORTIDA 5	0.0000	20.0000
.001	.0001	+	I
.500	1.3921	I→+	I
.000	1.7939	I→+	I
.500	1.9391	I→+	I
1.000	2.0177	I→+	I
1.500	2.0789	I→+	I
1.000	2.1355	I→+	I
1.500	2.1907	I→+	I
1.000	2.2455	I→+	I
1.500	2.3000	I→+	I
1.000	2.3543	I→+	I
1.500	2.4085	I→+	I
1.000	2.4625	I→+	I
1.500	2.5163	I→+	I
7.000	2.5700	I→+	I
7.500	2.6235	I→+	I
8.000	2.6768	I→+	I
3.500	2.7300	I→+	I
9.000	2.7830	I→+	I
9.500	2.8359	I→+	I
0.000	2.8885	I→+	I
0.500	2.9411	I→+	I
1.000	2.9934	I→+	I
1.500	3.0456	I→+	I
2.000	3.0977	I→+	I
2.500	3.1495	I→+	I
3.000	3.2013	I→+	I
3.500	3.2528	I→+	I
4.000	3.3042	I→+	I
4.500	3.3555	I→+	I
15.000	3.4065	I→+	I
5.500	3.4575	I→+	I
16.000	3.5083	I→+	I
16.500	3.5589	I→+	I
17.000	3.6093	I→+	I
17.500	3.6596	I→+	I
18.000	3.7098	I→+	I
18.500	3.7598	I→+	I
19.000	3.8096	I→+	I
19.500	3.8593	I→+	I
20.000	3.9089	I→+	I
20.500	3.9583	I→+	I
21.000	4.0075	I→+	I
21.500	4.0566	I→+	I
22.000	4.1055	I→+	I
22.500	4.1543	I→+	I
23.000	4.2029	I→+	I
23.500	4.2514	I→+	I
24.000	4.2998	I→+	I
24.500	4.3479	I→+	I
25.000	4.3960	I→+	I
25.500	4.4439	I→+	I
26.000	4.4916	I→+	I
26.500	4.5392	I→+	I
27.000	4.5867	I→+	I
27.500	4.6340	I→+	I
28.000	4.6811	I→+	I
28.500	4.7282	I→+	I
29.000	4.7750	I→+	I
29.500	4.8218	I→+	I
30.000	4.8684	I→+	I
30.500	4.9148	I→+	I
31.000	4.9611	I→+	I
31.500	5.0073	I→+	I
32.000	5.0533	I→+	I
32.500	5.0991	I→+	I
33.000	5.1449	I→+	I
33.500	5.1905	I→+	I
34.000	5.2359	I→+	I
34.500	5.2812	I→+	I
35.000	5.3264	I→+	I
35.500	5.3715	I→+	I
36.000	5.4164	I→+	I
36.500	5.4611	I→+	I
37.000	5.5057	I→+	I
37.500	5.5502	I→+	I
38.000	5.5946	I→+	I
38.500	5.6388	I→+	I
39.000	5.6829	I→+	I
39.500	5.7268	I→+	I
40.000	5.7706	I→+	I

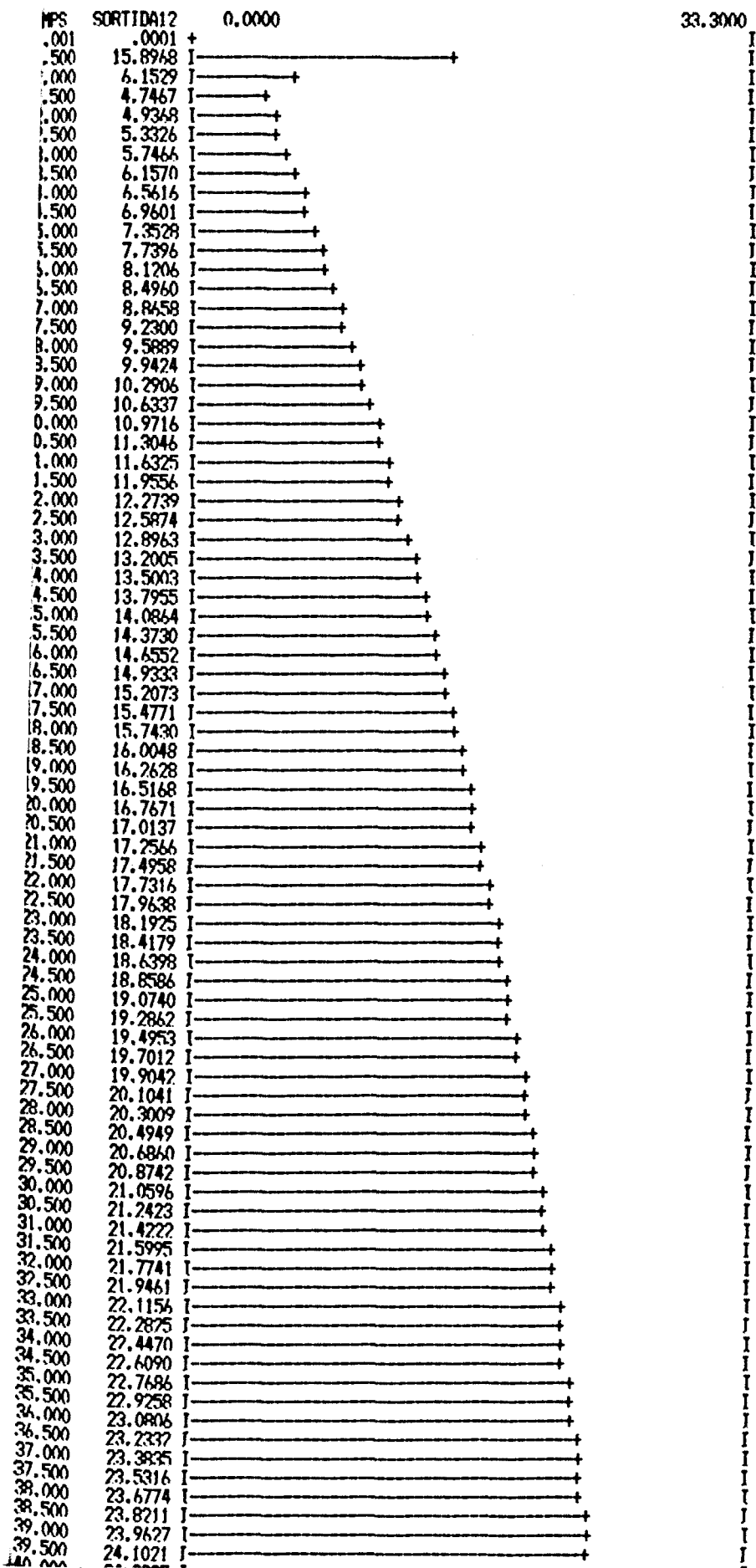
RSR-10 (Gurney)

LOC EIX Y (5) MINIM (0.0000) MAXIM (21.7390)

MPS	SORTIDA 5	0.0000	21.7390
.001	.0001	+	I
.500	1.7238	I → +	I
1.000	2.5221	I → +	I
1.500	2.9160	I → +	I
2.000	3.1330	I → +	I
2.500	3.2727	I → +	I
3.000	3.3784	I → +	I
3.500	3.4690	I → +	I
4.000	3.5528	I → +	I
4.500	3.6335	I → +	I
5.000	3.7126	I → +	I
5.500	3.7909	I → +	I
6.000	3.8686	I → +	I
6.500	3.9458	I → +	I
7.000	4.0227	I → +	I
7.500	4.0992	I → +	I
8.000	4.1754	I → +	I
8.500	4.2512	I → +	I
9.000	4.3268	I → +	I
9.500	4.4019	I → +	I
10.000	4.4768	I → +	I
10.500	4.5514	I → +	I
11.000	4.6256	I → +	I
11.500	4.6995	I → +	I
12.000	4.7731	I → +	I
12.500	4.8463	I → +	I
13.000	4.9193	I → +	I
13.500	4.9919	I → +	I
14.000	5.0642	I → +	I
14.500	5.1362	I → +	I
15.000	5.2079	I → +	I
15.500	5.2793	I → +	I
16.000	5.3504	I → +	I
16.500	5.4212	I → +	I
17.000	5.4916	I → +	I
17.500	5.5618	I → +	I
18.000	5.6316	I → +	I
18.500	5.7012	I → +	I
19.000	5.7704	I → +	I
19.500	5.8394	I → +	I
20.000	5.9081	I → +	I
20.500	5.9764	I → +	I
21.000	6.0445	I → +	I
21.500	6.1123	I → +	I
22.000	6.1797	I → +	I
22.500	6.2469	I → +	I
23.000	6.3138	I → +	I
23.500	6.3804	I → +	I
24.000	6.4468	I → +	I
24.500	6.5128	I → +	I
25.000	6.5786	I → +	I
25.500	6.6440	I → +	I
26.000	6.7092	I → +	I
26.500	6.7741	I → +	I
27.000	6.8387	I → +	I
27.500	6.9031	I → +	I
28.000	6.9671	I → +	I
28.500	7.0309	I → +	I
29.000	7.0944	I → +	I
29.500	7.1577	I → +	I
30.000	7.2206	I → +	I
30.500	7.2833	I → +	I
31.000	7.3458	I → +	I
31.500	7.4079	I → +	I
32.000	7.4698	I → +	I
32.500	7.5314	I → +	I
33.000	7.5928	I → +	I
33.500	7.6539	I → +	I
34.000	7.7147	I → +	I
34.500	7.7752	I → +	I
35.000	7.8355	I → +	I
35.500	7.8956	I → +	I
36.000	7.9554	I → +	I
36.500	8.0149	I → +	I
37.000	8.0741	I → +	I
37.500	8.1331	I → +	I
38.000	8.1919	I → +	I
38.500	8.2504	I → +	I
39.000	8.3086	I → +	I
39.500	8.3666	I → +	I
40.000	8.4244	I → +	I

RSR-12 (Bryce)

LOC EIX Y (12) MINIM (0.0000) MAXIM (33.3000)

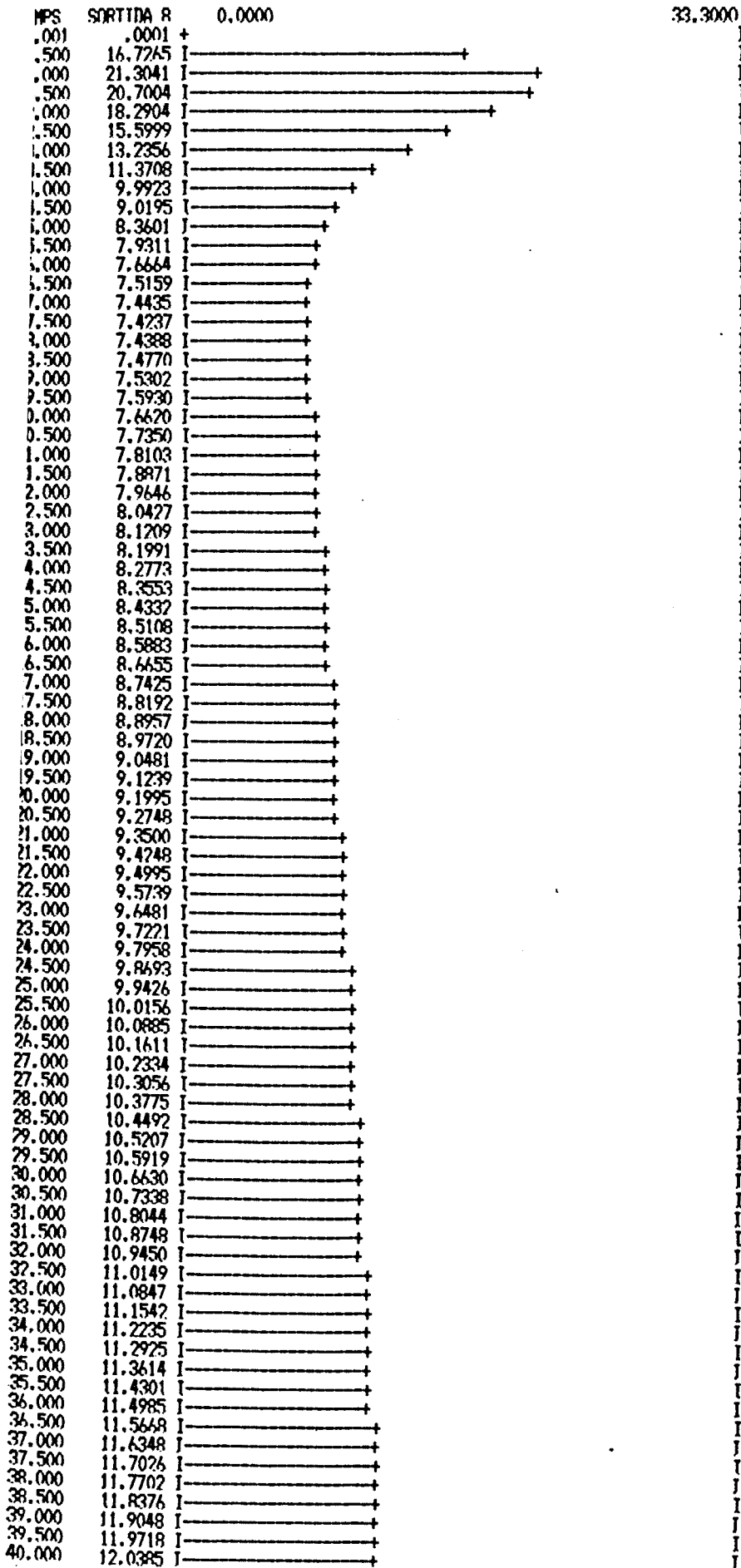


RSR-14 (Bryce, electrónico)

.000	24.2395	I	-----+	I
.500	24.3748	I	-----+	I
1.000	24.5081	I	-----+	I
.500	24.6394	I	-----+	I
1.000	24.7688	I	-----+	I
.500	24.8962	I	-----+	I
1.000	25.0218	I	-----+	I
.500	25.1454	I	-----+	I
1.000	25.2673	I	-----+	I
.500	25.3873	I	-----+	I
1.000	25.5055	I	-----+	I
.500	25.6220	I	-----+	I
1.000	25.7367	I	-----+	I
.500	25.8497	I	-----+	I
1.000	25.9611	I	-----+	I
.500	26.0708	I	-----+	I
1.000	26.1788	I	-----+	I
.500	26.2852	I	-----+	I
1.000	26.3902	I	-----+	I
.500	26.4934	I	-----+	I
1.000	26.5951	I	-----+	I
.500	26.6953	I	-----+	I
1.000	26.7941	I	-----+	I
.500	26.8914	I	-----+	I
1.000	26.9873	I	-----+	I
.500	27.0816	I	-----+	I
1.000	27.1747	I	-----+	I
.500	27.2663	I	-----+	I
1.000	27.3565	I	-----+	I
.500	27.4454	I	-----+	I
1.000	27.5330	I	-----+	I
.500	27.6193	I	-----+	I
1.000	27.7043	I	-----+	I
.500	27.7880	I	-----+	I
1.000	27.8705	I	-----+	I
.500	27.9518	I	-----+	I
1.000	28.0318	I	-----+	I
.500	28.1107	I	-----+	I
1.000	28.1884	I	-----+	I
.500	28.2649	I	-----+	I
1.000	28.3403	I	-----+	I
.500	28.4145	I	-----+	I
1.000	28.4877	I	-----+	I
.500	28.5598	I	-----+	I
1.000	28.6308	I	-----+	I
.500	28.7007	I	-----+	I
1.000	28.7696	I	-----+	I
.500	28.8375	I	-----+	I
1.000	28.9043	I	-----+	I
.500	28.9702	I	-----+	I
1.000	29.0351	I	-----+	I
.500	29.0990	I	-----+	I
1.000	29.1620	I	-----+	I
.500	29.2240	I	-----+	I
1.000	29.2851	I	-----+	I
.500	29.3453	I	-----+	I
1.000	29.4046	I	-----+	I
.500	29.4630	I	-----+	I
1.000	29.5206	I	-----+	I
.500	29.5773	I	-----+	I
1.000	29.6331	I	-----+	I
.500	29.6881	I	-----+	I
1.000	29.7423	I	-----+	I
.500	29.7957	I	-----+	I
1.000	29.8483	I	-----+	I
.500	29.9001	I	-----+	I
1.000	29.9511	I	-----+	I
.500	30.0014	I	-----+	I
1.000	30.0509	I	-----+	I
.500	30.0997	I	-----+	I
1.000	30.1478	I	-----+	I
.500	30.1951	I	-----+	I
1.000	30.2418	I	-----+	I
.500	30.2877	I	-----+	I
1.000	30.3330	I	-----+	I
.500	30.3776	I	-----+	I
1.000	30.4215	I	-----+	I
.500	30.4648	I	-----+	I
1.000	30.5074	I	-----+	I
.500	30.5494	I	-----+	I
1.000	30.5908	I	-----+	I

RSR-15 (Bryce, electron.
-continuación)

LOC FIX Y (8) MINIM (0.0000) MAXIM (33.3000)



RSR-16 (Bryce, mecánico)

LOC ETX Y (5) MINIM (0.0000) MAXIM (22.2770)

MPS	SORTIDA 5	0.0000	22.2770
0.001	0.0001	+	I
0.500	1.1474	I→+	I
1.000	1.6777	I→+	I
1.500	1.9606	I→+	I
2.000	2.1384	I→+	I
2.500	2.2773	I→+	I
3.000	2.3877	I→+	I
3.500	2.4951	I→+	I
4.000	2.5988	I→+	I
4.500	2.7007	I→+	I
5.000	2.8016	I→+	I
5.500	2.9018	I→+	I
6.000	3.0013	I→+	I
6.500	3.1003	I→+	I
7.000	3.1987	I→+	I
7.500	3.2967	I→+	I
8.000	3.3941	I→+	I
8.500	3.4910	I→+	I
9.000	3.5875	I→+	I
9.500	3.6834	I→+	I
10.000	3.7788	I→+	I
10.500	3.8738	I→+	I
11.000	3.9682	I→+	I
11.500	4.0622	I→+	I
12.000	4.1557	I→+	I
12.500	4.2487	I→+	I
13.000	4.3412	I→+	I
13.500	4.4333	I→+	I
14.000	4.5249	I→+	I
14.500	4.6160	I→+	I
15.000	4.7066	I→+	I
15.500	4.7968	I→+	I
16.000	4.8865	I→+	I
16.500	4.9757	I→+	I
17.000	5.0645	I→+	I
17.500	5.1529	I→+	I
18.000	5.2407	I→+	I
18.500	5.3281	I→+	I
19.000	5.4151	I→+	I
19.500	5.5016	I→+	I
20.000	5.5877	I→+	I
20.500	5.6734	I→+	I
21.000	5.7586	I→+	I
21.500	5.8433	I→+	I
22.000	5.9276	I→+	I
22.500	6.0115	I→+	I
23.000	6.0950	I→+	I
23.500	6.1780	I→+	I
24.000	6.2606	I→+	I
24.500	6.3428	I→+	I
25.000	6.4245	I→+	I
25.500	6.5058	I→+	I
26.000	6.5867	I→+	I
26.500	6.6672	I→+	I
27.000	6.7473	I→+	I
27.500	6.8270	I→+	I
28.000	6.9062	I→+	I
28.500	6.9851	I→+	I
29.000	7.0635	I→+	I
29.500	7.1416	I→+	I
30.000	7.2192	I→+	I
30.500	7.2964	I→+	I
31.000	7.3733	I→+	I
31.500	7.4497	I→+	I
32.000	7.5258	I→+	I
32.500	7.6014	I→+	I
33.000	7.6767	I→+	I
33.500	7.7516	I→+	I
34.000	7.8261	I→+	I
34.500	7.9002	I→+	I
35.000	7.9739	I→+	I
35.500	8.0473	I→+	I
36.000	8.1202	I→+	I
36.500	8.1928	I→+	I
37.000	8.2650	I→+	I
37.500	8.3369	I→+	I
38.000	8.4084	I→+	I
38.500	8.4795	I→+	I
39.000	8.5502	I→+	I
39.500	8.6206	I→+	I
40.000	8.6904	I→+	I

RSR-18 (Sankanara...)

0.000	8.6906	I	→
0.500	8.7603	I	→
1.000	8.8296	I	→
1.500	8.8986	I	→
2.000	8.9671	I	→
2.500	9.0354	I	→
3.000	9.1033	I	→
3.500	9.1708	I	→
4.000	9.2380	I	→
4.500	9.3048	I	→
5.000	9.3713	I	→
5.500	9.4375	I	→
6.000	9.5033	I	→
6.500	9.5688	I	→
7.000	9.6339	I	→
7.500	9.6987	I	→
8.000	9.7632	I	→
8.500	9.8273	I	→
9.000	9.8911	I	→
9.500	9.9544	I	→
10.000	10.0178	I	→
10.500	10.0806	I	→
11.000	10.1431	I	→
11.500	10.2053	I	→
12.000	10.2671	I	→
12.500	10.3287	I	→
13.000	10.3899	I	→
13.500	10.4508	I	→
14.000	10.5114	I	→
14.500	10.5717	I	→
15.000	10.6317	I	→
15.500	10.6914	I	→
16.000	10.7507	I	→
16.500	10.8098	I	→
17.000	10.8685	I	→
17.500	10.9270	I	→
18.000	10.9851	I	→
18.500	11.0430	I	→
19.000	11.1005	I	→
19.500	11.1578	I	→
20.000	11.2147	I	→
20.500	11.2714	I	→
21.000	11.3278	I	→
21.500	11.3839	I	→
22.000	11.4396	I	→
22.500	11.4952	I	→
23.000	11.5504	I	→
23.500	11.6053	I	→
24.000	11.6600	I	→
24.500	11.7143	I	→
25.000	11.7684	I	→
25.500	11.8223	I	→
26.000	11.8758	I	→
26.500	11.9291	I	→
27.000	11.9820	I	→
27.500	12.0348	I	→
28.000	12.0872	I	→
28.500	12.1394	I	→
29.000	12.1913	I	→
29.500	12.2429	I	→
30.000	12.2943	I	→
30.500	12.3454	I	→
31.000	12.3962	I	→
31.500	12.4468	I	→
32.000	12.4971	I	→
32.500	12.5472	I	→
33.000	12.5970	I	→
33.500	12.6466	I	→
34.000	12.6959	I	→
34.500	12.7449	I	→
35.000	12.7937	I	→

RSR-19 (Sanka...,contin.)

TEMPS	SORTIDA12	SORTIDA24	SORTIDA38	SORTIDA44
.00	.0001	.0001	.0001	.0001
.25	-7.4245	-18.3751	-4.3502	-30.1496
.50	-14.8904	-14.2859	-5.4032	-34.5794
.75	-15.0555	-3.4437	-5.2573	-23.7763
1.00	-8.5344	6.5379	-4.3432	-6.3396
1.25	2.1756	14.1801	-2.9360	13.4197
1.50	14.7648	19.7298	-1.2218	33.2728
1.75	27.6151	23.7834	.6741	52.0725
2.00	39.7627	26.8520	2.6670	69.2816
2.25	50.7231	29.2926	4.7002	84.7159
2.50	60.3199	31.3341	6.7363	98.3901
2.75	68.5564	33.1167	8.7504	110.4234
3.00	75.5307	34.7247	10.7267	120.9870
3.25	81.3817	36.2083	12.6551	130.2450
3.50	86.2594	37.5972	14.5297	138.3862
3.75	90.3072	38.9095	16.3470	145.5635
4.00	93.6568	40.1563	18.1056	151.9187
4.25	96.4277	41.3451	19.8052	157.5729
4.50	98.7034	42.4809	21.4462	162.6304
4.75	100.5820	43.5672	23.0297	167.1788
5.00	102.1285	44.6070	24.5569	171.2923
5.25	103.4010	45.6026	26.0294	175.0330
5.50	104.4478	46.5563	27.4489	178.4529
5.75	105.3089	47.4698	28.8171	181.5957
6.00	106.0168	48.3449	30.1356	184.4972
6.25	106.5986	49.1834	31.4061	187.1880
6.50	107.0771	49.9868	32.6304	189.6942
6.75	107.4706	50.7564	33.8100	192.0369
7.00	107.7942	51.4939	34.9445	194.2345
7.25	108.0601	52.2005	36.0416	196.3021
7.50	108.2789	52.8775	37.0967	198.2530
7.75	108.4586	53.5262	38.1132	200.0979
8.00	108.6063	54.1477	39.0976	201.8465
8.25	108.7276	54.7431	40.0362	203.5069
8.50	108.8273	55.3137	40.9454	205.0863
8.75	108.9094	55.8605	41.8213	206.5911
9.00	108.9767	56.3843	42.6651	208.0260
9.25	109.0373	56.8861	43.4782	209.3965
9.50	109.0780	57.3671	44.2615	210.7065
9.75	109.1154	57.8278	45.0162	211.9593
10.00	109.1461	58.2692	45.7434	213.1585
10.25	109.1714	58.6922	46.4439	214.3074
10.50	109.1923	59.0975	47.1188	215.4085
10.75	109.2094	59.4858	47.7691	216.4641
11.00	109.2234	59.8579	48.3955	217.4767
11.25	109.2351	60.2144	48.9991	218.4485
11.50	109.2446	60.5560	49.5807	219.3812
11.75	109.2525	60.8833	50.1409	220.2767
12.00	109.2590	61.1968	50.6807	221.1364
12.25	109.2641	61.4973	51.2008	221.9620
12.50	109.2685	61.7852	51.7018	222.7554
12.75	109.2722	62.0609	52.1845	223.5175
13.00	109.2749	62.3251	52.6497	224.2496
13.25	109.2774	62.5784	53.0977	224.9534
13.50	109.2792	62.8210	53.5294	225.6295
13.75	109.2809	63.0535	53.9454	226.2797
14.00	109.2824	63.2762	54.3461	226.9046
14.25	109.2834	63.4897	54.7322	227.5053
14.50	109.2845	63.6942	55.1042	228.0828
14.75	109.2851	63.8901	55.4626	228.6377
15.00	109.2856	64.0778	55.8078	229.1711
15.25	109.2858	64.2576	56.1405	229.6838
15.50	109.2863	64.4299	56.4610	230.1771
15.75	109.2869	64.5950	56.7697	230.6515
16.00	109.2874	64.7532	57.0672	231.1078
16.25	109.2877	64.9048	57.3539	231.5463
16.50	109.2877	65.0501	57.6300	231.9677
16.75	109.2877	65.1893	57.8960	232.3729
17.00	109.2877	65.3226	58.1524	232.7626
17.25	109.2877	65.4503	58.3993	233.1372
17.50	109.2877	65.5727	58.6372	233.4975
17.75	109.2877	65.6900	58.8664	233.8441
18.00	109.2877	65.8024	59.0873	234.1772
18.25	109.2877	65.9101	59.3000	234.4977
18.50	109.2877	66.0132	59.5051	234.8059
18.75	109.2877	66.1121	59.7026	235.1023

19.25	109.2877	66.2977	60.0761	235.6614
19.50	109.2877	66.3845	60.2528	235.9249
19.75	109.2877	66.4678	60.4230	236.1784
20.00	109.2877	66.5476	60.5870	236.4222
20.00	109.2877	66.5476	60.5870	236.4222
20.25	109.2877	66.6241	60.7449	236.6566
20.50	109.2877	66.6973	60.8971	236.8820
20.75	109.2877	66.7675	61.0437	237.0988
21.00	109.2877	66.8349	61.1850	237.3075
21.25	109.2877	66.8992	61.3211	237.5079
21.50	109.2877	66.9610	61.4522	237.7007
21.75	109.2877	67.0202	61.5786	237.8863
22.00	109.2877	67.0769	61.7002	238.0647
22.25	109.2877	67.1312	61.8175	238.2363
22.50	109.2877	67.1832	61.9305	238.4013
22.75	109.2877	67.2332	62.0393	238.5601
23.00	109.2877	67.2809	62.1442	238.7127
23.25	109.2877	67.3267	62.2452	238.8595
23.50	109.2877	67.3705	62.3426	239.0007
23.75	109.2877	67.4126	62.4364	239.1366
24.00	109.2877	67.4529	62.5268	239.2673
24.25	109.2877	67.4915	62.6138	239.3929
24.50	109.2877	67.5284	62.6977	239.5138
24.75	109.2877	67.5639	62.7785	239.6299
25.00	109.2877	67.5978	62.8563	239.7417
25.25	109.2877	67.6304	62.9313	239.8492
25.50	109.2877	67.6615	63.0036	239.9527
25.75	109.2877	67.6913	63.0732	240.0522
26.00	109.2877	67.7200	63.1403	240.1479
26.25	109.2877	67.7473	63.2049	240.2398
26.50	109.2877	67.7736	63.2677	240.3284
26.75	109.2877	67.7987	63.3273	240.4136
27.00	109.2877	67.8229	63.3850	240.4955
27.25	109.2877	67.8459	63.4407	240.5742
27.50	109.2877	67.8681	63.4943	240.6499
27.75	109.2877	67.8893	63.5459	240.7228
28.00	109.2877	67.9096	63.5958	240.7930
28.25	109.2877	67.9291	63.6438	240.8605
28.50	109.2877	67.9477	63.6900	240.9253
28.75	109.2877	67.9656	63.7345	240.9877
29.00	109.2877	67.9827	63.7775	241.0478
29.25	109.2877	67.9991	63.8188	241.1055
29.50	109.2877	68.0148	63.8586	241.1609
29.75	109.2877	68.0299	63.8969	241.2144
30.00	109.2877	68.0444	63.9339	241.2659
30.25	109.2877	68.0582	63.9695	241.3152
30.50	109.2877	68.0714	64.0038	241.3628
30.75	109.2877	68.0841	64.0369	241.4086
31.00	109.2877	68.0963	64.0687	241.4526
31.25	109.2877	68.1079	64.0994	241.4949
31.50	109.2877	68.1191	64.1290	241.5357
31.75	109.2877	68.1297	64.1575	241.5747
32.00	109.2877	68.1399	64.1849	241.6124
32.25	109.2877	68.1498	64.2114	241.6488
32.50	109.2877	68.1592	64.2369	241.6838
32.75	109.2877	68.1683	64.2614	241.7173
33.00	109.2877	68.1769	64.2851	241.7496
33.25	109.2877	68.1852	64.3079	241.7807
33.50	109.2877	68.1932	64.3298	241.8106
33.75	109.2877	68.2008	64.3510	241.8393
34.00	109.2877	68.2080	64.3713	241.8669
34.25	109.2877	68.2150	64.3910	241.8925
34.50	109.2877	68.2216	64.4099	241.9191
34.75	109.2877	68.2280	64.4281	241.9437
35.00	109.2877	68.2342	64.4457	241.9675
35.25	109.2877	68.2401	64.4626	241.9902
35.50	109.2877	68.2458	64.4789	242.0122
35.75	109.2877	68.2512	64.4946	242.0333
36.00	109.2877	68.2564	64.5097	242.0537
36.25	109.2877	68.2613	64.5243	242.0732
36.50	109.2877	68.2660	64.5383	242.0919
36.75	109.2877	68.2706	64.5518	242.1099
37.00	109.2877	68.2750	64.5648	242.1273
37.25	109.2877	68.2791	64.5773	242.1441
37.50	109.2877	68.2832	64.5895	242.1602
37.75	109.2877	68.2870	64.6011	242.1757

RS - 1 (bis)

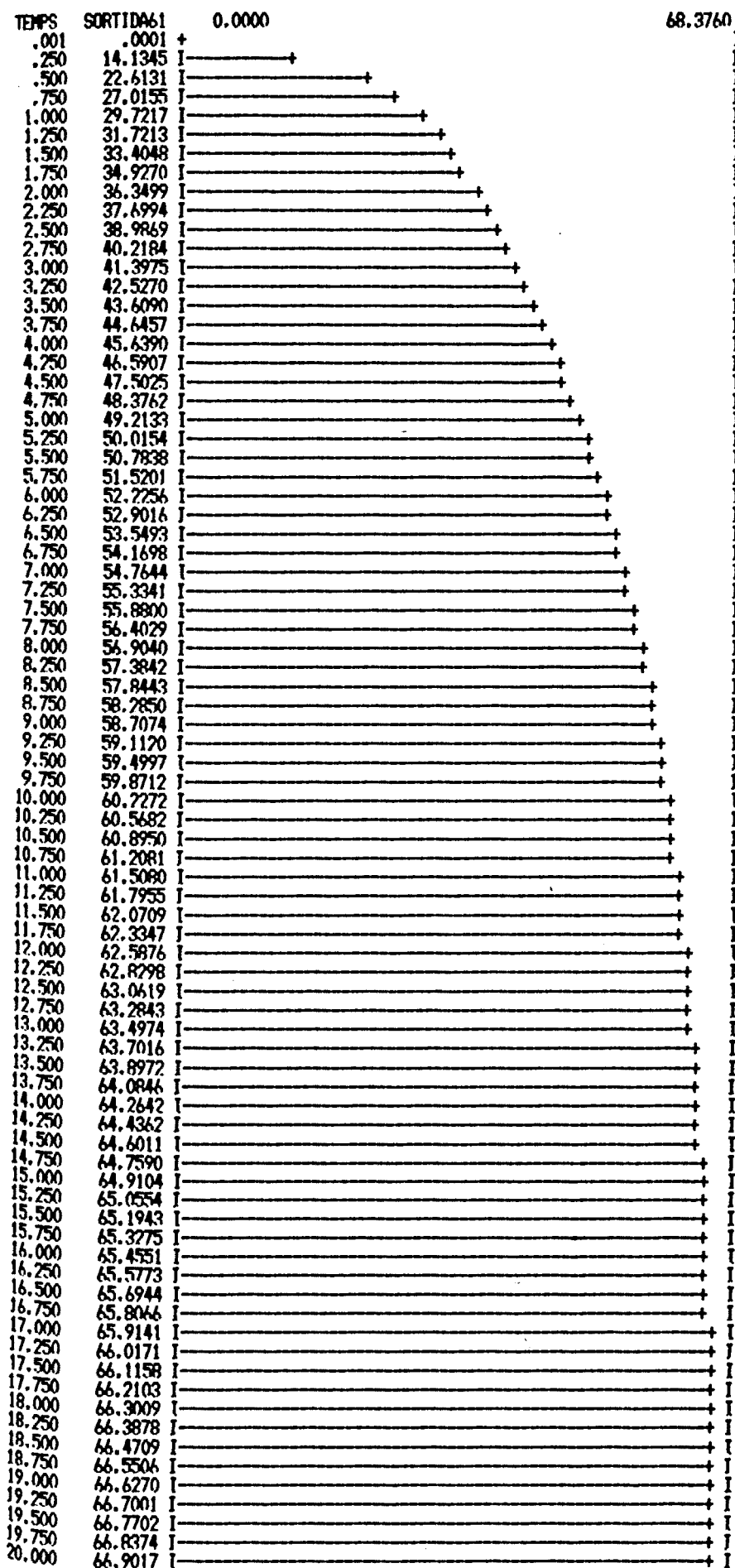
INICIO ETX Y (60) MINIM (0.0000) MAXIM (109.2900)

TEMPS	SORTIDA60	0.0000	109.2900
.001	.0001	+	I
.750	5.2573	I+	I
.500	16.2518	I-----+	I
.750	28.8248	I-----+	I
1.000	41.0332	I-----+	I
1.250	52.0611	I-----+	I
1.500	61.6523	I-----+	I
1.750	69.8152	I-----+	I
2.000	76.6730	I-----+	I
2.250	82.3687	I-----+	I
2.500	87.1286	I-----+	I
2.750	91.0470	I-----+	I
3.000	94.2798	I-----+	I
3.250	96.9436	I-----+	I
3.500	99.1366	I-----+	I
3.750	100.9411	I-----+	I
4.000	102.4253	I-----+	I
4.250	103.6460	I-----+	I
4.500	104.6498	I-----+	I
4.750	105.4750	I-----+	I
5.000	106.1536	I-----+	I
5.250	106.7114	I-----+	I
5.500	107.1700	I-----+	I
5.750	107.5469	I-----+	I
6.000	107.8569	I-----+	I
6.250	108.1117	I-----+	I
6.500	108.3212	I-----+	I
6.750	108.4934	I-----+	I
7.000	108.6349	I-----+	I
7.250	108.7513	I-----+	I
7.500	108.8469	I-----+	I
7.750	108.9255	I-----+	I
8.000	108.9900	I-----+	I
8.250	109.0432	I-----+	I
8.500	109.0869	I-----+	I
8.750	109.1228	I-----+	I
9.000	109.1523	I-----+	I
9.250	109.1765	I-----+	I
9.500	109.1965	I-----+	I
9.750	109.2129	I-----+	I
10.000	109.2264	I-----+	I
10.250	109.2375	I-----+	I
10.500	109.2467	I-----+	I
10.750	109.2541	I-----+	I
11.000	109.2603	I-----+	I
11.250	109.2654	I-----+	I
11.500	109.2696	I-----+	I
11.750	109.2730	I-----+	I
12.000	109.2758	I-----+	I
12.250	109.2781	I-----+	I
12.500	109.2800	I-----+	I
12.750	109.2815	I-----+	I
13.000	109.2828	I-----+	I
13.250	109.2838	I-----+	I
13.500	109.2847	I-----+	I
13.750	109.2854	I-----+	I
14.000	109.2860	I-----+	I
14.250	109.2865	I-----+	I
14.500	109.2868	I-----+	I
14.750	109.2871	I-----+	I
15.000	109.2874	I-----+	I
15.250	109.2877	I-----+	I
15.500	109.2880	I-----+	I
15.750	109.2880	I-----+	I
16.000	109.2880	I-----+	I
16.250	109.2880	I-----+	I
16.500	109.2880	I-----+	I
16.750	109.2880	I-----+	I
17.000	109.2880	I-----+	I
17.250	109.2880	I-----+	I
17.500	109.2880	I-----+	I
17.750	109.2880	I-----+	I
18.000	109.2880	I-----+	I
18.250	109.2880	I-----+	I
18.500	109.2880	I-----+	I
18.750	109.2880	I-----+	I
19.000	109.2880	I-----+	I
19.250	109.2880	I-----+	I
19.500	109.2880	I-----+	I

RS - 2

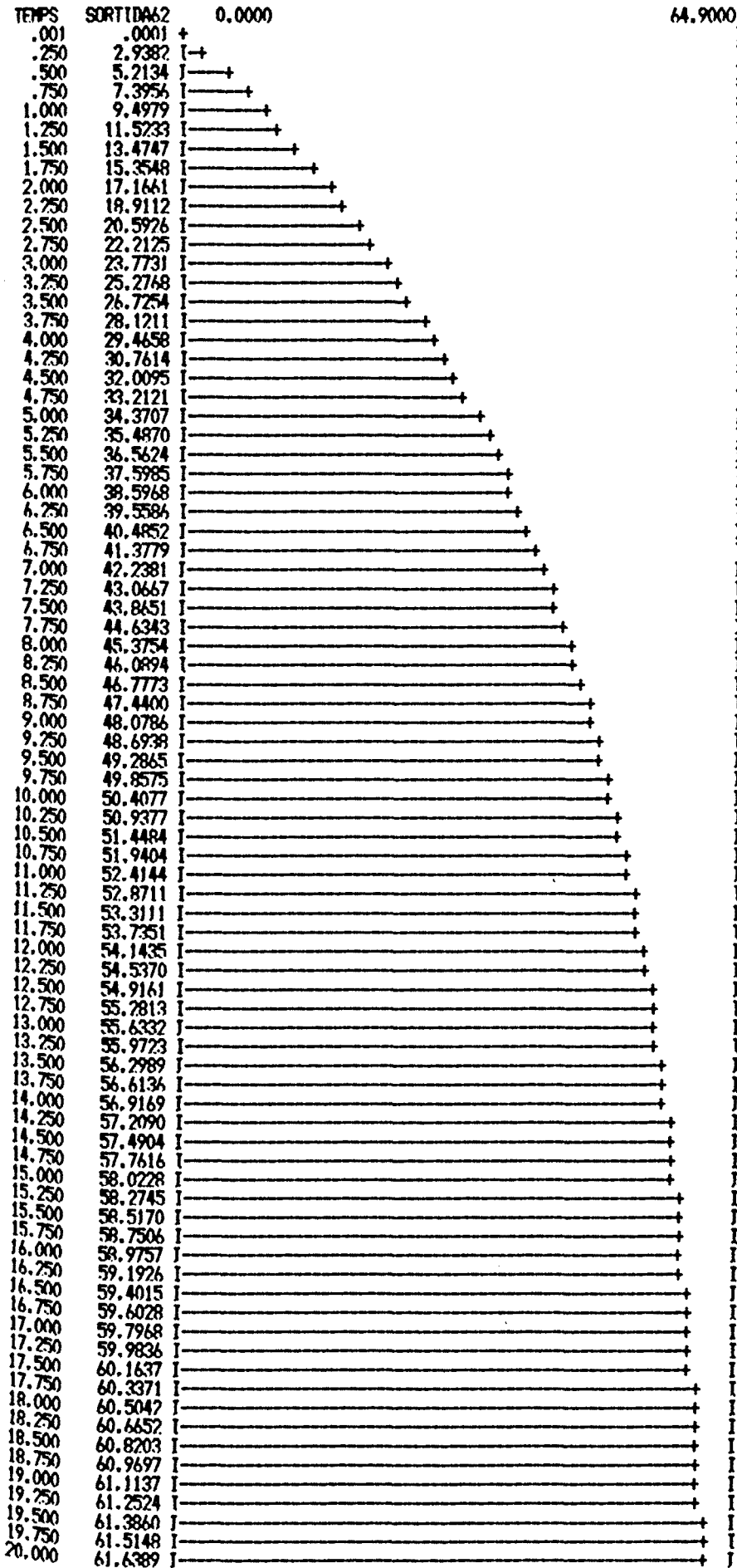
APERTURA DEL
DISTRIBUIDOR DE LA
CENTRAL A

BLOC EIX Y (61) MINIM (0.0000) MAXIM (68.3760)



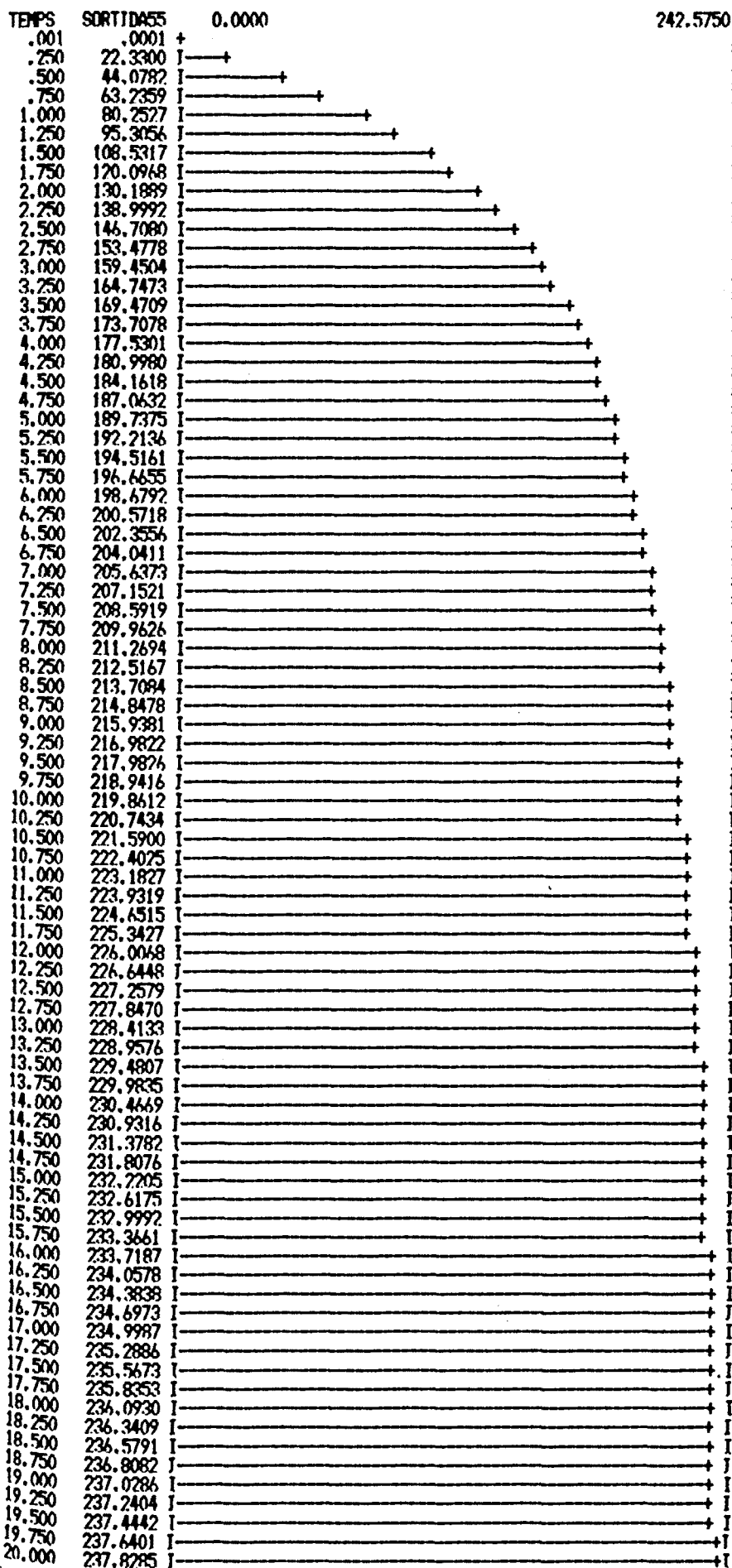
RS - 3
 APERTURA DEL DISTRIBUIDOR
 DE LA CENTRAL B

RLOC: FIX Y (62) MINIM (0.0000) MAXIM (64.9000)



RS - 4
APERTURA DEL DISTRIBUIDOR
DE LA CENTRAL C

BLOC EIX Y (55) MINIM (0.0000) MAXIM (242.5750)



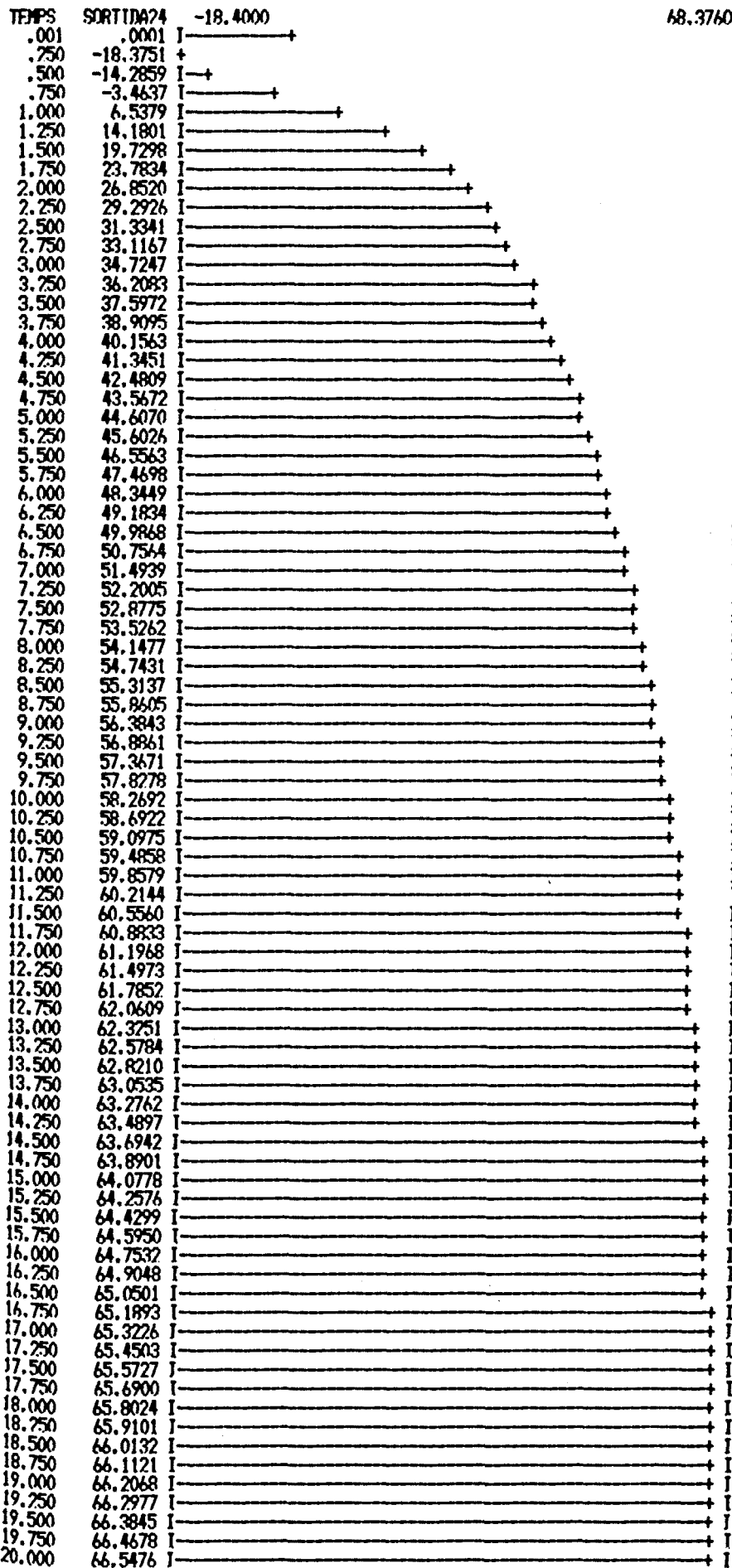
RS - 5
 APERTURA TOTAL DE LOS
 DISTRIBUIDORES

BLOC FIX Y (12) MINIM (-15.1000) MAXIM (109.2900)

TEMPS	SORTIDA12	-15.1000	109.2900
.001	.0001	I → +	I
.250	-7.4245	I → +	I
.500	-14.8904	I → +	I
.750	-15.0555	I → +	I
1.000	-8.5344	I → +	I
1.250	2.1756	I → +	I
1.500	14.7648	I → +	I
1.750	27.6151	I → +	I
2.000	39.7627	I → +	I
2.250	50.7731	I → +	I
2.500	60.3199	I → +	I
2.750	68.5544	I → +	I
3.000	75.5307	I → +	I
3.250	81.3817	I → +	I
3.500	86.2594	I → +	I
3.750	90.3072	I → +	I
4.000	93.6568	I → +	I
4.250	96.4227	I → +	I
4.500	98.7024	I → +	I
4.750	100.5820	I → +	I
5.000	102.1285	I → +	I
5.250	103.4010	I → +	I
5.500	104.4478	I → +	I
5.750	105.3089	I → +	I
6.000	106.0168	I → +	I
6.250	106.5986	I → +	I
6.500	107.0771	I → +	I
6.750	107.4706	I → +	I
7.000	107.7942	I → +	I
7.250	108.0601	I → +	I
7.500	108.2789	I → +	I
7.750	108.4586	I → +	I
8.000	108.6063	I → +	I
8.250	108.7276	I → +	I
8.500	108.8273	I → +	I
8.750	108.9094	I → +	I
9.000	108.9767	I → +	I
9.250	109.0323	I → +	I
9.500	109.0780	I → +	I
9.750	109.1154	I → +	I
10.000	109.1461	I → +	I
10.250	109.1714	I → +	I
10.500	109.1923	I → +	I
10.750	109.2094	I → +	I
11.000	109.2234	I → +	I
11.250	109.2351	I → +	I
11.500	109.2446	I → +	I
11.750	109.2525	I → +	I
12.000	109.2590	I → +	I
12.250	109.2641	I → +	I
12.500	109.2685	I → +	I
12.750	109.2722	I → +	I
13.000	109.2749	I → +	I
13.250	109.2774	I → +	I
13.500	109.2792	I → +	I
13.750	109.2809	I → +	I
14.000	109.2824	I → +	I
14.250	109.2834	I → +	I
14.500	109.2845	I → +	I
14.750	109.2851	I → +	I
15.000	109.2856	I → +	I
15.250	109.2858	I → +	I
15.500	109.2863	I → +	I
15.750	109.2869	I → +	I
16.000	109.2874	I → +	I
16.250	109.2877	I → +	I
16.500	109.2877	I → +	I
16.750	109.2877	I → +	I
17.000	109.2877	I → +	I
17.250	109.2877	I → +	I
17.500	109.2877	I → +	I
17.750	109.2877	I → +	I
18.000	109.2877	I → +	I
18.250	109.2877	I → +	I
18.500	109.2877	I → +	I
18.750	109.2877	I → +	I
19.000	109.2877	I → +	I
19.250	109.2877	I → +	I
19.500	109.2877	I → +	I
19.750	109.2877	I → +	I
20.000	109.2877	I → +	I

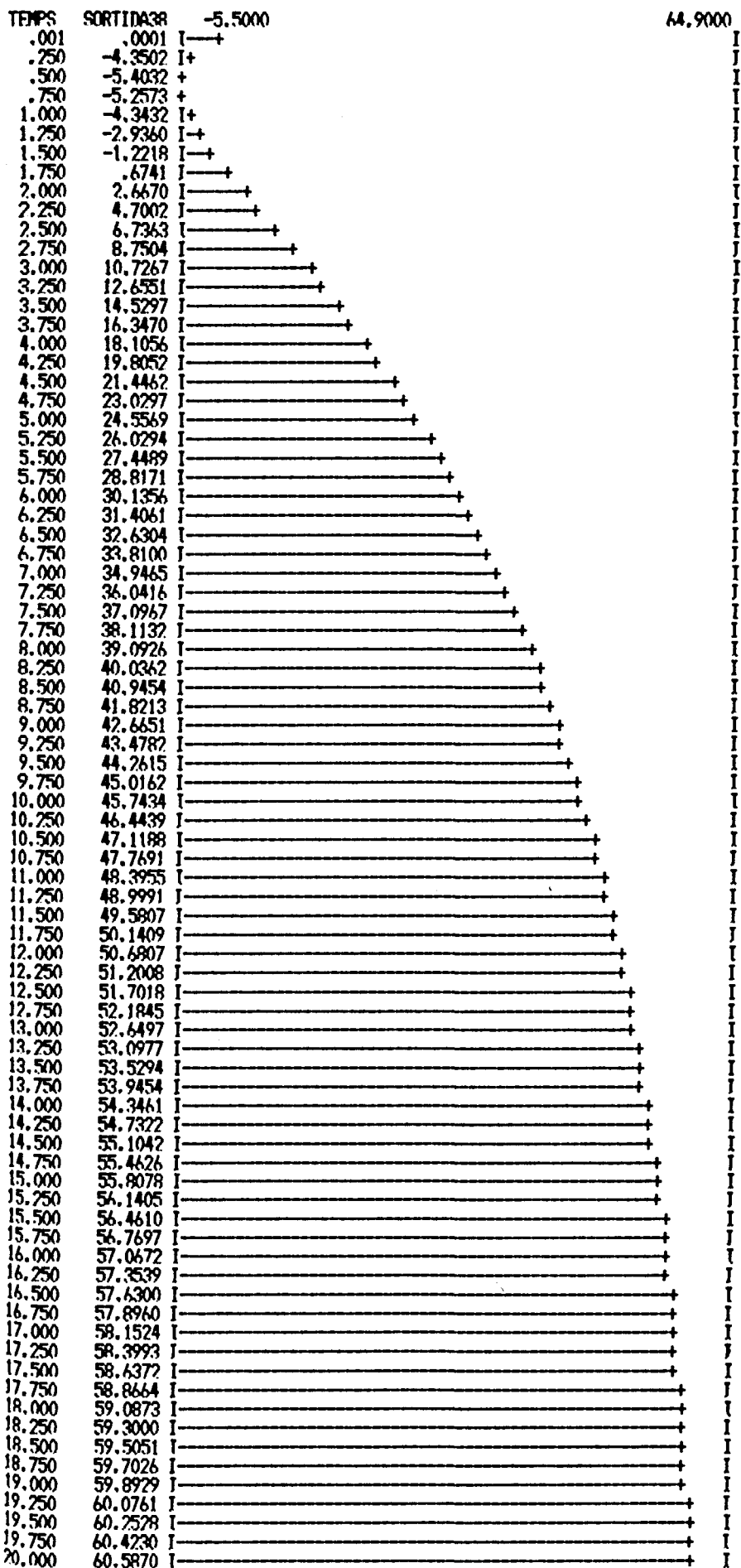
RS - 6
 POTENCIA GENERADA POR LA
 CENTRAL A

BLOC. EIX Y (24) MINIM (-18.4000) MAXIM (68.3760)



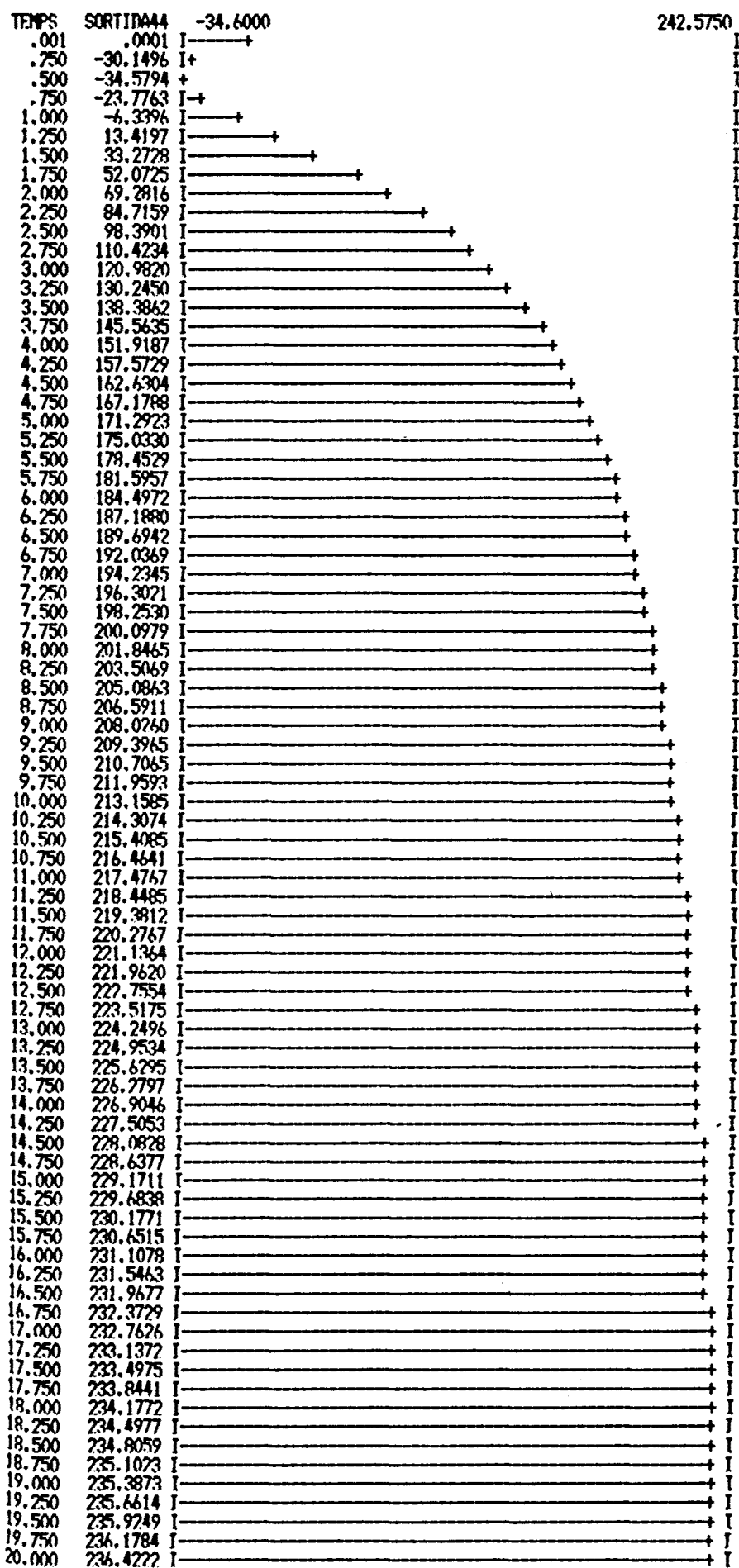
RS - 7
 POTENCIA GENERADA POR LA
 CENTRAL B

BLOC EIX Y (38) MINIM (-5.5000) MAXIM (64.9000)



RS - 8
 POTENCIA GENERADA POR LA
 CENTRAL C

BLOC EIX Y (44) MINIM (-34.6000) MAXIM (242.5750)



RS - 9
 POTENCIA GENERADA TOTAL

BLOC EIX Y (5) MINIM (0.0000) MAXIM (1.0000)

TEMPS SORTIDA 5 0.0000

1.0000

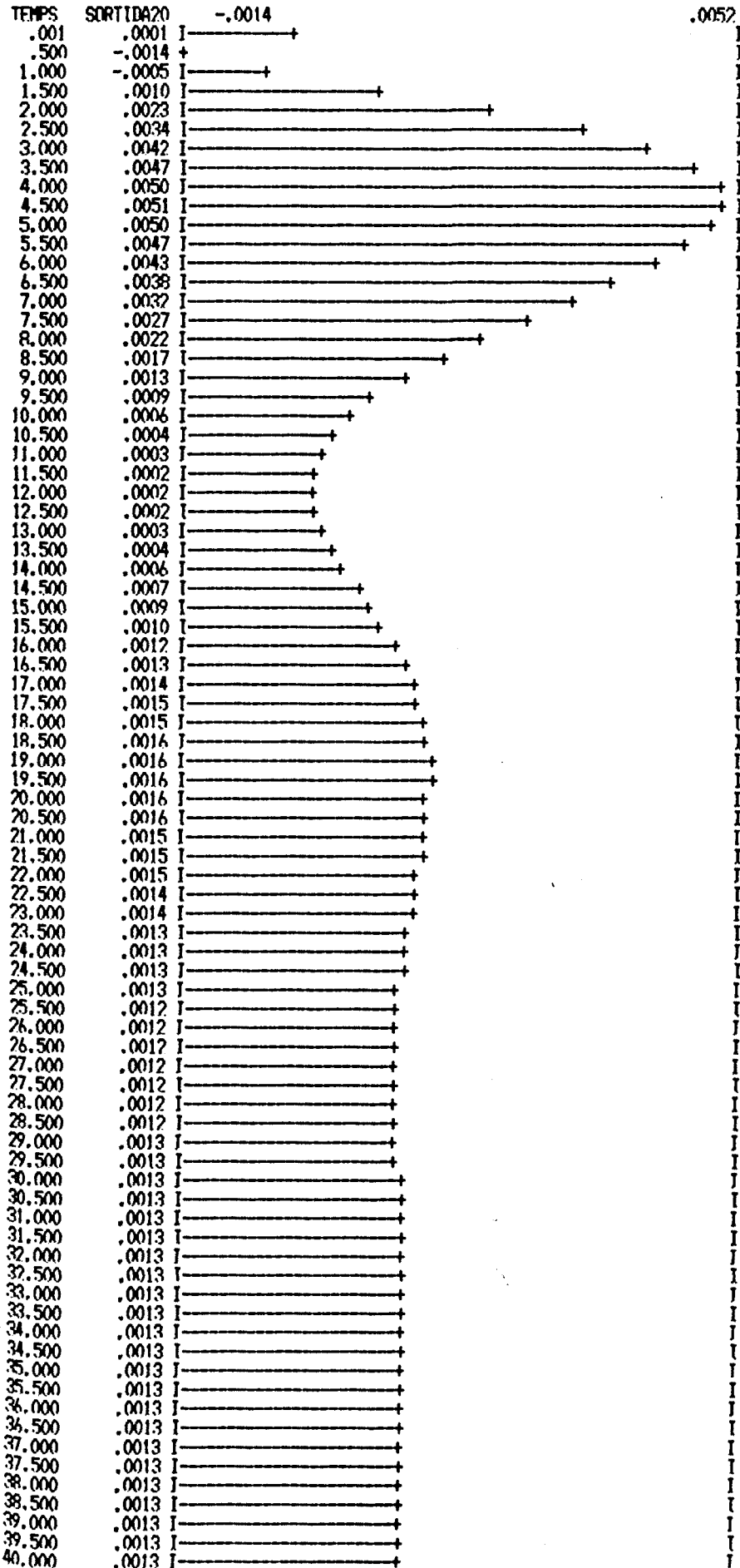
TEMPS	SORTIDA 5	SORTIDA20	SORTIDA24	SORTIDA 2
.00	.0001	.0001	.0001	.1000
.50	.0017	-.0014	-.0031	.1031
1.00	.0029	-.0005	-.0059	.1059
1.50	.0038	.0010	-.0048	.1048
2.00	.0044	.0023	.0004	.0997
2.50	.0048	.0034	.0090	.0911
3.00	.0049	.0042	.0201	.0800
3.50	.0049	.0047	.0328	.0673
4.00	.0046	.0050	.0461	.0540
4.50	.0043	.0051	.0594	.0407
5.00	.0038	.0050	.0719	.0282
5.50	.0033	.0047	.0832	.0169
6.00	.0028	.0043	.0928	.0073
6.50	.0023	.0038	.1007	-.0007
7.00	.0019	.0032	.1067	-.0067
7.50	.0014	.0027	.1107	-.0107
8.00	.0011	.0022	.1130	-.0130
8.50	.0008	.0017	.1136	-.0136
9.00	.0005	.0013	.1127	-.0127
9.50	.0004	.0009	.1108	-.0108
10.00	.0003	.0006	.1079	-.0079
10.50	.0003	.0004	.1044	-.0044
11.00	.0003	.0003	.1005	-.0005
11.50	.0003	.0002	.0965	.0036
12.00	.0004	.0002	.0925	.0076
12.50	.0006	.0002	.0888	.0113
13.00	.0007	.0003	.0855	.0146
13.50	.0009	.0004	.0826	.0175
14.00	.0010	.0006	.0803	.0198
14.50	.0011	.0007	.0785	.0216
15.00	.0012	.0009	.0772	.0229
15.50	.0014	.0010	.0764	.0237
16.00	.0014	.0012	.0762	.0239
16.50	.0015	.0013	.0763	.0238
17.00	.0015	.0014	.0767	.0234
17.50	.0016	.0015	.0775	.0226
18.00	.0016	.0015	.0784	.0217
18.50	.0016	.0016	.0794	.0207
19.00	.0016	.0016	.0804	.0197
19.50	.0015	.0016	.0815	.0186
20.00	.0015	.0016	.0825	.0176
20.50	.0015	.0016	.0834	.0167
21.00	.0014	.0015	.0841	.0160
21.50	.0014	.0015	.0848	.0153
22.00	.0014	.0015	.0853	.0148
22.50	.0013	.0014	.0856	.0145
23.00	.0013	.0014	.0858	.0143
23.50	.0013	.0013	.0859	.0142
24.00	.0013	.0013	.0859	.0142
24.50	.0012	.0013	.0857	.0144
25.00	.0012	.0013	.0855	.0146
25.50	.0012	.0012	.0853	.0148
26.00	.0012	.0012	.0850	.0151
26.50	.0012	.0012	.0847	.0154
27.00	.0012	.0012	.0844	.0157
27.50	.0012	.0012	.0842	.0159
28.00	.0013	.0012	.0839	.0162
28.50	.0013	.0012	.0837	.0164
29.00	.0013	.0013	.0835	.0166
29.50	.0013	.0013	.0834	.0167
30.00	.0013	.0013	.0833	.0168
30.50	.0013	.0013	.0832	.0169
31.00	.0013	.0013	.0832	.0169
31.50	.0013	.0013	.0832	.0169
32.00	.0013	.0013	.0832	.0169
32.50	.0013	.0013	.0833	.0168
33.00	.0013	.0013	.0834	.0167
33.50	.0013	.0013	.0834	.0167
34.00	.0013	.0013	.0835	.0166
34.50	.0013	.0013	.0836	.0165
35.00	.0013	.0013	.0837	.0164
35.50	.0013	.0013	.0837	.0164
36.00	.0013	.0013	.0838	.0163
36.50	.0013	.0013	.0838	.0163
37.00	.0013	.0013	.0839	.0162
37.50	.0013	.0013	.0839	.0162
38.00	.0013	.0013	.0839	.0162
38.50	.0013	.0013	.0839	.0162

RS - 17

AREA 1

 $\Delta f = 0,1 \text{ Hz}$.

BLOC EIX Y (20) MINIM (-.0014) MAXIM (.0052)

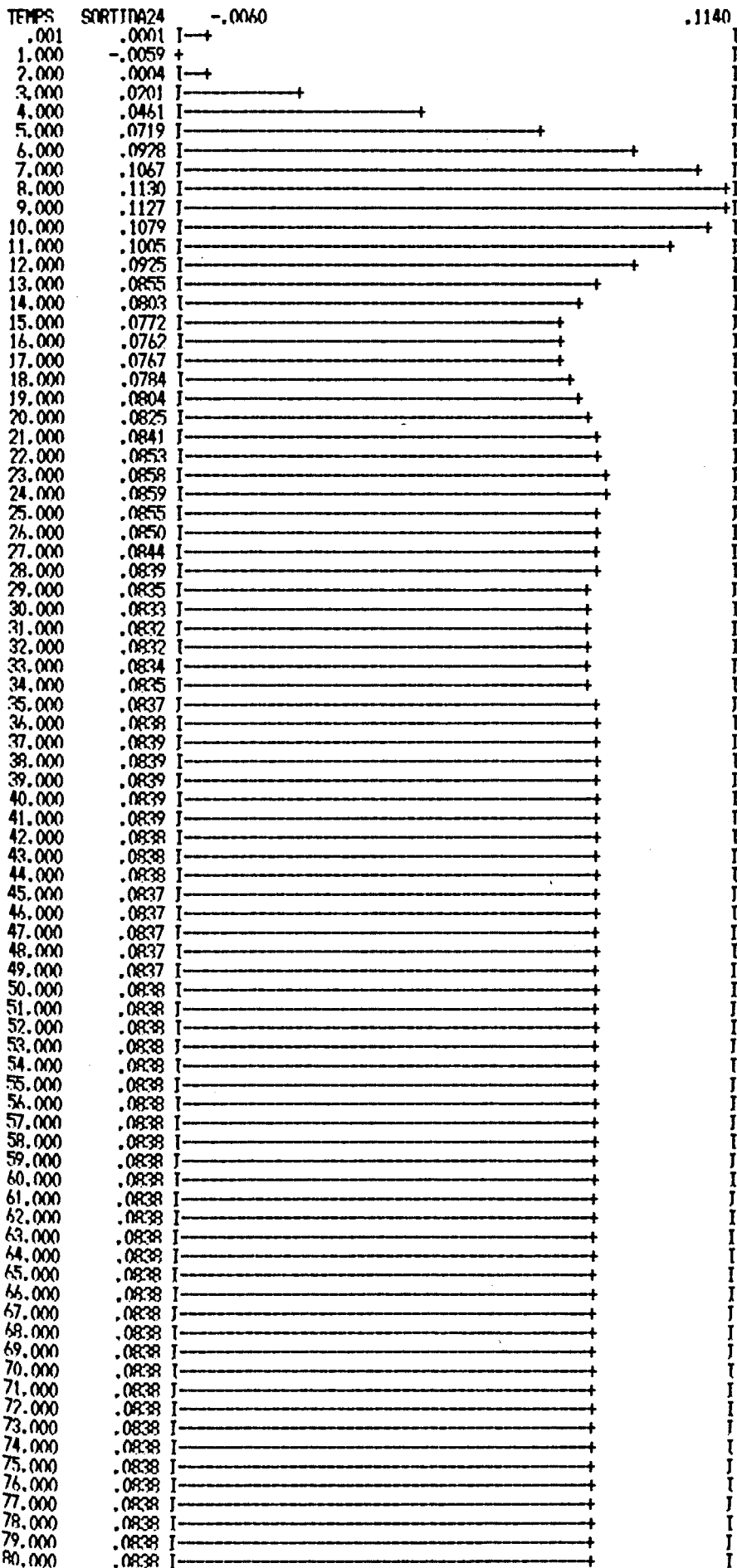


RS - 18

AREA 1

POTENCIA GENERADA

BLOC ETX Y (24) MTNTH (-.0060) MAXTH (.1140)

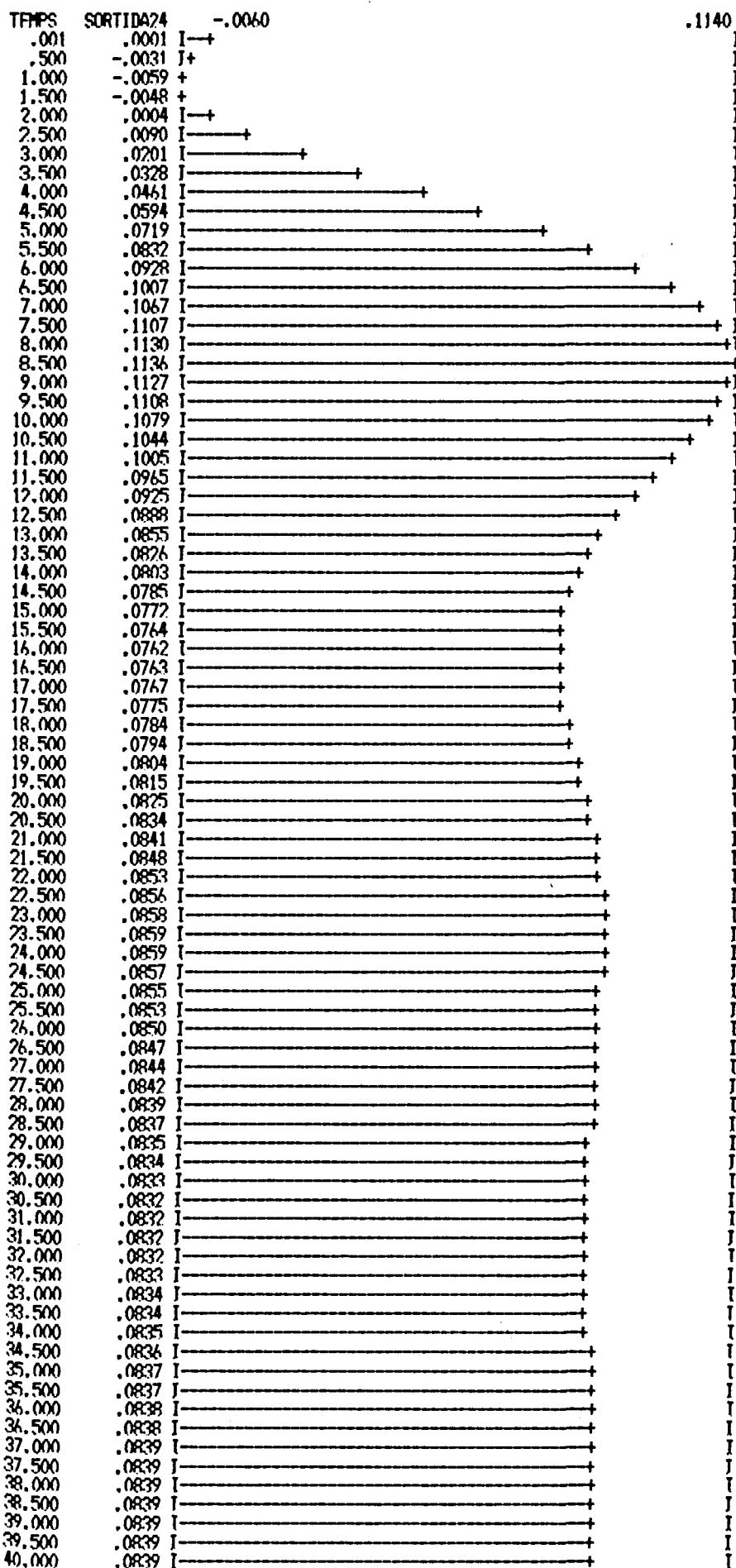


RS - 19

AREA 1

VARIACIONES DE
FRECUENCIA

BLOC ETX Y (24) MINIM (-.0060) MAXIM (.1140)



R S - 20

AREA 1

VARIACIONES DE FRECUENCIA

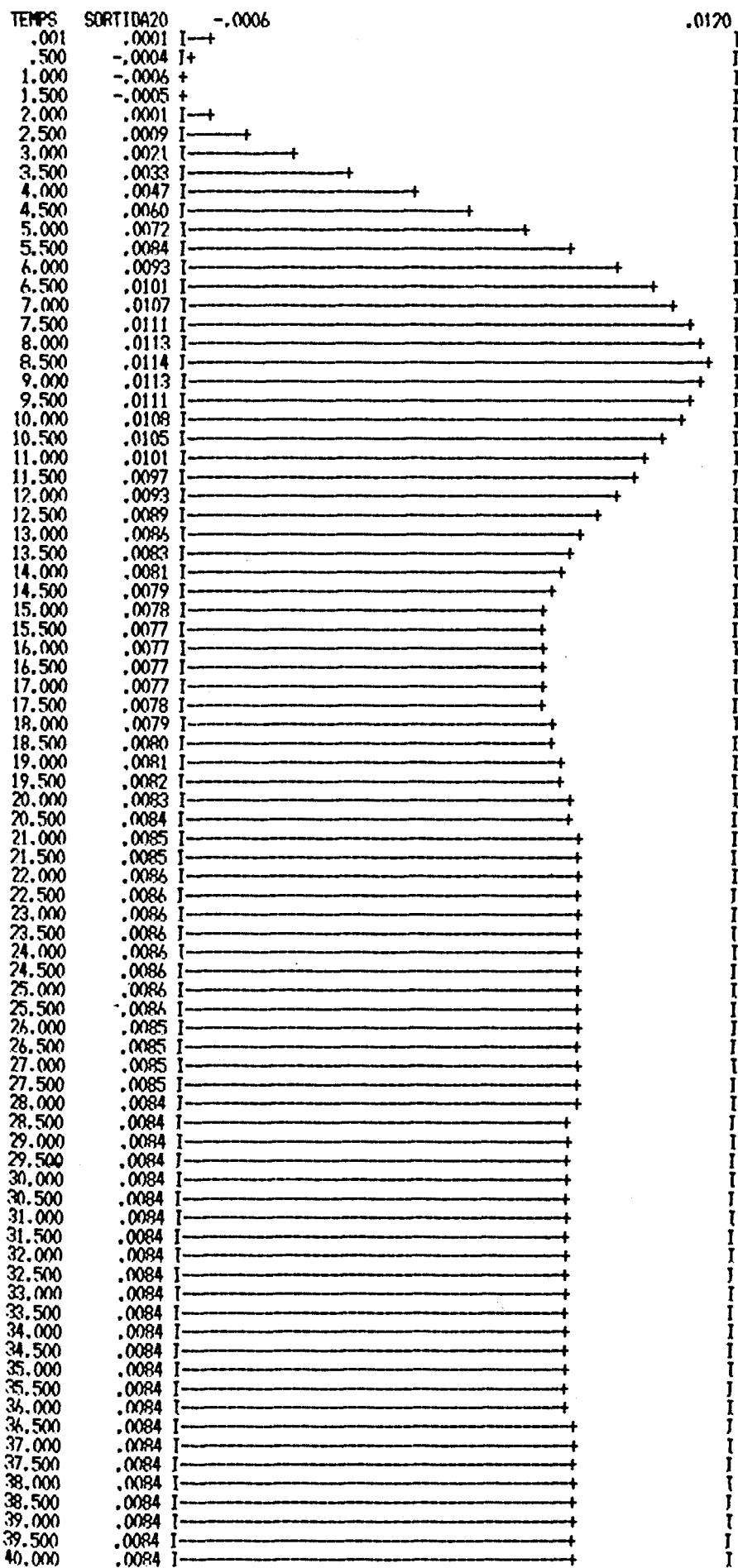
TFMPS	SORTIDA 5	SORTIDA20	SORTIDA24	SORTIDA22
.00	.0001	.0001	.0001	-.0100
.50	.0003	-.0004	-.0310	-.0104
1.00	.0010	-.0006	-.0615	-.0106
1.50	.0020	-.0005	-.0909	-.0105
2.00	.0031	.0001	-.1181	-.0100
2.50	.0044	.0009	-.1418	-.0092
3.00	.0056	.0021	-.1615	-.0080
3.50	.0069	.0033	-.1766	-.0068
4.00	.0080	.0047	-.1870	-.0054
4.50	.0090	.0060	-.1928	-.0041
5.00	.0098	.0072	-.1945	-.0029
5.50	.0104	.0084	-.1924	-.0017
6.00	.0109	.0093	-.1872	-.0008
6.50	.0112	.0101	-.1796	.0001
7.00	.0113	.0107	-.1702	.0007
7.50	.0112	.0111	-.1597	.0011
8.00	.0111	.0113	-.1488	.0013
8.50	.0108	.0114	-.1379	.0014
9.00	.0105	.0113	-.1275	.0013
9.50	.0102	.0111	-.1181	.0011
10.00	.0098	.0108	-.1099	.0008
10.50	.0094	.0105	-.1030	.0005
11.00	.0090	.0101	-.0975	.0001
11.50	.0087	.0097	-.0935	-.0004
12.00	.0084	.0093	-.0910	-.0008
12.50	.0082	.0089	-.0897	-.0012
13.00	.0080	.0086	-.0895	-.0015
13.50	.0078	.0083	-.0903	-.0018
14.00	.0077	.0081	-.0919	-.0020
14.50	.0077	.0079	-.0940	-.0022
15.00	.0077	.0078	-.0965	-.0023
15.50	.0077	.0077	-.0992	-.0024
16.00	.0078	.0077	-.1019	-.0024
16.50	.0079	.0077	-.1046	-.0024
17.00	.0080	.0077	-.1070	-.0024
17.50	.0081	.0078	-.1091	-.0023
18.00	.0082	.0079	-.1109	-.0022
18.50	.0083	.0080	-.1123	-.0021
19.00	.0084	.0081	-.1133	-.0020
19.50	.0084	.0082	-.1139	-.0019
20.00	.0085	.0083	-.1142	-.0018
20.50	.0085	.0084	-.1142	-.0017
21.00	.0086	.0085	-.1140	-.0016
21.50	.0086	.0085	-.1135	-.0016
22.00	.0086	.0086	-.1129	-.0015
22.50	.0086	.0086	-.1122	-.0015
23.00	.0086	.0086	-.1114	-.0015
23.50	.0086	.0086	-.1107	-.0015
24.00	.0086	.0086	-.1099	-.0015
24.50	.0086	.0086	-.1092	-.0015
25.00	.0085	.0086	-.1086	-.0015
25.50	.0085	.0086	-.1081	-.0015
26.00	.0085	.0085	-.1077	-.0016
26.50	.0084	.0085	-.1074	-.0016
27.00	.0084	.0085	-.1072	-.0016
27.50	.0084	.0085	-.1072	-.0016
28.00	.0084	.0084	-.1071	-.0017
28.50	.0084	.0084	-.1072	-.0017
29.00	.0084	.0084	-.1073	-.0017
29.50	.0084	.0084	-.1075	-.0017
30.00	.0084	.0084	-.1077	-.0017
30.50	.0084	.0084	-.1079	-.0017
31.00	.0084	.0084	-.1081	-.0017
31.50	.0084	.0084	-.1083	-.0017
32.00	.0084	.0084	-.1085	-.0017
32.50	.0084	.0084	-.1086	-.0017
33.00	.0084	.0084	-.1088	-.0017
33.50	.0084	.0084	-.1089	-.0017
34.00	.0084	.0084	-.1090	-.0017
34.50	.0084	.0084	-.1090	-.0017
35.00	.0084	.0084	-.1090	-.0017
35.50	.0084	.0084	-.1090	-.0017
36.00	.0084	.0084	-.1090	-.0017
36.50	.0084	.0084	-.1090	-.0017
37.00	.0084	.0084	-.1090	-.0017
37.50	.0084	.0084	-.1089	-.0017
38.00	.0084	.0084	-.1088	-.0017
38.50	.0084	.0084	-.1088	-.0017
39.00	.0084	.0084	-.1087	-.0017
39.50	.0084	.0084	-.1087	-.0017
40.00	.0084	.0084	-.1086	-.0017

R S - 21

AREA 1

$\Delta P = 0,01 \text{ p.u. MW}$

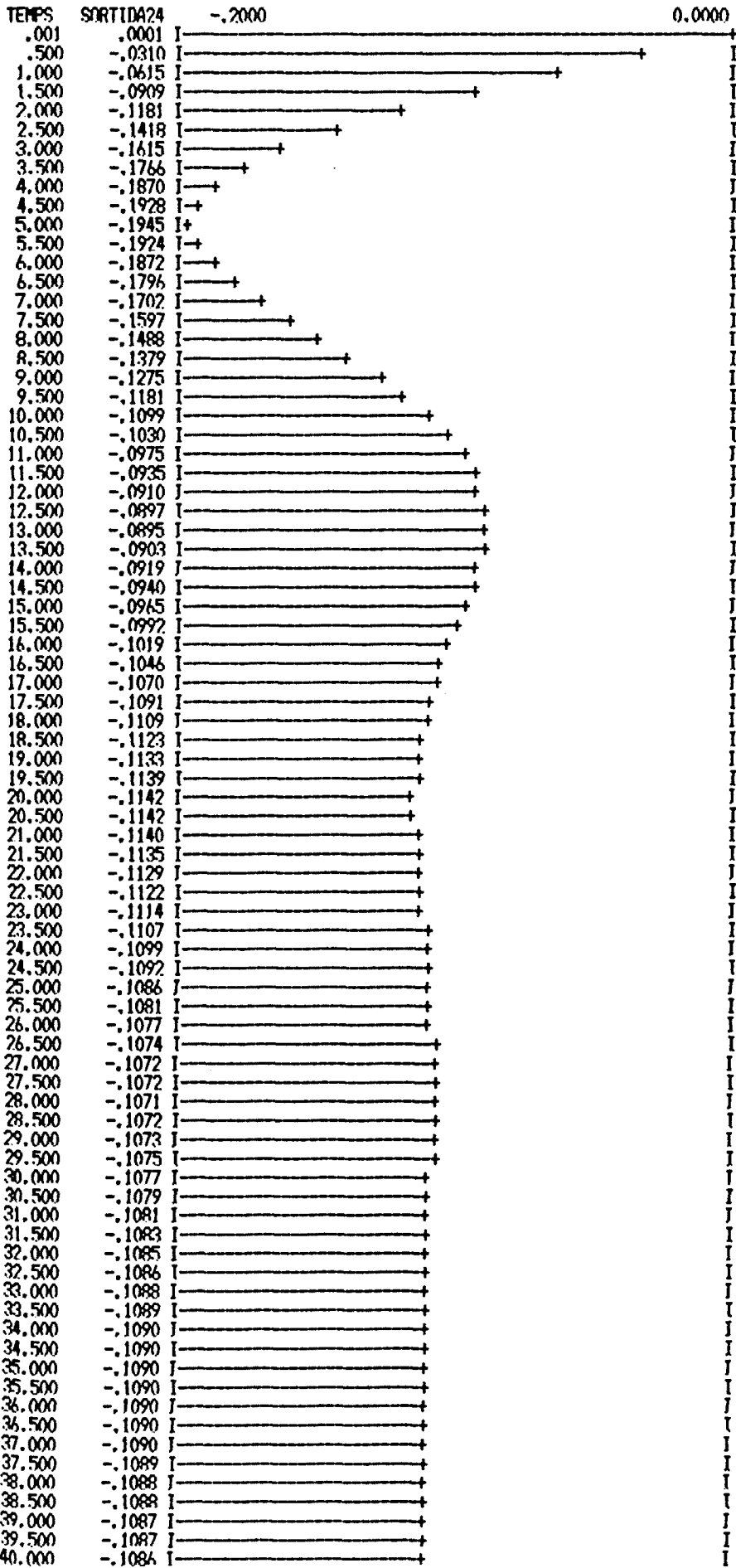
BLOC FIX Y (20) MINIM (-.0006) MAXIM (.0120)



RS - 22

POTENCIA GENERADA

BLOC FIX Y (24) MINIM (-.2000) MAXIM (0.0000)



R S - 23

VARIACIONES DE FRECUENCIA

TEMPS	SORTIDA24	SORTIDA30	SORTIDA27	SORTIDA20
.00	.0001	.0001	.0001	.0001
1.00	-.0198	-.0274	-.0062	-.0002
2.00	-.0331	-.0378	-.0101	.0002
3.00	-.0405	-.0394	-.0102	.0009
4.00	-.0422	-.0389	-.0083	.0015
5.00	-.0404	-.0389	-.0069	.0020
6.00	-.0381	-.0388	-.0068	.0022
7.00	-.0368	-.0382	-.0073	.0024
8.00	-.0364	-.0370	-.0075	.0025
9.00	-.0363	-.0360	-.0074	.0025
10.00	-.0360	-.0355	-.0070	.0026
11.00	-.0356	-.0354	-.0069	.0026
12.00	-.0352	-.0354	-.0069	.0026
13.00	-.0351	-.0353	-.0070	.0026
14.00	-.0351	-.0351	-.0070	.0026
15.00	-.0350	-.0350	-.0070	.0026
16.00	-.0349	-.0349	-.0069	.0027
17.00	-.0349	-.0348	-.0069	.0027
18.00	-.0348	-.0348	-.0069	.0027
19.00	-.0347	-.0348	-.0069	.0027
20.00	-.0347	-.0347	-.0069	.0027
21.00	-.0347	-.0347	-.0069	.0027
22.00	-.0347	-.0347	-.0069	.0027
23.00	-.0347	-.0347	-.0069	.0027
24.00	-.0346	-.0346	-.0069	.0027
25.00	-.0346	-.0346	-.0069	.0027
26.00	-.0346	-.0346	-.0069	.0027
27.00	-.0346	-.0346	-.0069	.0027
28.00	-.0346	-.0346	-.0069	.0027
29.00	-.0346	-.0346	-.0069	.0027
30.00	-.0346	-.0346	-.0069	.0027
31.00	-.0346	-.0346	-.0069	.0027
32.00	-.0346	-.0346	-.0069	.0027
33.00	-.0346	-.0346	-.0069	.0027
34.00	-.0346	-.0346	-.0069	.0027
35.00	-.0346	-.0346	-.0069	.0027
36.00	-.0346	-.0346	-.0069	.0027
37.00	-.0346	-.0346	-.0069	.0027
38.00	-.0346	-.0346	-.0069	.0027
39.00	-.0346	-.0346	-.0069	.0027
40.00	-.0346	-.0346	-.0069	.0027
41.00	-.0346	-.0346	-.0069	.0027
42.00	-.0346	-.0346	-.0069	.0027
43.00	-.0346	-.0346	-.0069	.0027
44.00	-.0346	-.0346	-.0069	.0027
45.00	-.0346	-.0346	-.0069	.0027
46.00	-.0346	-.0346	-.0069	.0027
47.00	-.0346	-.0346	-.0069	.0027
48.00	-.0346	-.0346	-.0069	.0027
49.00	-.0346	-.0346	-.0069	.0027
50.00	-.0346	-.0346	-.0069	.0027
51.00	-.0346	-.0346	-.0069	.0027
52.00	-.0346	-.0346	-.0069	.0027
53.00	-.0346	-.0346	-.0069	.0027
54.00	-.0346	-.0346	-.0069	.0027
55.00	-.0346	-.0346	-.0069	.0027
56.00	-.0346	-.0346	-.0069	.0027
57.00	-.0346	-.0346	-.0069	.0027
58.00	-.0346	-.0346	-.0069	.0027
59.00	-.0346	-.0346	-.0069	.0027
60.00	-.0346	-.0346	-.0069	.0027
61.00	-.0346	-.0346	-.0069	.0027
62.00	-.0346	-.0346	-.0069	.0027
63.00	-.0346	-.0346	-.0069	.0027
64.00	-.0346	-.0346	-.0069	.0027
65.00	-.0346	-.0346	-.0069	.0027
66.00	-.0346	-.0346	-.0069	.0027
67.00	-.0346	-.0346	-.0069	.0027
68.00	-.0346	-.0346	-.0069	.0027
69.00	-.0346	-.0346	-.0069	.0027
70.00	-.0346	-.0346	-.0069	.0027
71.00	-.0346	-.0346	-.0069	.0027
72.00	-.0346	-.0346	-.0069	.0027
73.00	-.0346	-.0346	-.0069	.0027
74.00	-.0346	-.0346	-.0069	.0027
75.00	-.0346	-.0346	-.0069	.0027
76.00	-.0346	-.0346	-.0069	.0027
77.00	-.0346	-.0346	-.0069	.0027
78.00	-.0346	-.0346	-.0069	.0027
79.00	-.0346	-.0346	-.0069	.0027
80.00	-.0346	-.0346	-.0069	.0027

RS - 24

AREA 1 INTERCONECTADA AL AREA 2
SIN GENERACION EN EL AREA 2

P = 0,01 p.u.MW

24: variaciones de f en Area 1

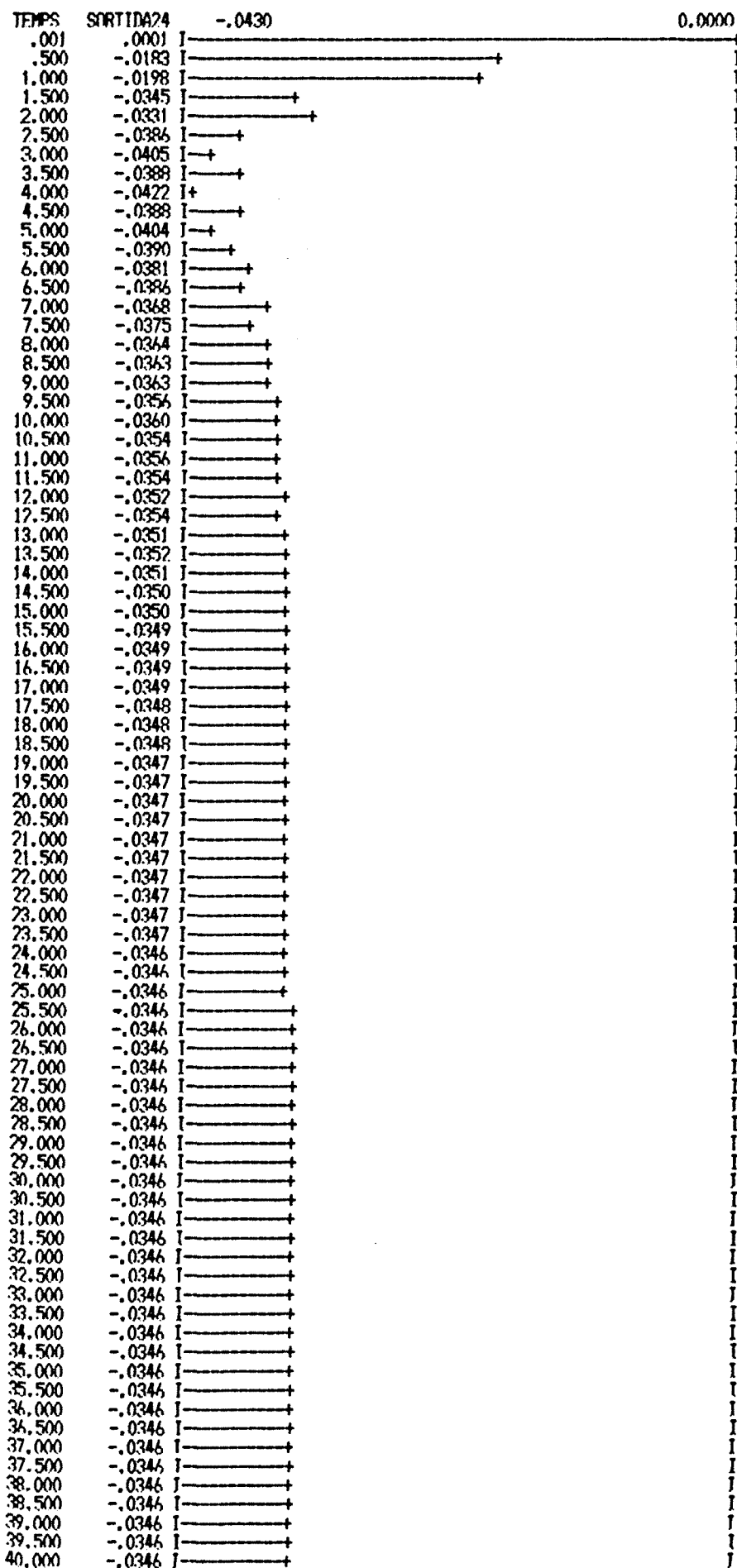
30: " " f en Area 2

27: variaciones de potencia en
la interconexión.

20: potencia generada en el Area 1

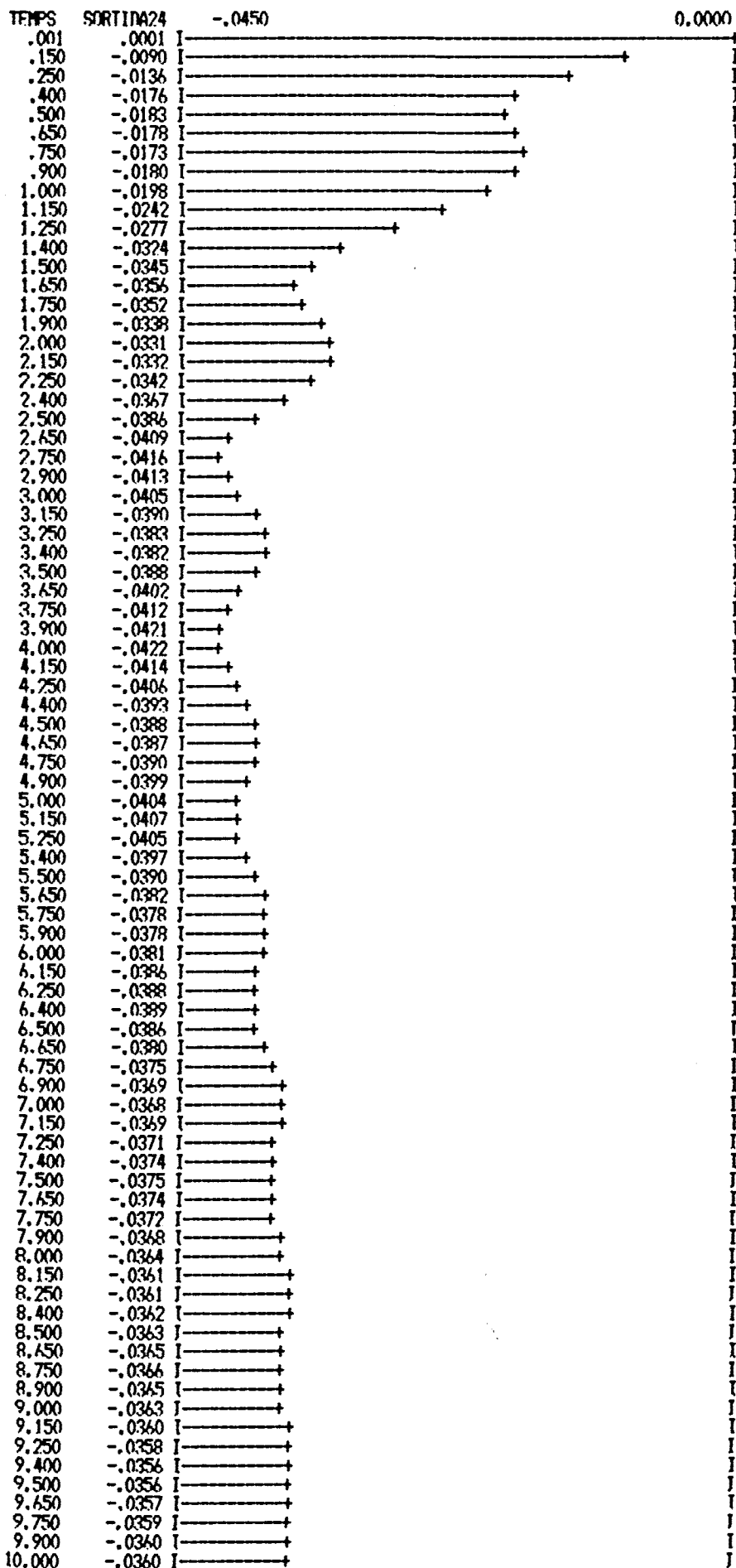
T_{ie} = 2,16 p.u.MW x seg / Hz

BLQC FJX Y (24) MINIM (-.0430) MAXIM (0.0000)



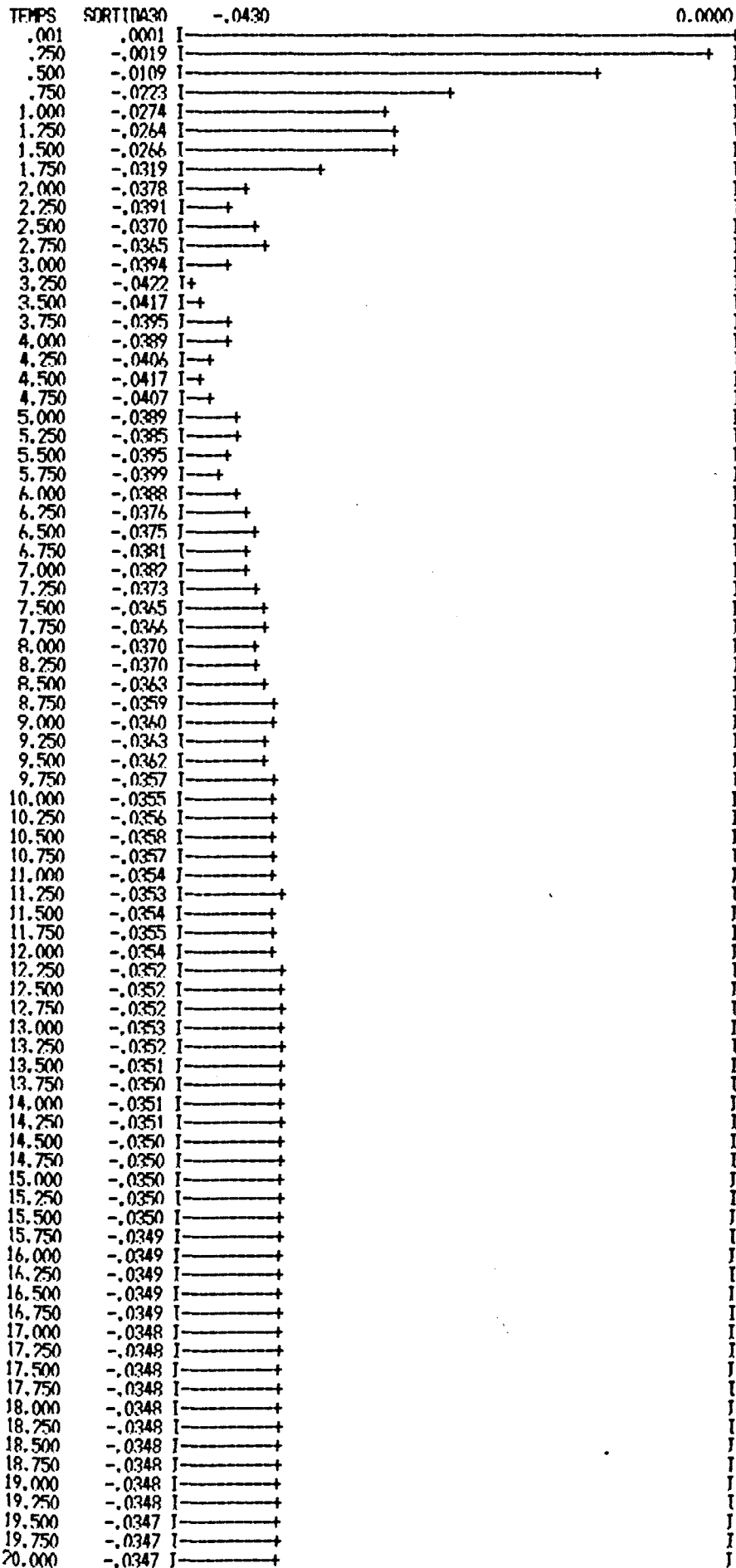
R S-25

BLDC FTX Y (24) MINIM (-.0450) MAXIM (0.0000)



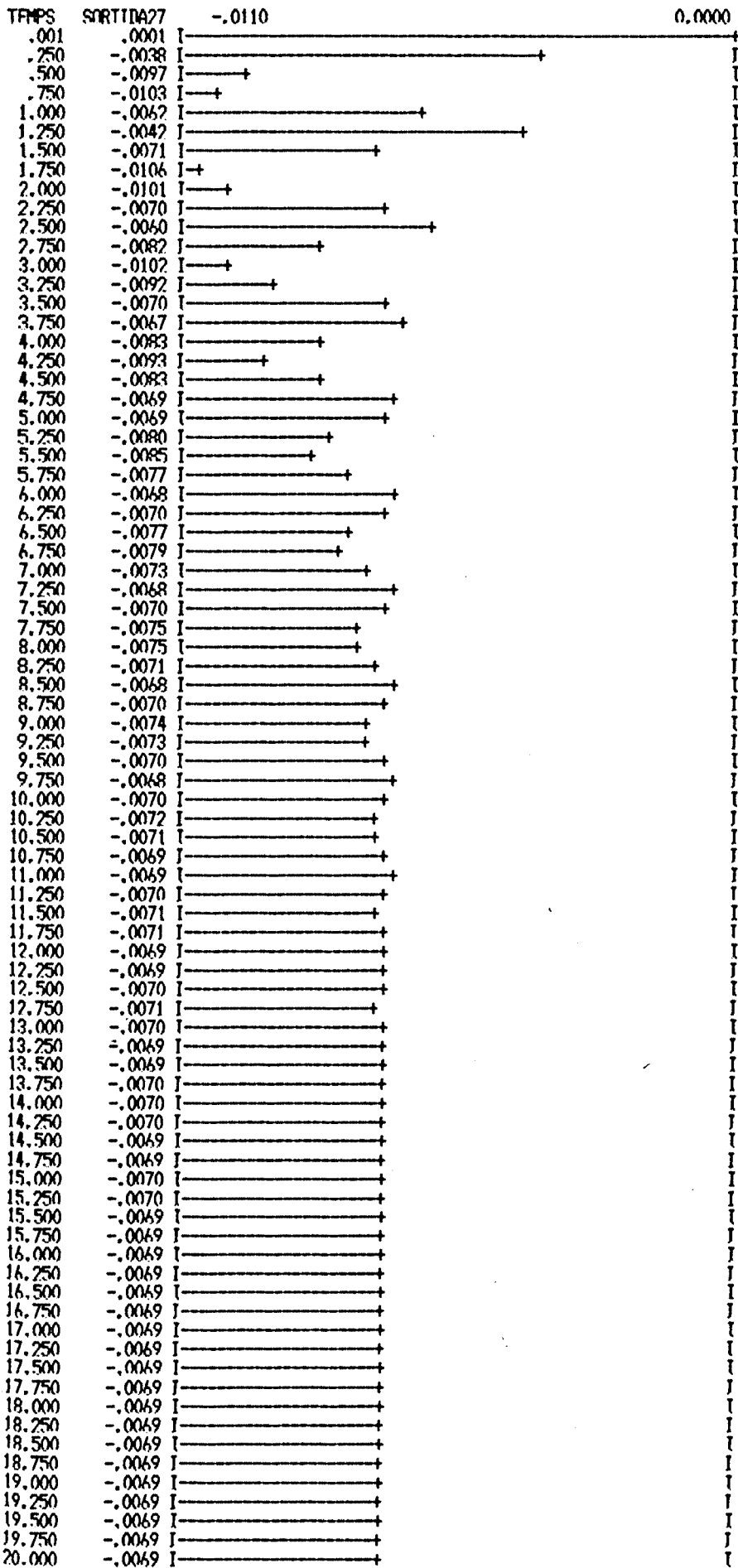
R S -26

BLOC FIX Y (30) MINIM (-.0430) MAXIM (0.0000)



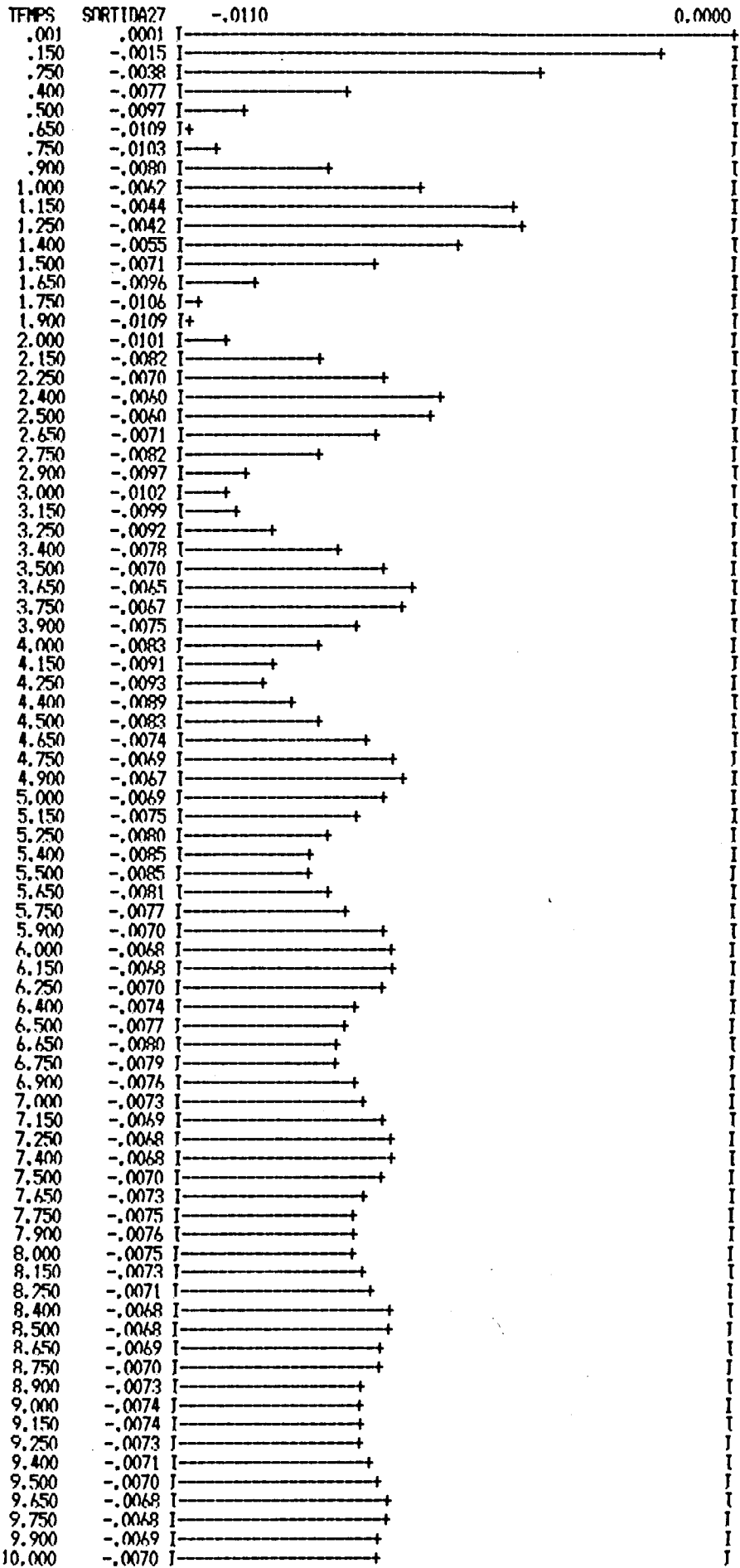
RS - 27

RUC ELX Y (27) MTNIM (-.0110) MAXIM (0.0000)



RS - 28

RLOC FIX Y (27) MINIM (-.0110) MAXIM (0.0000)



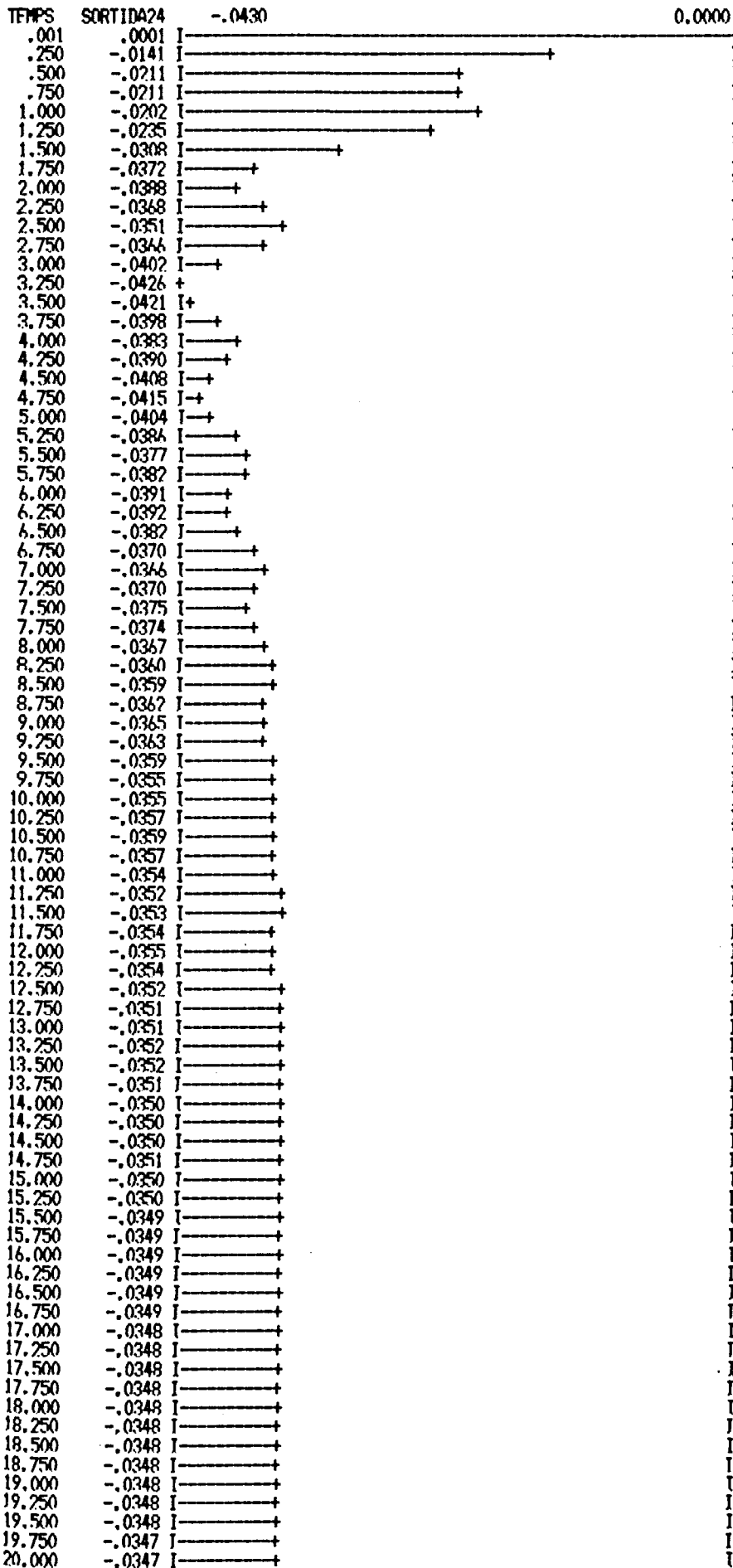
RS - 29

TEMPS	SORTIDA24	SORTIDA30	SORTIDA27	SORTIDA20
.00	.0001	.0001	.0001	.0001
.50	-.0211	-.0085	-.0081	-.0003
1.00	-.0202	-.0286	-.0094	-.0002
1.50	-.0308	-.0295	-.0047	.0001
2.00	-.0388	-.0325	-.0098	.0002
2.50	-.0351	-.0415	-.0091	.0006
3.00	-.0402	-.0385	-.0063	.0010
3.50	-.0421	-.0392	-.0094	.0012
4.00	-.0383	-.0427	-.0082	.0016
4.50	-.0408	-.0391	-.0067	.0018
5.00	-.0404	-.0393	-.0087	.0019
5.50	-.0377	-.0404	-.0075	.0021
6.00	-.0391	-.0377	-.0068	.0022
6.50	-.0382	-.0379	-.0080	.0023
7.00	-.0366	-.0382	-.0071	.0024
7.50	-.0375	-.0364	-.0069	.0024
8.00	-.0367	-.0368	-.0076	.0025
8.50	-.0359	-.0368	-.0070	.0025
9.00	-.0365	-.0357	-.0070	.0025
9.50	-.0359	-.0361	-.0073	.0025
10.00	-.0355	-.0359	-.0069	.0026
10.50	-.0359	-.0353	-.0070	.0026
11.00	-.0354	-.0356	-.0072	.0026
11.50	-.0353	-.0355	-.0069	.0026
12.00	-.0355	-.0352	-.0070	.0026
12.50	-.0352	-.0354	-.0071	.0026
13.00	-.0351	-.0352	-.0069	.0026
13.50	-.0352	-.0350	-.0070	.0026
14.00	-.0350	-.0352	-.0070	.0026
14.50	-.0350	-.0350	-.0069	.0026
15.00	-.0350	-.0349	-.0070	.0026
15.50	-.0349	-.0350	-.0070	.0027
16.00	-.0349	-.0349	-.0069	.0027
16.50	-.0349	-.0349	-.0069	.0027
17.00	-.0348	-.0349	-.0069	.0027
17.50	-.0348	-.0348	-.0069	.0027
18.00	-.0348	-.0348	-.0069	.0027
18.50	-.0348	-.0348	-.0069	.0027
19.00	-.0348	-.0348	-.0069	.0027
19.50	-.0348	-.0347	-.0069	.0027
20.00	-.0347	-.0347	-.0069	.0027
20.50	-.0347	-.0347	-.0069	.0027
21.00	-.0347	-.0347	-.0069	.0027
21.50	-.0347	-.0347	-.0069	.0027
22.00	-.0347	-.0347	-.0069	.0027
22.50	-.0347	-.0347	-.0069	.0027
23.00	-.0347	-.0347	-.0069	.0027
23.50	-.0347	-.0346	-.0069	.0027
24.00	-.0346	-.0346	-.0069	.0027
24.50	-.0346	-.0346	-.0069	.0027
25.00	-.0346	-.0346	-.0069	.0027
25.50	-.0346	-.0346	-.0069	.0027
26.00	-.0346	-.0346	-.0069	.0027
26.50	-.0346	-.0346	-.0069	.0027
27.00	-.0346	-.0346	-.0069	.0027
27.50	-.0346	-.0346	-.0069	.0027
28.00	-.0346	-.0346	-.0069	.0027
28.50	-.0346	-.0346	-.0069	.0027
29.00	-.0346	-.0346	-.0069	.0027
29.50	-.0346	-.0346	-.0069	.0027
30.00	-.0346	-.0346	-.0069	.0027
30.50	-.0346	-.0346	-.0069	.0027
31.00	-.0346	-.0346	-.0069	.0027
31.50	-.0346	-.0346	-.0069	.0027
32.00	-.0346	-.0346	-.0069	.0027
32.50	-.0346	-.0346	-.0069	.0027
33.00	-.0346	-.0346	-.0069	.0027
33.50	-.0346	-.0346	-.0069	.0027
34.00	-.0346	-.0346	-.0069	.0027
34.50	-.0346	-.0346	-.0069	.0027
35.00	-.0346	-.0346	-.0069	.0027
35.50	-.0346	-.0346	-.0069	.0027
36.00	-.0346	-.0346	-.0069	.0027
36.50	-.0346	-.0346	-.0069	.0027
37.00	-.0346	-.0346	-.0069	.0027
37.50	-.0346	-.0346	-.0069	.0027
38.00	-.0346	-.0346	-.0069	.0027
38.50	-.0346	-.0346	-.0069	.0027
39.00	-.0346	-.0346	-.0069	.0027
39.50	-.0346	-.0346	-.0069	.0027
40.00	-.0346	-.0346	-.0069	.0027

RS - 30

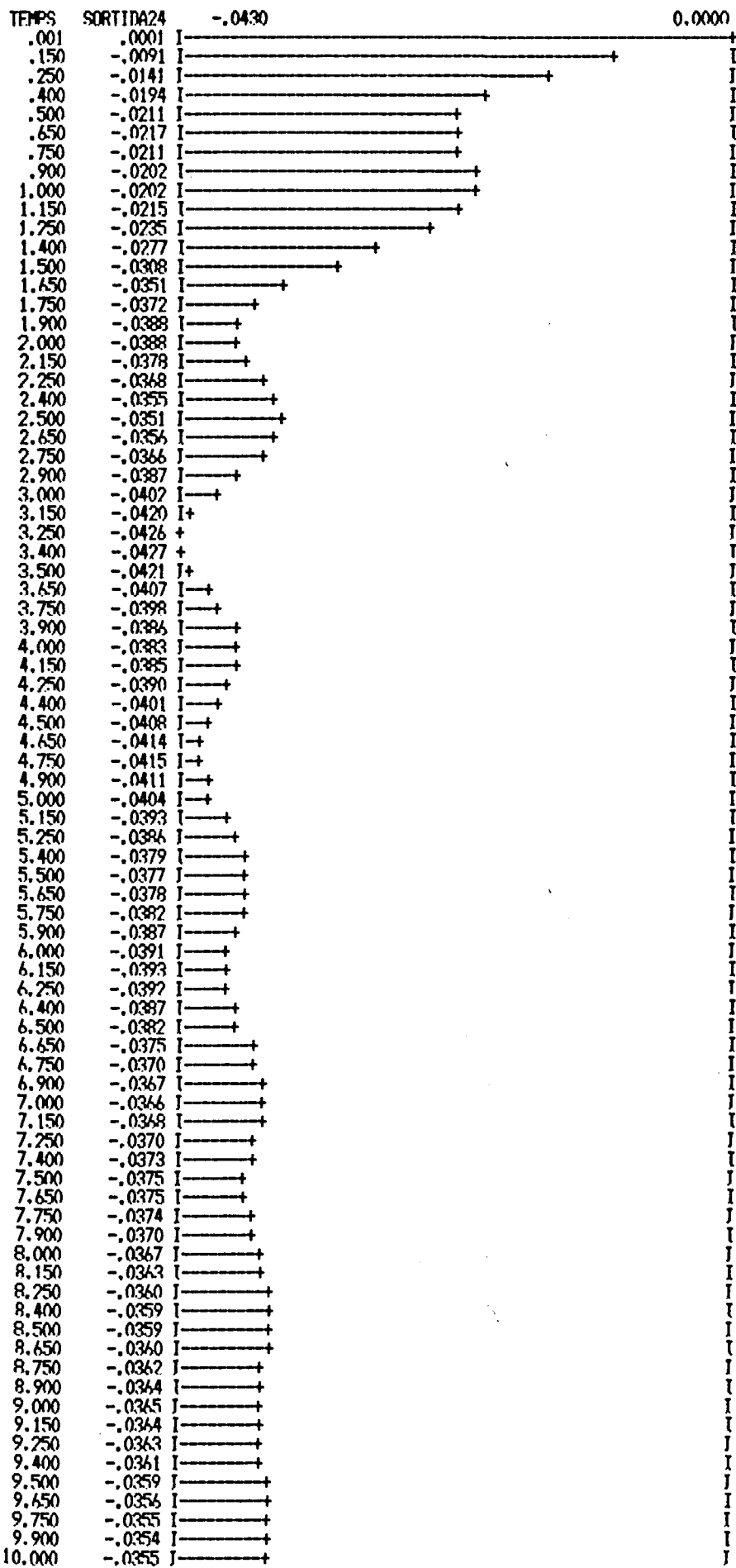
$$T_{ie} = 1,53 \text{ p.u.MW} \times \text{seg} / \text{Hz}$$

BLOC ETX Y (24) MINIM (-.0430) MAXIM (0.0000)



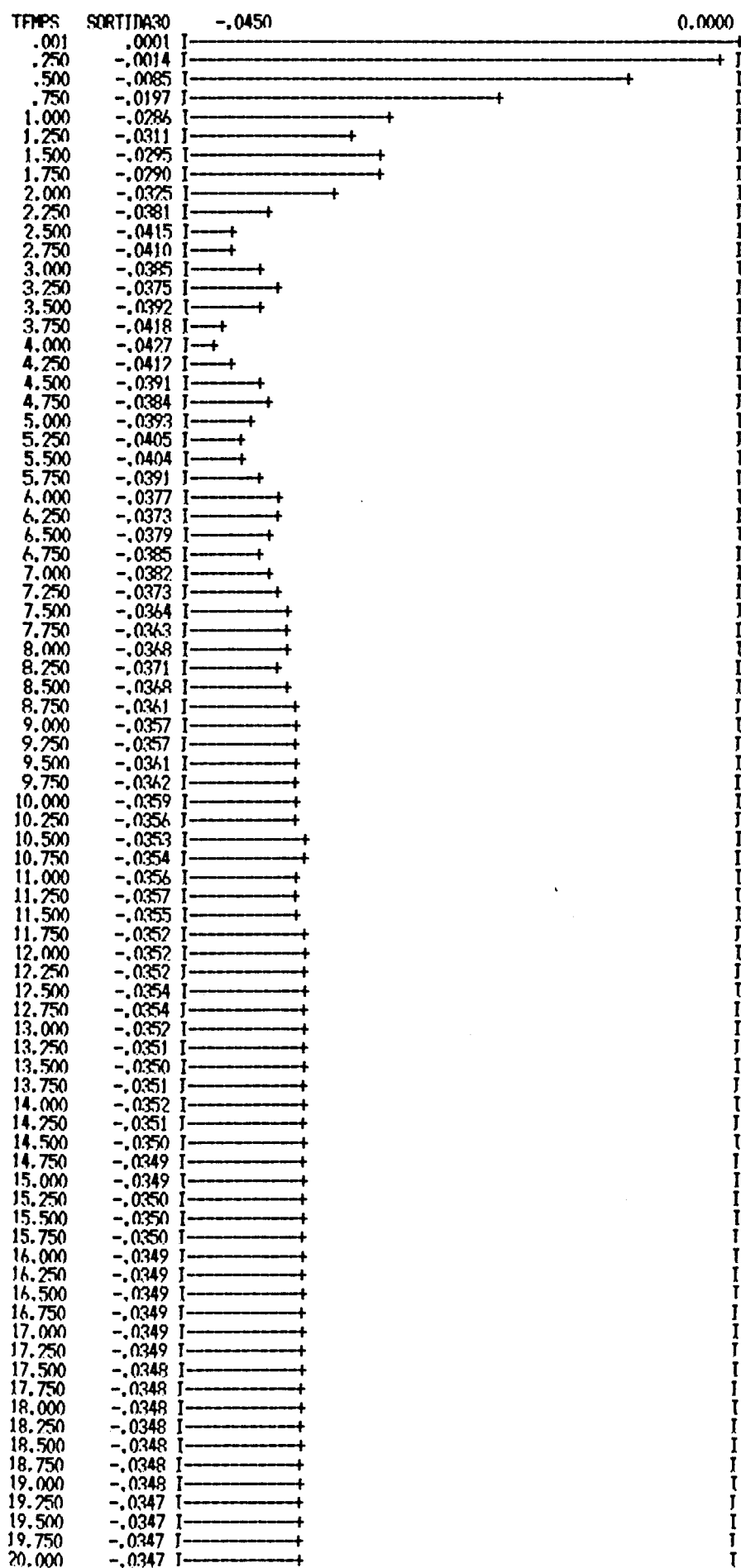
R S - 31

RLOC FIX Y (24) MINIM (-.0430) MAXIM (0.0000)



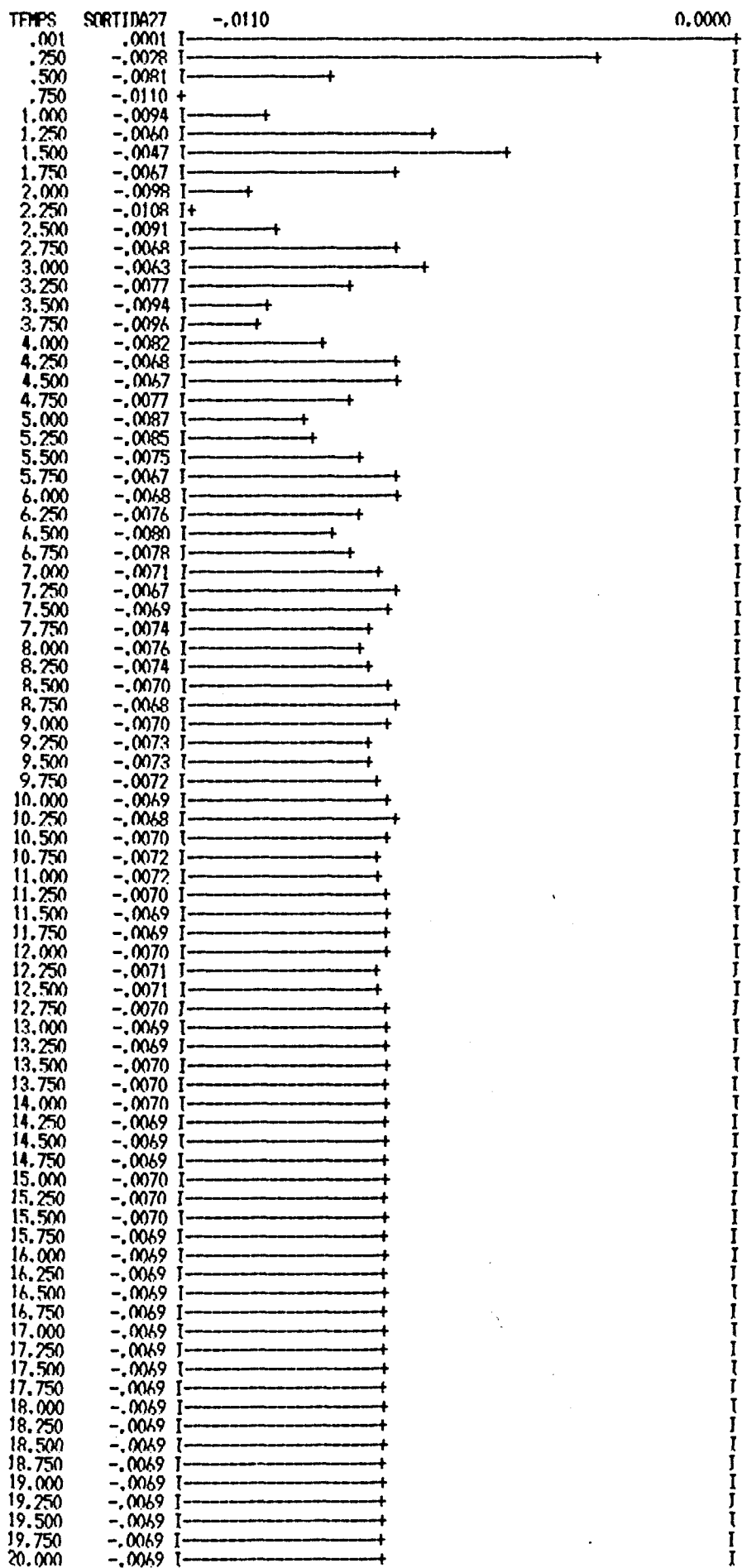
R S - 32

BLOC ETX Y (30) MINIM (-.0450) MAXIM (0.0000)



R S -33

BLOC FIX Y (27) MINIM (-.0110) MAXIM (0.0000)

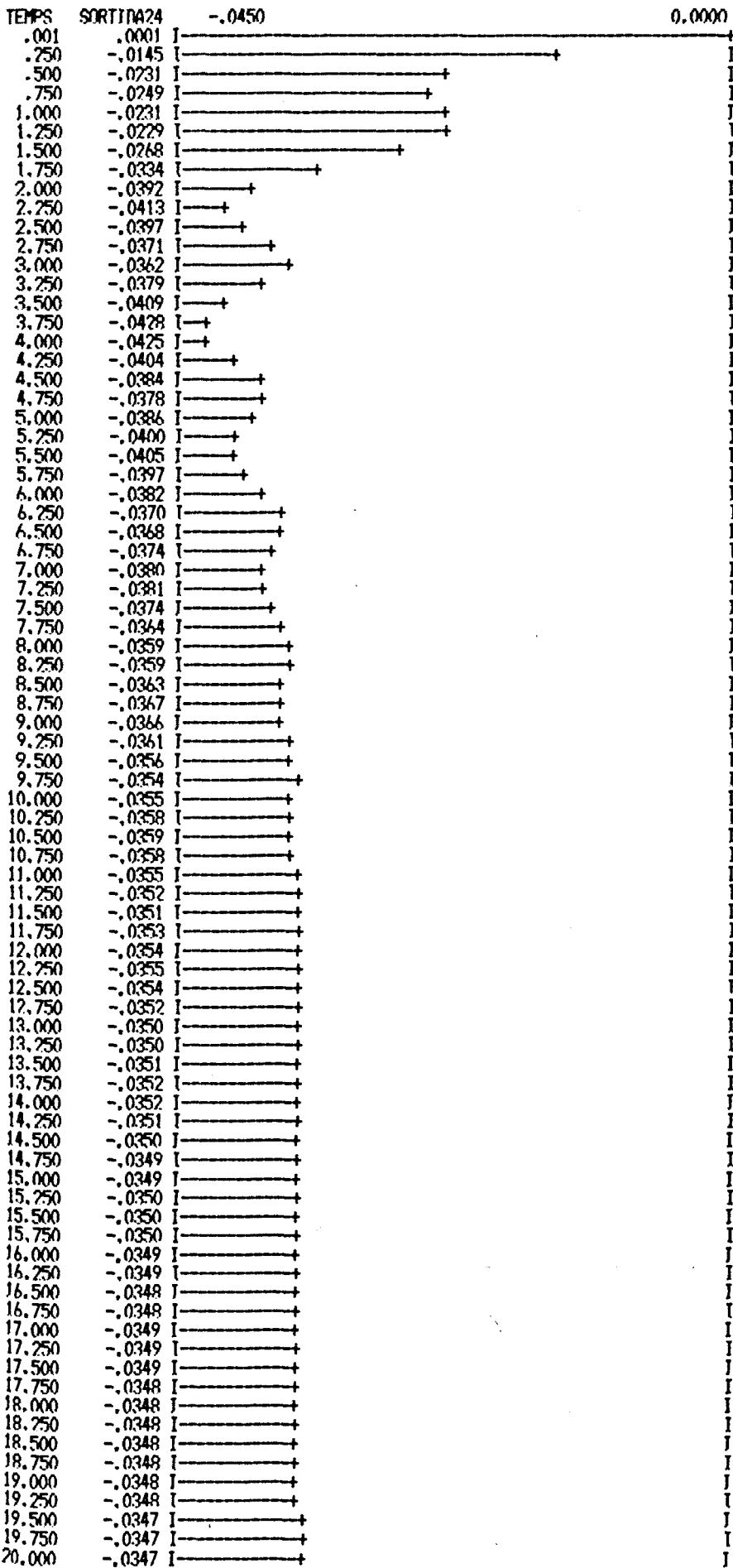


TEMPS	SORTINA24	SORTINA30	SORTINA20	SORTINA27
.00	.0001	.0001	.0001	.0001
.50	-.0231	-.0068	-.0003	-.0068
1.00	-.0231	-.0773	-.0003	-.0110
1.50	-.0268	-.0340	.0001	-.0059
2.00	-.0392	-.0309	.0003	-.0064
2.50	-.0397	-.0380	.0006	-.0104
3.00	-.0362	-.0431	.0010	-.0083
3.50	-.0409	-.0390	.0013	-.0064
4.00	-.0475	-.0388	.0015	-.0089
4.50	-.0384	-.0472	.0018	-.0087
5.00	-.0386	-.0400	.0020	-.0067
5.50	-.0405	-.0376	.0021	-.0075
6.00	-.0382	-.0391	.0022	-.0083
6.50	-.0368	-.0388	.0023	-.0070
7.00	-.0380	-.0366	.0024	-.0069
7.50	-.0374	-.0369	.0024	-.0077
8.00	-.0359	-.0374	.0025	-.0072
8.50	-.0363	-.0361	.0025	-.0068
9.00	-.0366	-.0357	.0025	-.0072
9.50	-.0356	-.0363	.0025	-.0073
10.00	-.0355	-.0359	.0026	-.0068
10.50	-.0359	-.0353	.0026	-.0070
11.00	-.0355	-.0356	.0026	-.0072
11.50	-.0351	-.0356	.0026	-.0070
12.00	-.0354	-.0352	.0026	-.0069
12.50	-.0354	-.0352	.0026	-.0071
13.00	-.0350	-.0353	.0026	-.0070
13.50	-.0351	-.0351	.0026	-.0069
14.00	-.0352	-.0350	.0026	-.0070
14.50	-.0350	-.0351	.0026	-.0070
15.00	-.0349	-.0350	.0027	-.0069
15.50	-.0350	-.0349	.0027	-.0069
16.00	-.0349	-.0349	.0027	-.0070
16.50	-.0348	-.0349	.0027	-.0069
17.00	-.0349	-.0348	.0027	-.0069
17.50	-.0349	-.0348	.0027	-.0069
18.00	-.0348	-.0348	.0027	-.0069
18.50	-.0348	-.0348	.0027	-.0069
19.00	-.0348	-.0347	.0027	-.0069
19.50	-.0347	-.0348	.0027	-.0069
20.00	-.0347	-.0347	.0027	-.0069
20.50	-.0347	-.0347	.0027	-.0069
21.00	-.0347	-.0347	.0027	-.0069
21.50	-.0347	-.0347	.0027	-.0069
22.00	-.0347	-.0347	.0027	-.0069
22.50	-.0347	-.0347	.0027	-.0069
23.00	-.0347	-.0347	.0027	-.0069
23.50	-.0346	-.0347	.0027	-.0069
24.00	-.0346	-.0346	.0027	-.0069
24.50	-.0346	-.0346	.0027	-.0069
25.00	-.0346	-.0346	.0027	-.0069
25.50	-.0346	-.0346	.0027	-.0069
26.00	-.0346	-.0346	.0027	-.0069
26.50	-.0346	-.0346	.0027	-.0069
27.00	-.0346	-.0346	.0027	-.0069
27.50	-.0346	-.0346	.0027	-.0069
28.00	-.0346	-.0346	.0027	-.0069
28.50	-.0346	-.0346	.0027	-.0069
29.00	-.0346	-.0346	.0027	-.0069
29.50	-.0346	-.0346	.0027	-.0069
30.00	-.0346	-.0346	.0027	-.0069
30.50	-.0346	-.0346	.0027	-.0069
31.00	-.0346	-.0346	.0027	-.0069
31.50	-.0346	-.0346	.0027	-.0069
32.00	-.0346	-.0346	.0027	-.0069
32.50	-.0346	-.0346	.0027	-.0069
33.00	-.0346	-.0346	.0027	-.0069
33.50	-.0346	-.0346	.0027	-.0069
34.00	-.0346	-.0346	.0027	-.0069
34.50	-.0346	-.0346	.0027	-.0069
35.00	-.0346	-.0346	.0027	-.0069
35.50	-.0346	-.0346	.0027	-.0069
36.00	-.0346	-.0346	.0027	-.0069
36.50	-.0346	-.0346	.0027	-.0069
37.00	-.0346	-.0346	.0027	-.0069
37.50	-.0346	-.0346	.0027	-.0069
38.00	-.0346	-.0346	.0027	-.0069
38.50	-.0346	-.0346	.0027	-.0069
39.00	-.0346	-.0346	.0027	-.0069
39.50	-.0346	-.0346	.0027	-.0069
40.00	-.0346	-.0346	.0027	-.0069

R S - 35

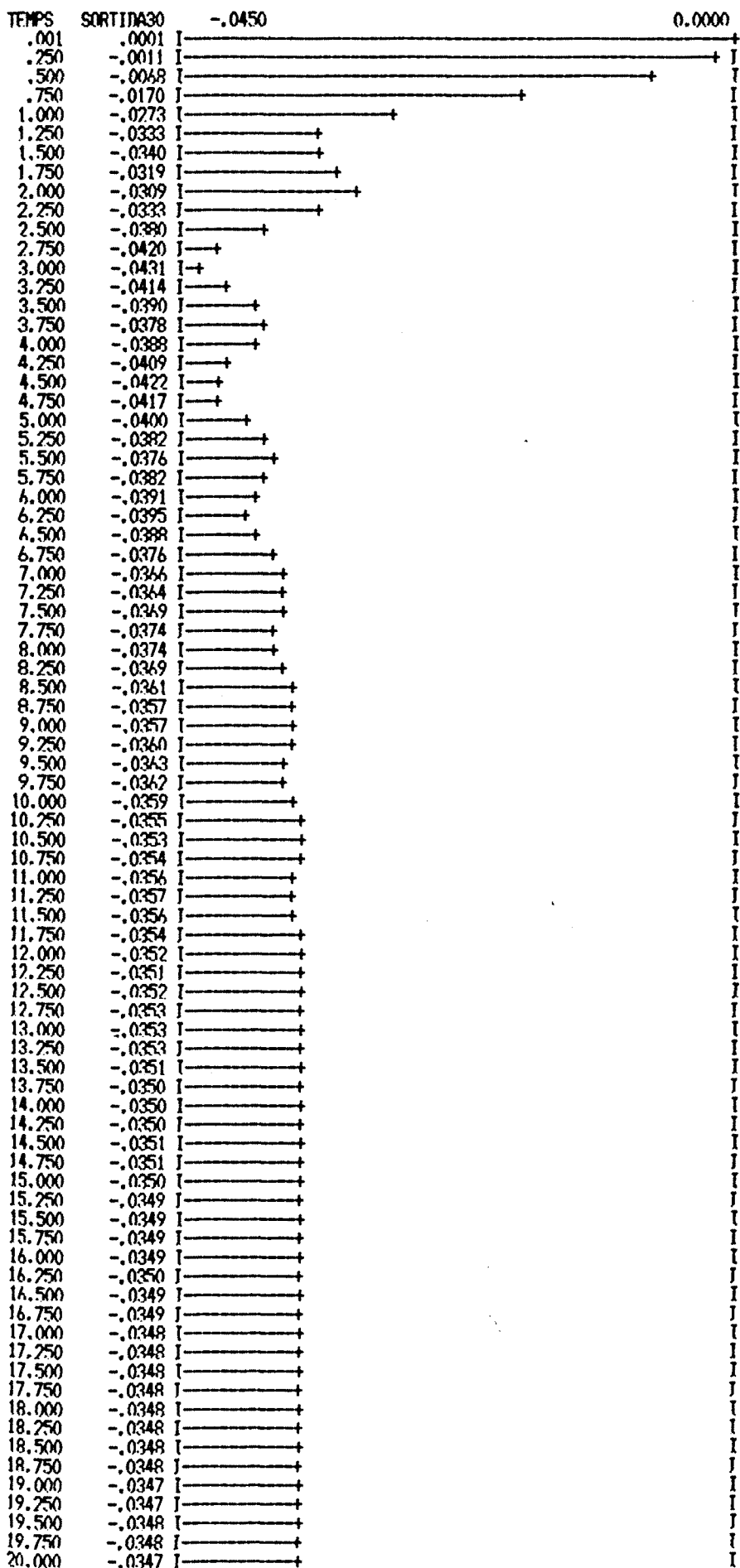
$$T_{ie} = \underline{1,155} \text{ p.u.MW} \times \text{seg.} / \text{HZ}$$

BLOC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



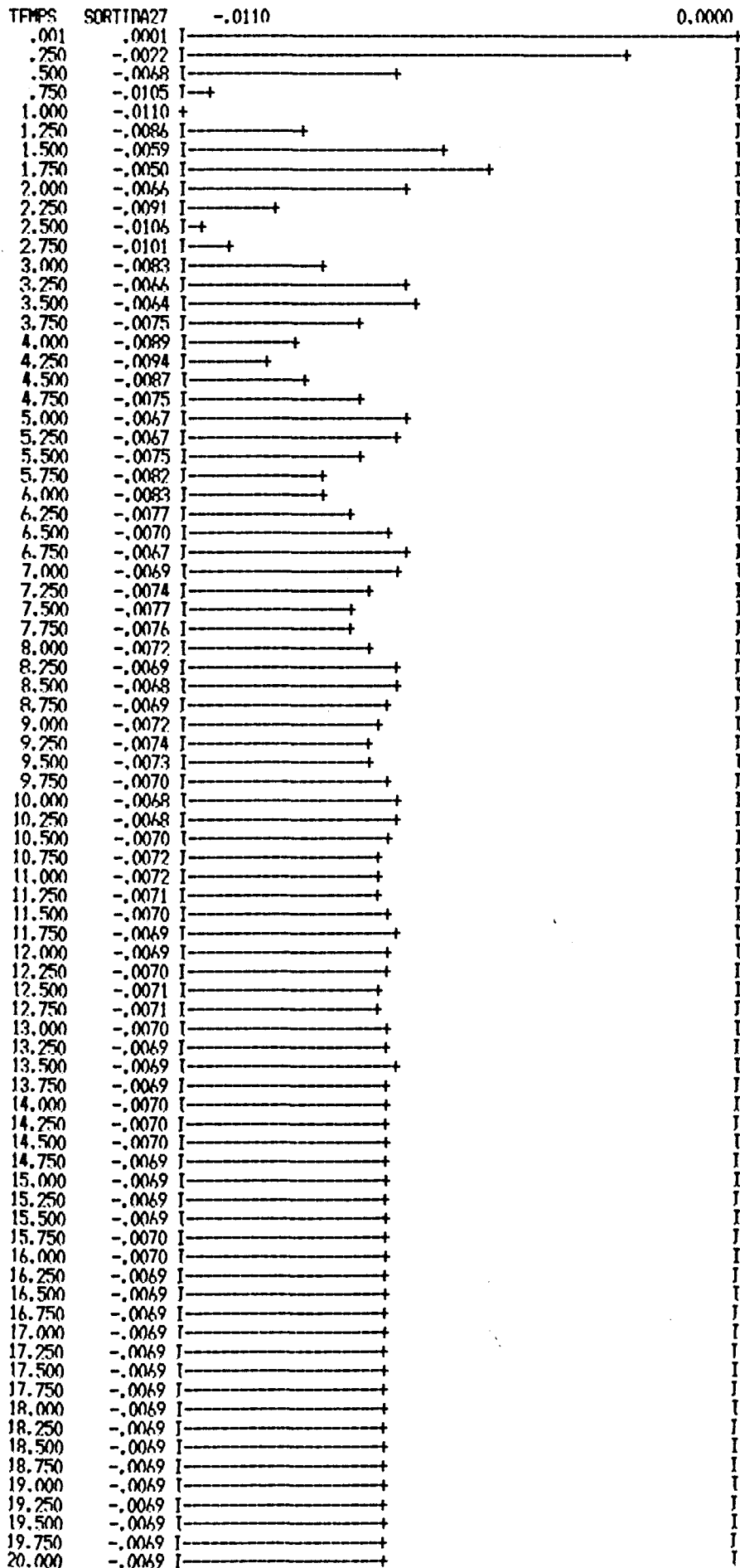
RS - 36

BLOC FIX Y (30) MINIM (-.0450) MAXIM (0.0000)



RS - 37

BI OC. FIX Y (27) MINIM (-.0110) MAXIM (0.0000)



TFMPS	SORTIDA24	SORTIDA30	SORTIDA27	SORTIDA38
.00	.0001	.0001	.0001	.0001
.50	-.0231	-.0048	-.0068	-.0001
1.00	-.0232	-.0279	-.0109	-.0005
1.50	-.0277	-.0351	-.0055	-.0007
2.00	-.0411	-.0318	-.0064	-.0002
2.50	-.0410	-.0384	-.0111	.0006
3.00	-.0354	-.0427	-.0088	.0012
3.50	-.0384	-.0359	-.0069	.0022
4.00	-.0374	-.0326	-.0100	.0034
4.50	-.0291	-.0331	-.0101	.0043
5.00	-.0255	-.0271	-.0078	.0052
5.50	-.0241	-.0202	-.0089	.0062
6.00	-.0177	-.0185	-.0101	.0069
6.50	-.0124	-.0150	-.0087	.0075
7.00	-.0111	-.0093	-.0084	.0081
7.50	-.0081	-.0070	-.0096	.0085
8.00	-.0041	-.0061	-.0092	.0087
8.50	-.0033	-.0032	-.0085	.0088
9.00	-.0030	-.0015	-.0092	.0090
9.50	-.0012	-.0020	-.0094	.0089
10.00	-.0009	-.0015	-.0088	.0089
10.50	-.0019	-.0009	-.0090	.0088
11.00	-.0019	-.0018	-.0095	.0087
11.50	-.0019	-.0026	-.0092	.0086
12.00	-.0030	-.0026	-.0091	.0085
12.50	-.0037	-.0033	-.0094	.0085
13.00	-.0039	-.0043	-.0094	.0084
13.50	-.0046	-.0046	-.0092	.0083
14.00	-.0053	-.0049	-.0094	.0083
14.50	-.0054	-.0055	-.0095	.0083
15.00	-.0056	-.0058	-.0094	.0082
15.50	-.0060	-.0058	-.0094	.0083
16.00	-.0061	-.0060	-.0095	.0083
16.50	-.0060	-.0061	-.0095	.0083
17.00	-.0060	-.0060	-.0094	.0083
17.50	-.0060	-.0059	-.0095	.0084
18.00	-.0058	-.0059	-.0095	.0084
18.50	-.0057	-.0057	-.0095	.0084
19.00	-.0056	-.0055	-.0095	.0085
19.50	-.0054	-.0054	-.0096	.0085
20.00	-.0053	-.0053	-.0095	.0085
20.50	-.0052	-.0052	-.0095	.0085
21.00	-.0051	-.0051	-.0095	.0086
21.50	-.0050	-.0050	-.0095	.0086
22.00	-.0050	-.0050	-.0095	.0086
22.50	-.0049	-.0049	-.0095	.0086
23.00	-.0049	-.0049	-.0096	.0086
23.50	-.0049	-.0049	-.0095	.0086
24.00	-.0049	-.0049	-.0096	.0086
24.50	-.0049	-.0049	-.0096	.0086
25.00	-.0049	-.0049	-.0096	.0086
25.50	-.0049	-.0049	-.0096	.0086
26.00	-.0049	-.0049	-.0096	.0086
26.50	-.0049	-.0049	-.0096	.0086
27.00	-.0049	-.0049	-.0096	.0086
27.50	-.0050	-.0049	-.0096	.0086
28.00	-.0050	-.0050	-.0096	.0086
28.50	-.0050	-.0050	-.0096	.0086
29.00	-.0050	-.0050	-.0096	.0086
29.50	-.0050	-.0050	-.0096	.0086
30.00	-.0050	-.0050	-.0096	.0086
30.50	-.0050	-.0050	-.0096	.0086
31.00	-.0050	-.0049	-.0096	.0086
31.50	-.0049	-.0049	-.0096	.0086
32.00	-.0049	-.0049	-.0096	.0086
32.50	-.0049	-.0049	-.0096	.0086
33.00	-.0049	-.0049	-.0096	.0086
33.50	-.0049	-.0049	-.0096	.0086
34.00	-.0049	-.0049	-.0096	.0086
34.50	-.0049	-.0049	-.0096	.0086
35.00	-.0049	-.0049	-.0096	.0086
35.50	-.0049	-.0049	-.0096	.0086
36.00	-.0049	-.0049	-.0096	.0086
36.50	-.0049	-.0049	-.0096	.0086
37.00	-.0049	-.0049	-.0096	.0086
37.50	-.0049	-.0049	-.0096	.0086
38.00	-.0049	-.0049	-.0096	.0086
38.50	-.0049	-.0049	-.0096	.0086
39.00	-.0049	-.0049	-.0096	.0086
39.50	-.0049	-.0049	-.0096	.0086
40.00	-.0049	-.0049	-.0096	.0086

RS - 39

$\Delta P_1 = 0,01 \text{ p.u.MW}$

$\Delta P_2 = 0$

$T_{ie} = 1,155 \text{ p.u.MW} \times \text{seg} / \text{Hz}$

20: GENERACION AREA 1

24: FRECUENCIA AREA 1

38: GENERACION AREA 2

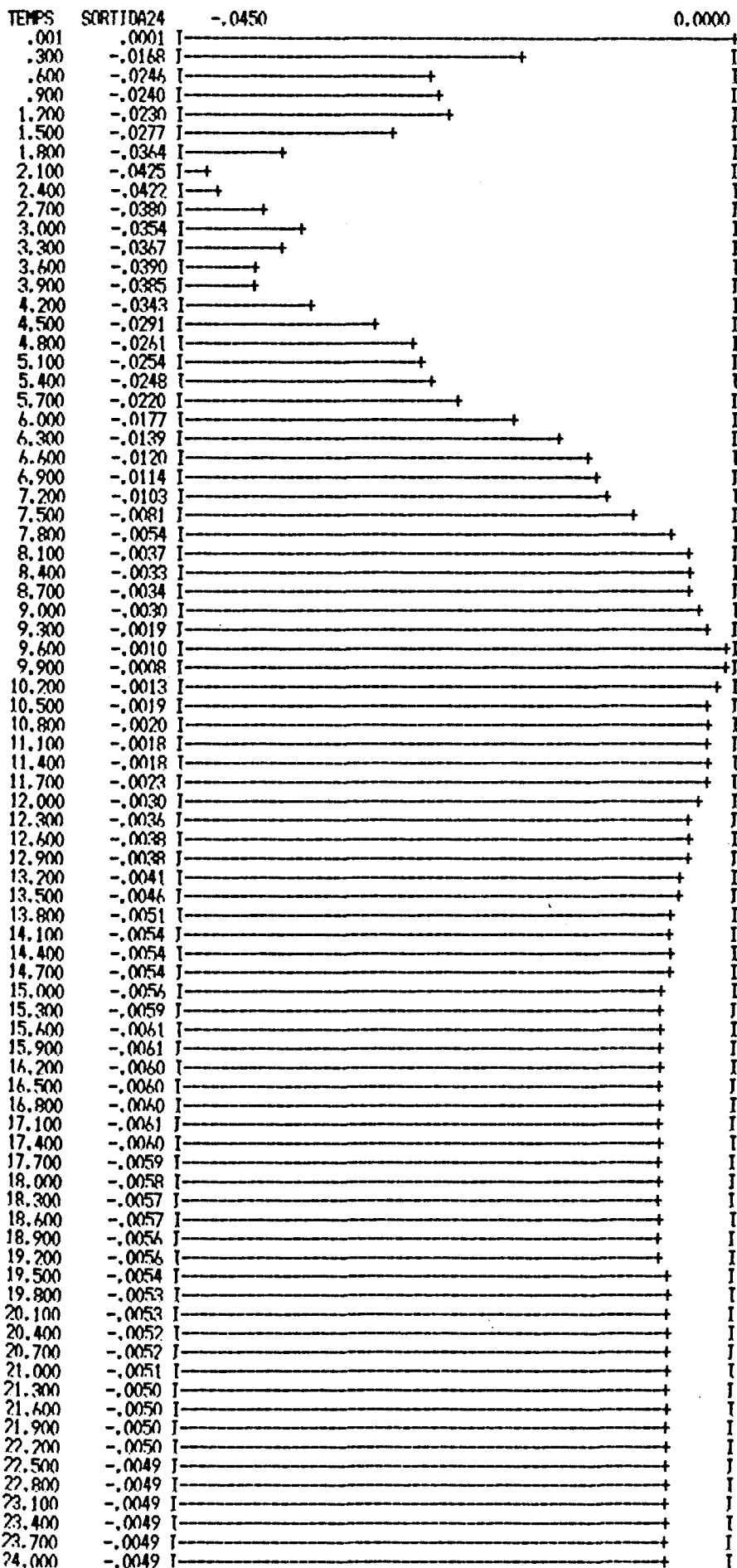
30: FRECUENCIA AREA 2

27: INTERCONEXION

TEMPS	SDRTIDA20	SDRTIDA38	SDRTIDA27	SDRTIDA22
.00	.0001	.0001	.0001	-.0100
.50	-.0003	-.0001	-.0068	-.0036
1.00	-.0003	-.0005	-.0109	.0007
1.50	.0001	-.0007	-.0055	-.0045
2.00	.0003	-.0002	-.0064	-.0035
2.50	.0006	.0006	-.0111	.0016
3.00	.0011	.0012	-.0088	-.0003
3.50	.0014	.0022	-.0049	-.0018
4.00	.0016	.0034	-.0100	.0015
4.50	.0019	.0043	-.0101	.0020
5.00	.0021	.0052	-.0078	-.0003
5.50	.0021	.0062	-.0089	.0009
6.00	.0021	.0069	-.0101	.0022
6.50	.0021	.0075	-.0087	.0007
7.00	.0019	.0081	-.0084	.0003
7.50	.0018	.0085	-.0096	.0014
8.00	.0016	.0087	-.0092	.0008
8.50	.0015	.0088	-.0085	-.0002
9.00	.0013	.0090	-.0092	.0004
9.50	.0011	.0089	-.0094	.0005
10.00	.0010	.0089	-.0088	-.0003
10.50	.0008	.0088	-.0090	-.0003
11.00	.0007	.0087	-.0095	.0002
11.50	.0007	.0086	-.0092	-.0003
12.00	.0006	.0085	-.0091	-.0005
12.50	.0005	.0085	-.0094	-.0002
13.00	.0005	.0084	-.0094	-.0002
13.50	.0005	.0083	-.0092	-.0004
14.00	.0005	.0083	-.0094	-.0003
14.50	.0005	.0083	-.0095	-.0001
15.00	.0005	.0082	-.0094	-.0003
15.50	.0005	.0083	-.0094	-.0002
16.00	.0005	.0083	-.0095	-.0001
16.50	.0005	.0083	-.0095	-.0001
17.00	.0005	.0083	-.0094	-.0002
17.50	.0005	.0084	-.0095	-.0001
18.00	.0005	.0084	-.0095	-.0001
18.50	.0005	.0084	-.0095	-.0001
19.00	.0005	.0085	-.0095	-.0001
19.50	.0005	.0085	-.0096	-.0001
20.00	.0005	.0085	-.0095	-.0001
20.50	.0005	.0085	-.0095	-.0001
21.00	.0005	.0086	-.0095	-.0001
21.50	.0005	.0086	-.0095	-.0001
22.00	.0005	.0086	-.0095	-.0001
22.50	.0005	.0086	-.0095	-.0001
23.00	.0005	.0086	-.0096	-.0001
23.50	.0005	.0086	-.0095	-.0001
24.00	.0005	.0086	-.0096	-.0001
24.50	.0005	.0086	-.0096	-.0001
25.00	.0005	.0086	-.0096	-.0001
25.50	.0005	.0086	-.0096	-.0001
26.00	.0005	.0086	-.0096	-.0001
26.50	.0005	.0086	-.0096	-.0001
27.00	.0004	.0086	-.0096	-.0001
27.50	.0004	.0086	-.0096	-.0001
28.00	.0004	.0086	-.0096	-.0001
28.50	.0004	.0086	-.0096	-.0001
29.00	.0004	.0086	-.0096	-.0001
29.50	.0004	.0086	-.0096	-.0001
30.00	.0004	.0086	-.0096	-.0001
30.50	.0004	.0086	-.0096	-.0001
31.00	.0004	.0086	-.0096	-.0001
31.50	.0004	.0086	-.0096	-.0001
32.00	.0004	.0086	-.0096	-.0001
32.50	.0004	.0086	-.0096	-.0001
33.00	.0004	.0086	-.0096	-.0001
33.50	.0004	.0086	-.0096	-.0001
34.00	.0004	.0086	-.0096	-.0001
34.50	.0004	.0086	-.0096	-.0001
35.00	.0004	.0086	-.0096	-.0001
35.50	.0004	.0086	-.0096	-.0001
36.00	.0004	.0086	-.0096	-.0001
36.50	.0004	.0086	-.0096	-.0001
37.00	.0004	.0086	-.0096	-.0001
37.50	.0004	.0086	-.0096	-.0001
38.00	.0004	.0086	-.0096	-.0001
38.50	.0004	.0086	-.0096	-.0001
39.00	.0004	.0086	-.0096	-.0001
39.50	.0004	.0086	-.0096	-.0001
40.00	.0004	.0086	-.0096	-.0001

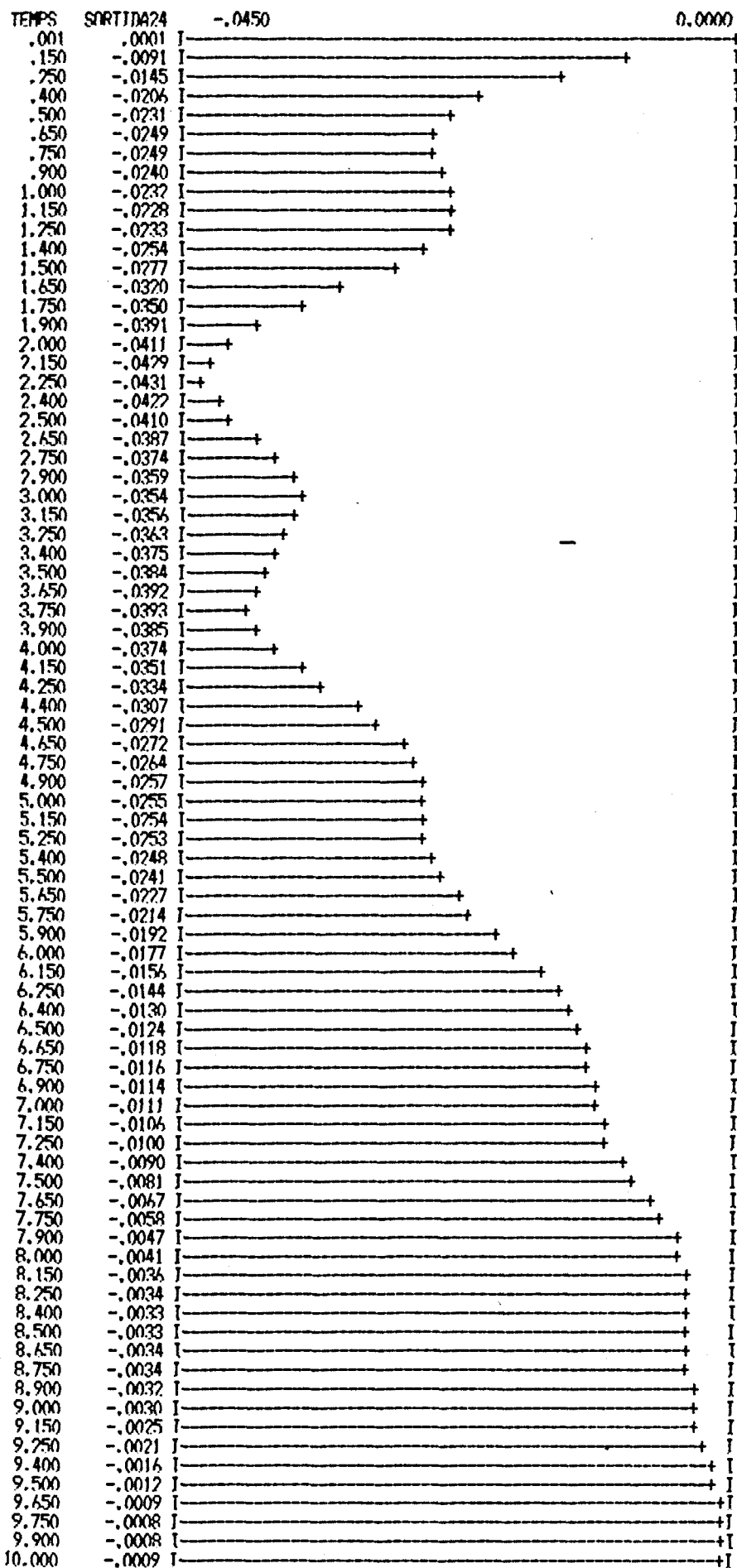
RS - 40

BLDC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



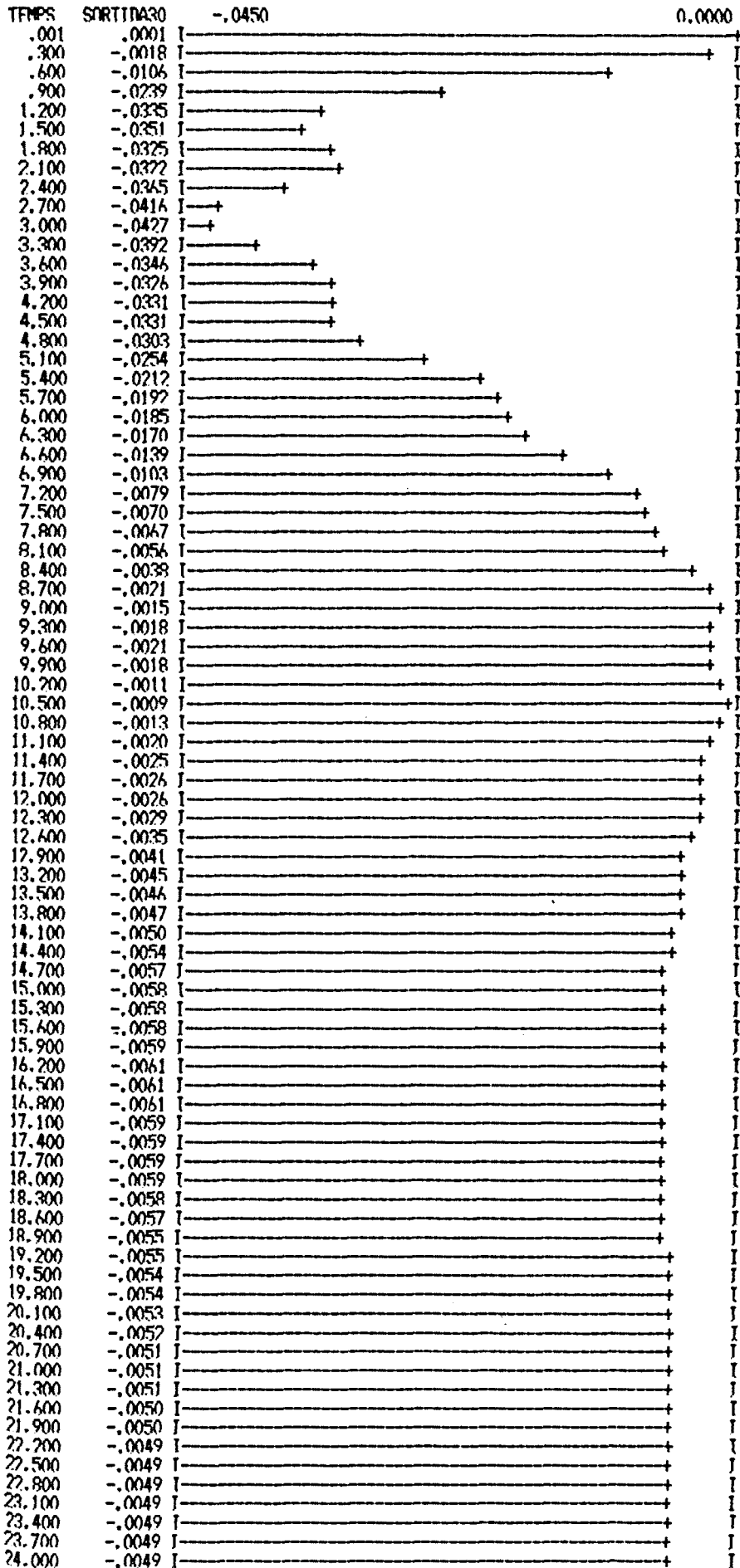
RS - 41

BLOC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



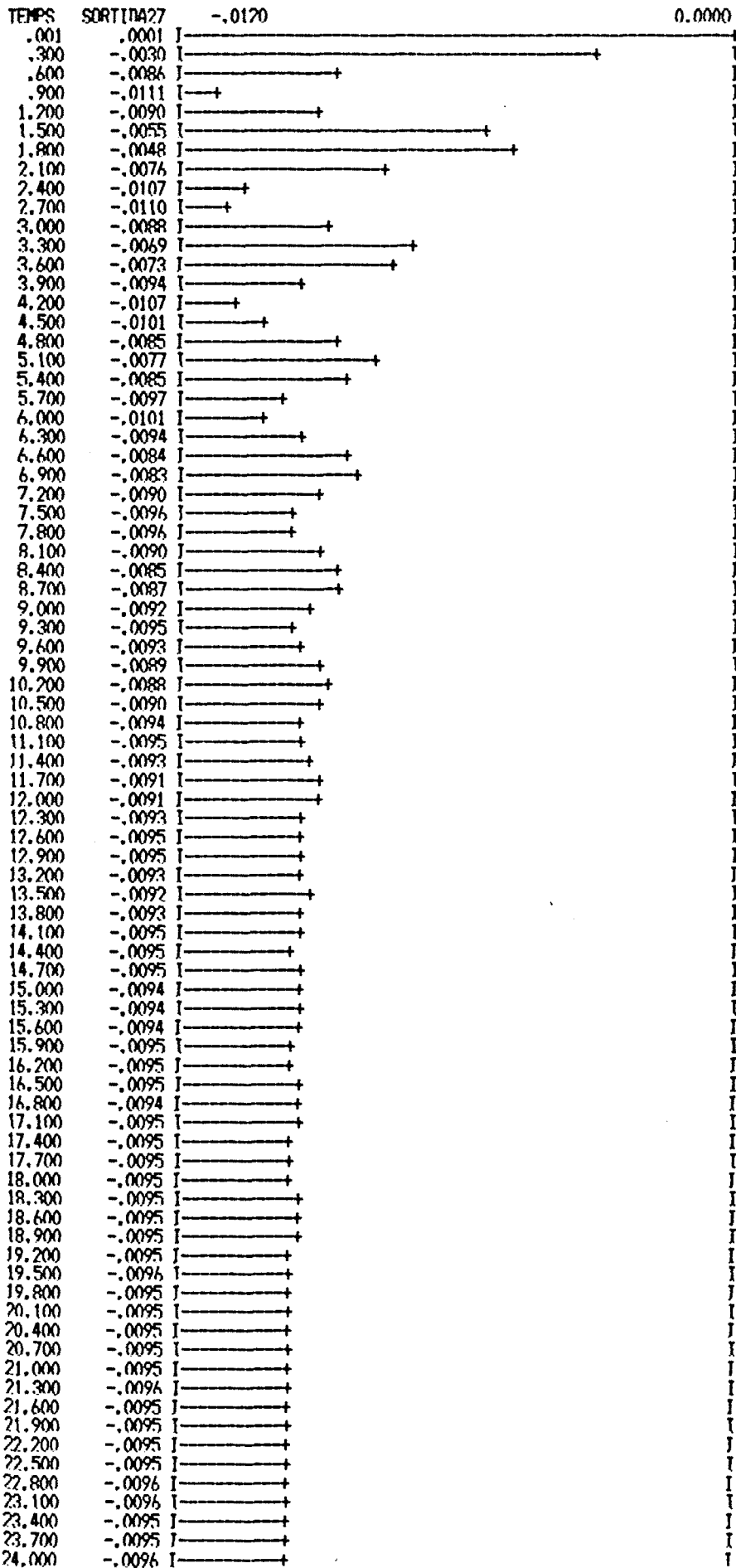
RS - 42

BLOC FIX Y (30) MINIM (-.0450) MAXIM (0.0000)



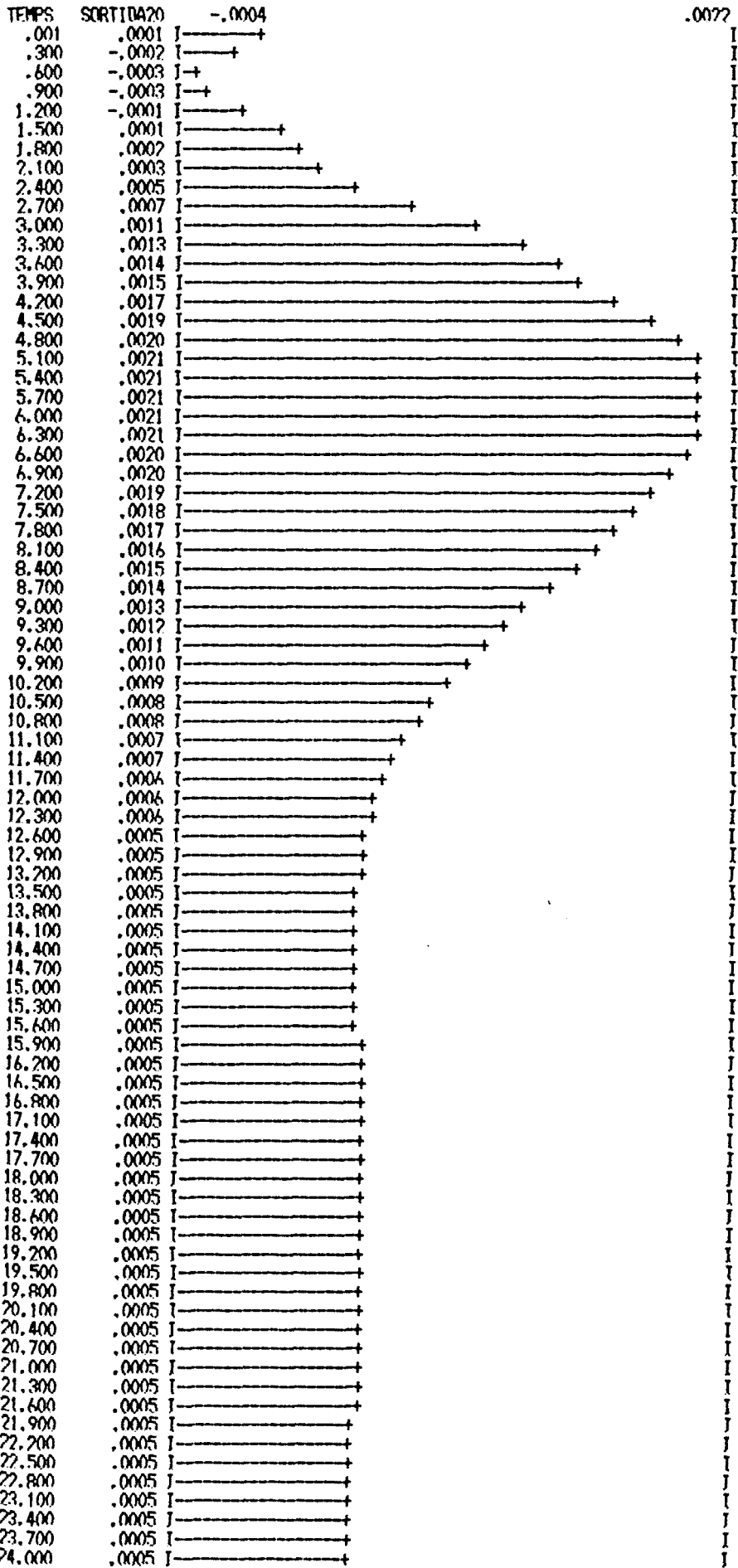
RS - 43

PLAC. FIX Y (27) MINIM (-.0120) MAXIM (0.0000)



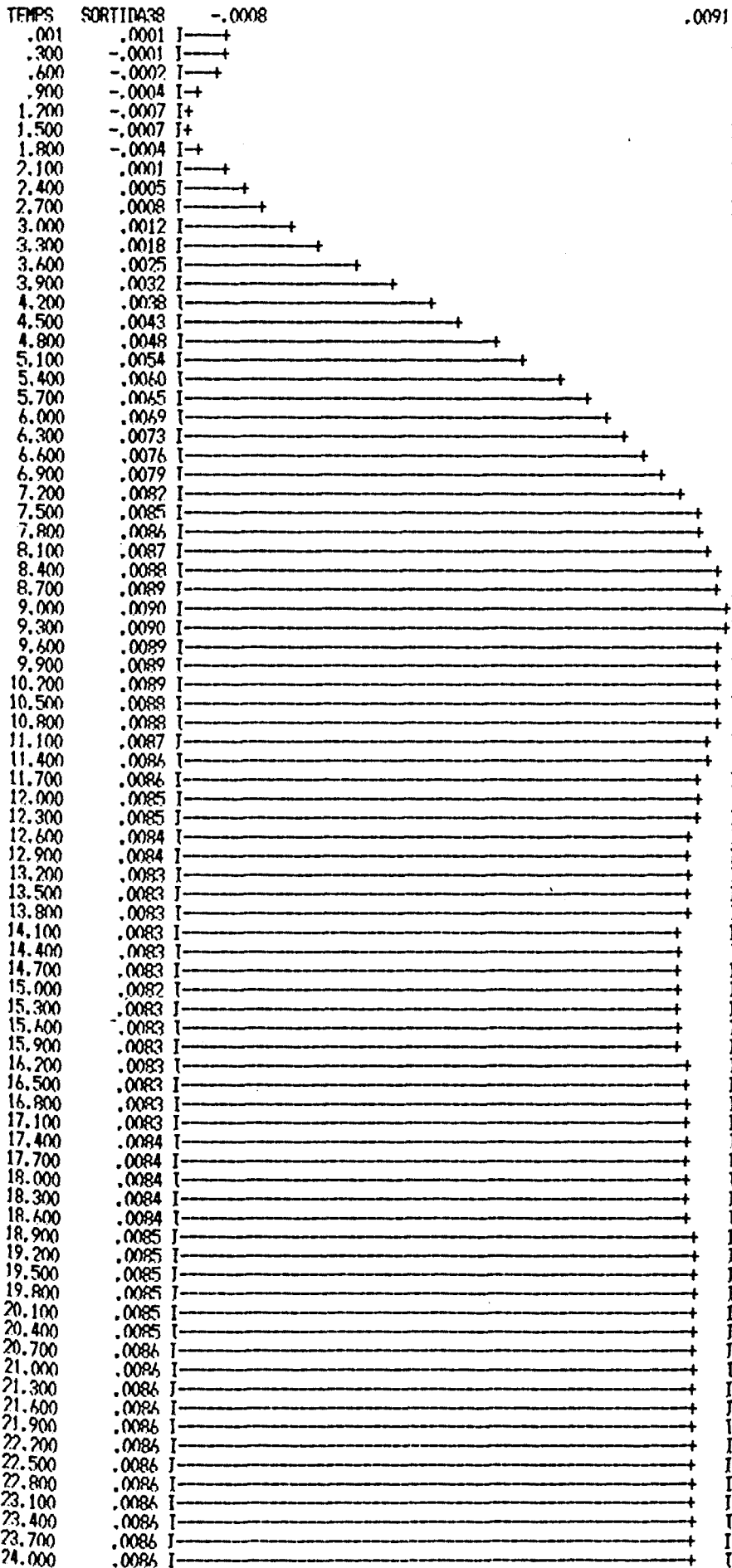
RS - 44

BLD FIX Y (20) MINIM (-.0004) MAXIM (.0022)



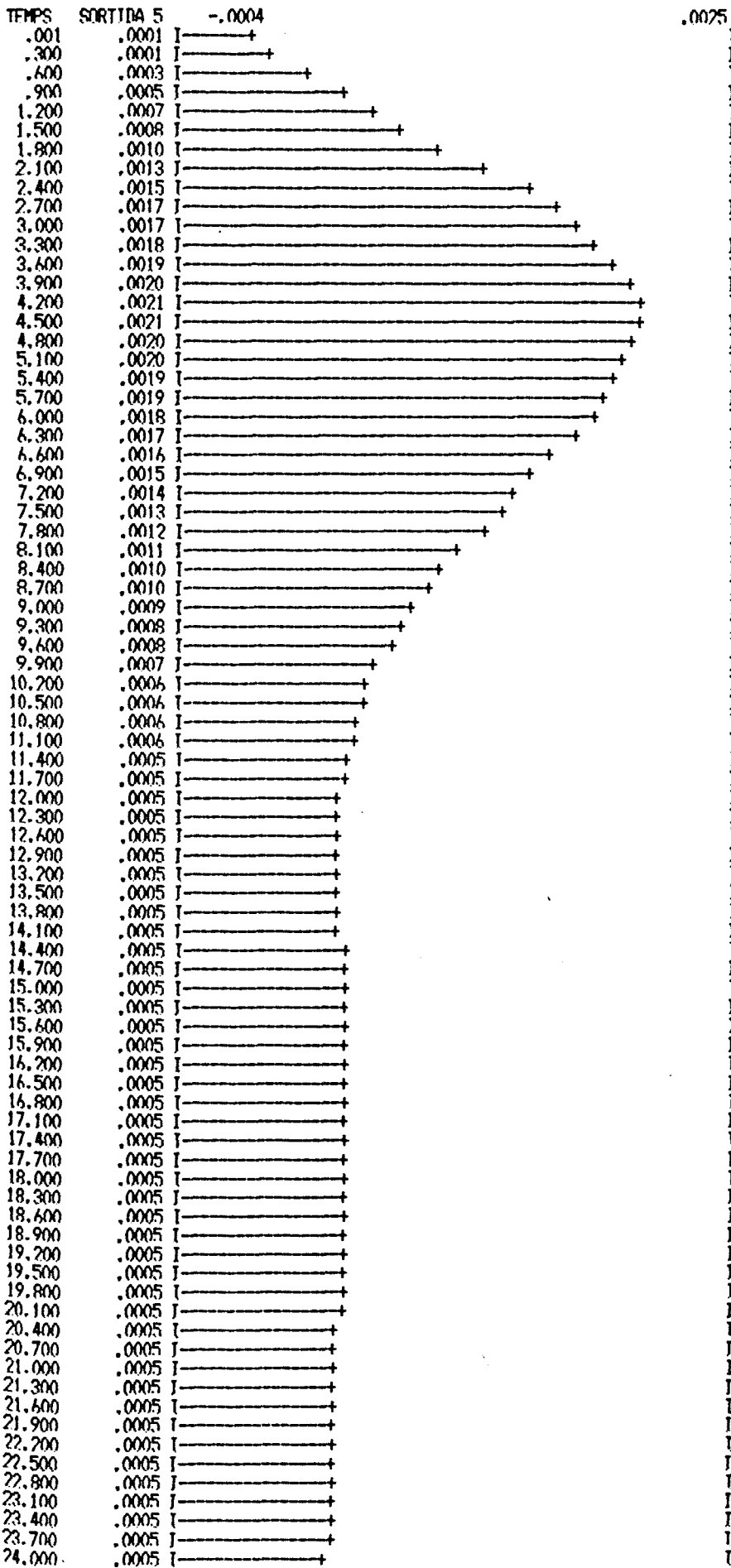
RS - 45

RLOC FIX Y (38) MINIM (-.0008) MAXIM (.0091)



RS - 46

BLOC. EIX Y (5) MINIM (-.0004) MAXIM (.0025)



RS - 47

APERTURA DISTRIBUIDOR AREA 1

TEMPS	SORTINA24	SORTINA30	SORTINA27	SORTINA38
.00	.0001	.0001	.0001	.0001
.50	-.0068	-.0179	.0056	-.0004
1.00	-.0279	-.0179	.0060	-.0004
1.50	-.0351	-.0286	-.0006	-.0002
2.00	-.0318	-.0405	.0009	-.0001
2.50	-.0384	-.0375	.0041	.0005
3.00	-.0427	-.0355	.0006	.0015
3.50	-.0359	-.0395	-.0007	.0023
4.00	-.0326	-.0359	.0023	.0033
4.50	-.0331	-.0285	.0016	.0044
5.00	-.0271	-.0268	-.0005	.0053
5.50	-.0202	-.0240	.0011	.0061
6.00	-.0185	-.0169	.0019	.0069
6.50	-.0150	-.0131	.0004	.0076
7.00	-.0093	-.0116	.0006	.0081
7.50	-.0070	-.0075	.0017	.0084
8.00	-.0061	-.0041	.0010	.0087
8.50	-.0032	-.0038	-.0005	.0089
9.00	-.0015	-.0027	.0013	.0089
9.50	-.0020	-.0009	.0012	.0090
10.00	-.0016	-.0011	.0006	.0089
10.50	-.0009	-.0018	.0009	.0088
11.00	-.0018	-.0015	.0012	.0088
11.50	-.0026	-.0019	.0007	.0087
12.00	-.0026	-.0030	.0007	.0086
12.50	-.0033	-.0035	.0009	.0085
13.00	-.0043	-.0037	.0008	.0084
13.50	-.0046	-.0046	.0006	.0083
14.00	-.0049	-.0052	.0007	.0083
14.50	-.0055	-.0053	.0007	.0083
15.00	-.0058	-.0056	.0006	.0083
15.50	-.0058	-.0060	.0006	.0083
16.00	-.0060	-.0060	.0007	.0083
16.50	-.0061	-.0059	.0006	.0083
17.00	-.0060	-.0061	.0006	.0083
17.50	-.0059	-.0060	.0006	.0084
18.00	-.0059	-.0057	.0006	.0084
18.50	-.0057	-.0057	.0005	.0084
19.00	-.0055	-.0056	.0006	.0085
19.50	-.0054	-.0054	.0006	.0085
20.00	-.0053	-.0053	.0006	.0085
20.50	-.0052	-.0052	.0006	.0086
21.00	-.0051	-.0051	.0006	.0086
21.50	-.0050	-.0050	.0006	.0086
22.00	-.0050	-.0050	.0005	.0086
22.50	-.0049	-.0049	.0006	.0086
23.00	-.0049	-.0049	.0006	.0086
23.50	-.0049	-.0049	.0005	.0086
24.00	-.0049	-.0049	.0005	.0086
24.50	-.0049	-.0049	.0005	.0086
25.00	-.0049	-.0049	.0005	.0086
25.50	-.0049	-.0049	.0005	.0086
26.00	-.0049	-.0049	.0005	.0086
26.50	-.0049	-.0049	.0005	.0086
27.00	-.0049	-.0049	.0005	.0086
27.50	-.0049	-.0049	.0005	.0086
28.00	-.0050	-.0049	.0005	.0086
28.50	-.0050	-.0050	.0005	.0086
29.00	-.0050	-.0050	.0005	.0086
29.50	-.0050	-.0050	.0005	.0086
30.00	-.0050	-.0050	.0005	.0086
30.50	-.0050	-.0050	.0005	.0086
31.00	-.0049	-.0049	.0005	.0086
31.50	-.0049	-.0049	.0005	.0086
32.00	-.0049	-.0049	.0005	.0086
32.50	-.0049	-.0049	.0005	.0086
33.00	-.0049	-.0049	.0005	.0086
33.50	-.0049	-.0049	.0005	.0086
34.00	-.0049	-.0049	.0005	.0086
34.50	-.0049	-.0049	.0005	.0086
35.00	-.0049	-.0049	.0005	.0086
35.50	-.0049	-.0049	.0005	.0086
36.00	-.0049	-.0049	.0005	.0086
36.50	-.0049	-.0049	.0005	.0086
37.00	-.0049	-.0049	.0005	.0086
37.50	-.0049	-.0049	.0005	.0086
38.00	-.0049	-.0049	.0005	.0086
38.50	-.0049	-.0049	.0005	.0086
39.00	-.0049	-.0049	.0005	.0086
39.50	-.0049	-.0049	.0005	.0086
40.00	-.0049	-.0049	.0005	.0086

RS - 48

$$\Delta P_1 = 0$$

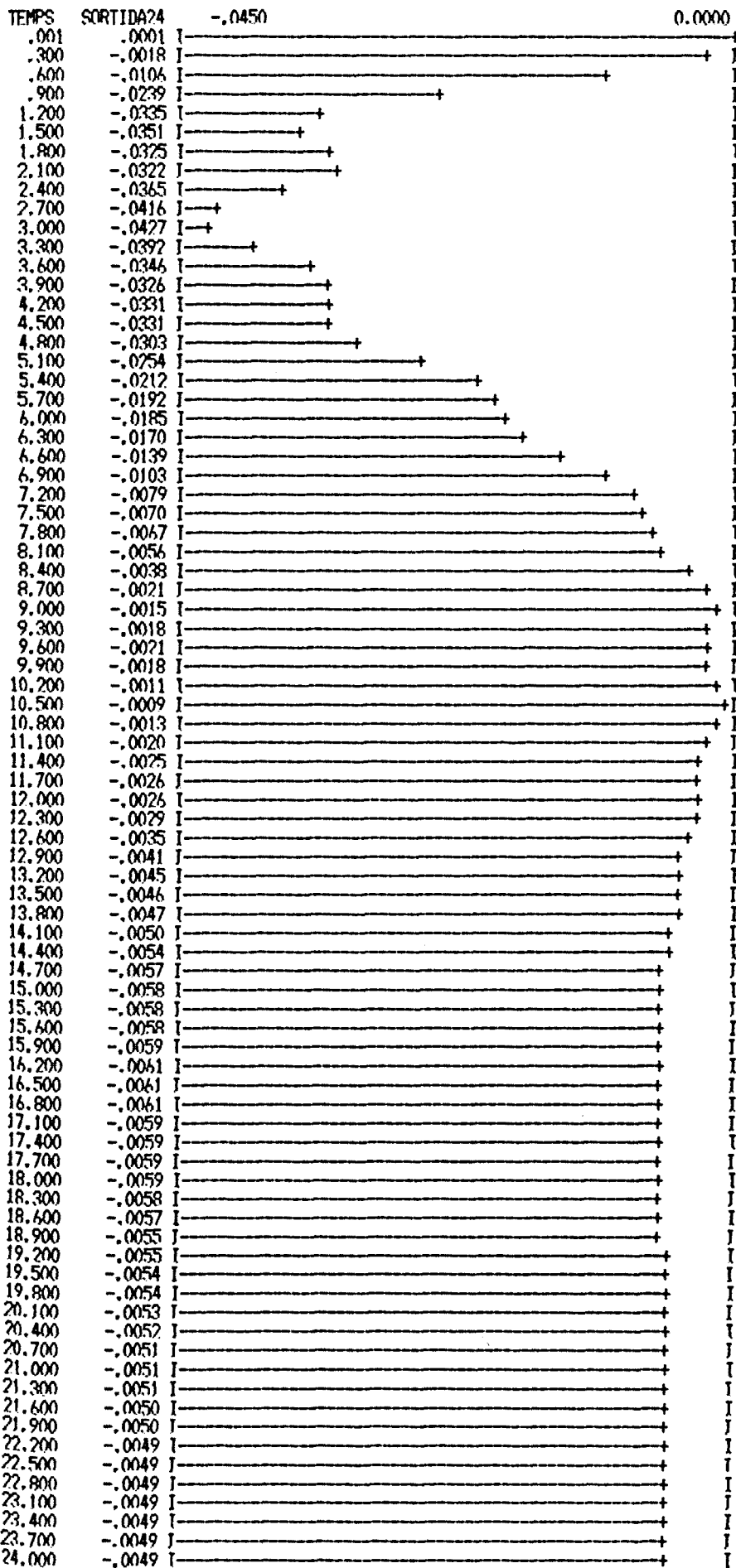
$$\Delta P_2 = 0,01 \text{ p.u.MW}$$

$$T_{ie} = 1,155 \text{ p.u.MW} \times \text{seg./Hz.}$$

TEMPS	SORTIDA20	SORTIDA38	SORTIDA27	SORTIDA28
.00	.0001	.0001	.0001	-.0100
.50	-.0001	-.0004	.0056	-.0049
1.00	-.0003	-.0004	.0060	-.0045
1.50	-.0003	-.0002	-.0006	-.0108
2.00	.0002	-.0001	.0009	-.0093
2.50	.0006	.0005	.0041	-.0055
3.00	.0008	.0015	.0006	-.0080
3.50	.0012	.0023	-.0007	-.0084
4.00	.0016	.0033	.0023	-.0046
4.50	.0018	.0044	.0016	-.0042
5.00	.0019	.0053	-.0005	-.0052
5.50	.0021	.0061	.0011	-.0029
6.00	.0021	.0069	.0019	-.0013
6.50	.0020	.0076	.0004	-.0021
7.00	.0019	.0081	.0006	-.0015
7.50	.0018	.0084	.0017	.0001
8.00	.0016	.0087	.0010	-.0004
8.50	.0014	.0089	.0005	-.0007
9.00	.0013	.0089	.0013	.0002
9.50	.0011	.0090	.0012	.0002
10.00	.0009	.0089	.0006	-.0006
10.50	.0008	.0088	.0009	-.0004
11.00	.0007	.0088	.0012	-.0002
11.50	.0006	.0087	.0007	-.0007
12.00	.0006	.0086	.0007	-.0009
12.50	.0005	.0085	.0009	-.0008
13.00	.0005	.0084	.0008	-.0010
13.50	.0005	.0083	.0006	-.0012
14.00	.0005	.0083	.0007	-.0011
14.50	.0005	.0083	.0007	-.0011
15.00	.0005	.0083	.0006	-.0013
15.50	.0005	.0083	.0006	-.0013
16.00	.0005	.0083	.0007	-.0012
16.50	.0005	.0083	.0006	-.0012
17.00	.0005	.0083	.0006	-.0013
17.50	.0005	.0084	.0006	-.0011
18.00	.0005	.0084	.0006	-.0011
18.50	.0005	.0084	.0005	-.0012
19.00	.0005	.0085	.0006	-.0011
19.50	.0005	.0085	.0006	-.0010
20.00	.0005	.0085	.0006	-.0011
20.50	.0005	.0086	.0006	-.0010
21.00	.0005	.0086	.0006	-.0010
21.50	.0005	.0086	.0006	-.0010
22.00	.0005	.0086	.0005	-.0010
22.50	.0005	.0086	.0006	-.0010
23.00	.0005	.0086	.0006	-.0010
23.50	.0005	.0086	.0005	-.0010
24.00	.0005	.0086	.0005	-.0010
24.50	.0005	.0086	.0005	-.0010
25.00	.0005	.0086	.0005	-.0010
25.50	.0005	.0086	.0005	-.0010
26.00	.0005	.0086	.0005	-.0010
26.50	.0004	.0086	.0005	-.0010
27.00	.0004	.0086	.0005	-.0010
27.50	.0004	.0086	.0005	-.0010
28.00	.0004	.0086	.0005	-.0010
28.50	.0004	.0086	.0005	-.0010
29.00	.0004	.0086	.0005	-.0010
29.50	.0004	.0086	.0005	-.0010
30.00	.0004	.0086	.0005	-.0010
30.50	.0004	.0086	.0005	-.0010
31.00	.0004	.0086	.0005	-.0010
31.50	.0004	.0086	.0005	-.0010
32.00	.0004	.0086	.0005	-.0010
32.50	.0004	.0086	.0005	-.0010
33.00	.0004	.0086	.0005	-.0010
33.50	.0004	.0086	.0005	-.0010
34.00	.0004	.0086	.0005	-.0010
34.50	.0004	.0086	.0005	-.0010
35.00	.0004	.0086	.0005	-.0010
35.50	.0004	.0086	.0005	-.0010
36.00	.0004	.0086	.0005	-.0010
36.50	.0004	.0086	.0005	-.0010
37.00	.0004	.0086	.0005	-.0010
37.50	.0004	.0086	.0005	-.0010
38.00	.0004	.0086	.0005	-.0010
38.50	.0004	.0086	.0005	-.0010
39.00	.0004	.0086	.0005	-.0010
39.50	.0004	.0086	.0005	-.0010
40.00	.0004	.0086	.0005	-.0010

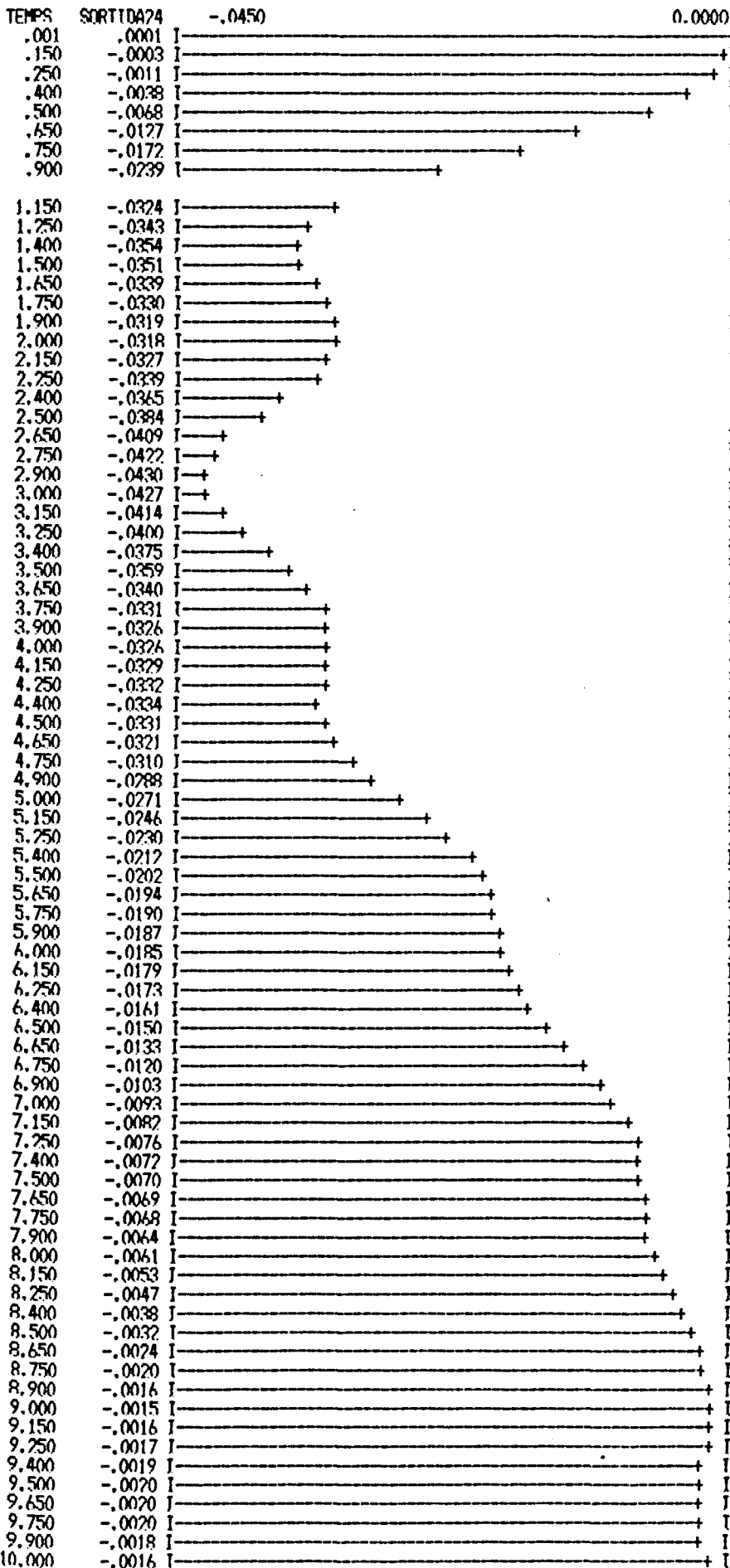
RS - 49

BLOC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



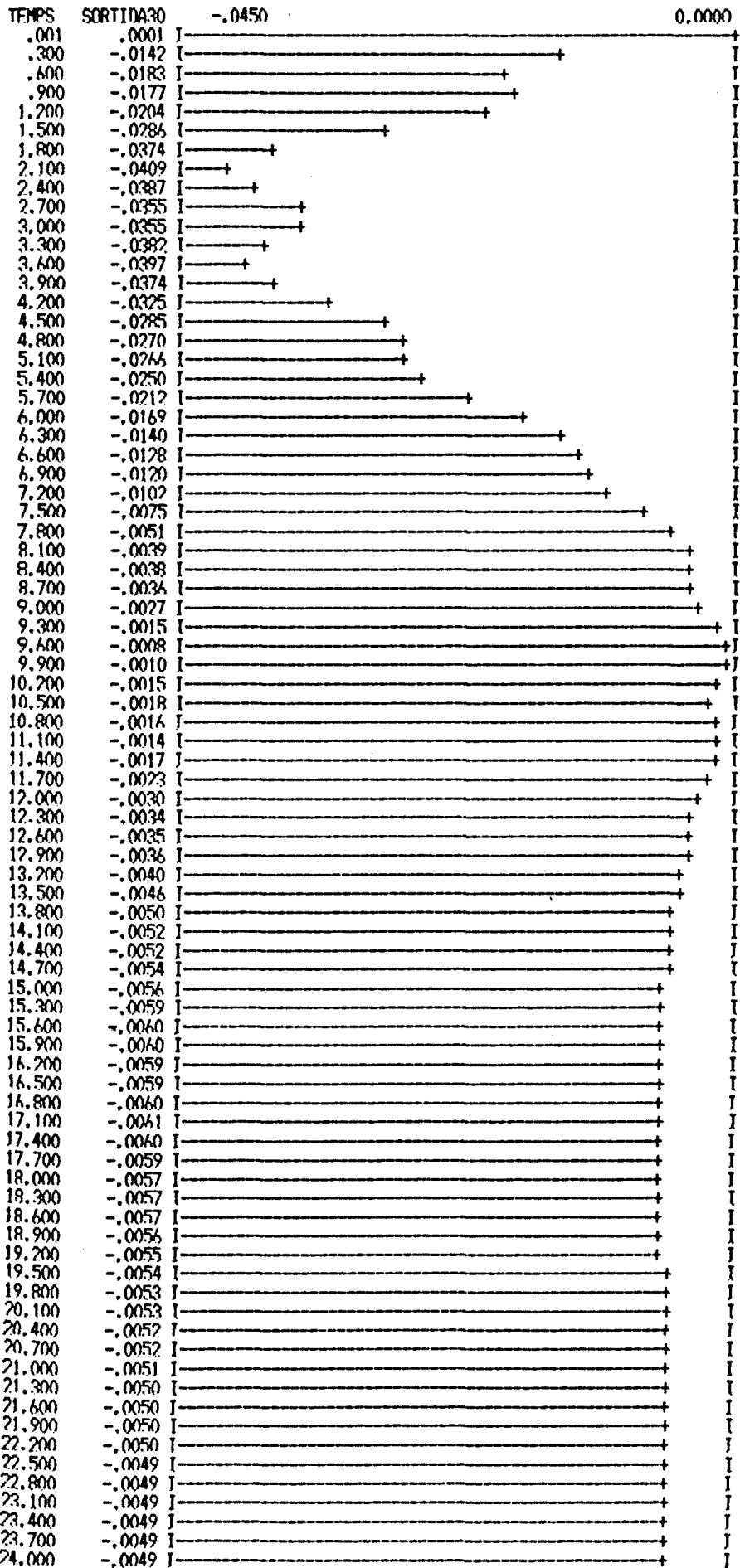
RS - 50

BLOC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



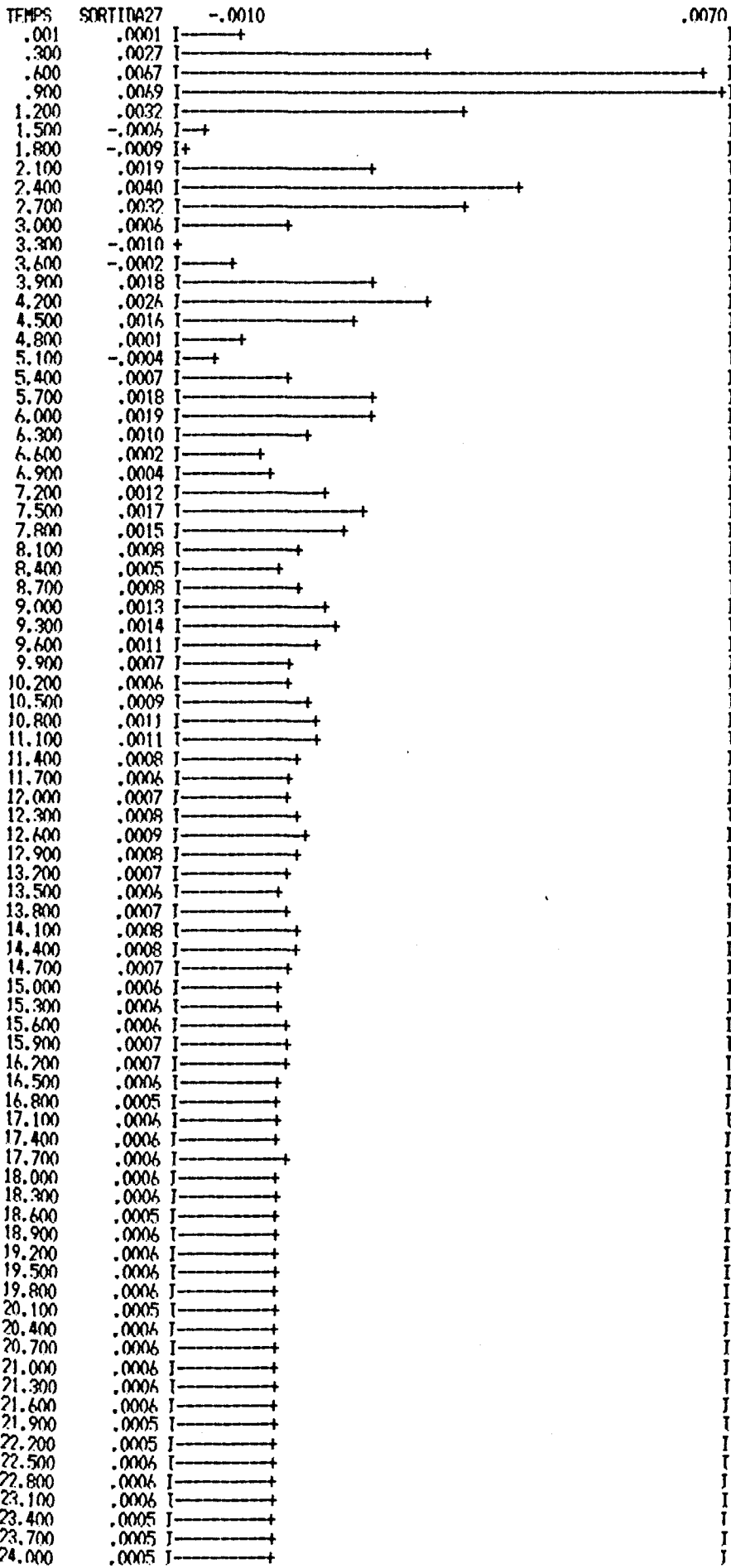
RS - 51

MINOC EIX Y (30) MINIM (-.0450) MAXIM (0.0000)



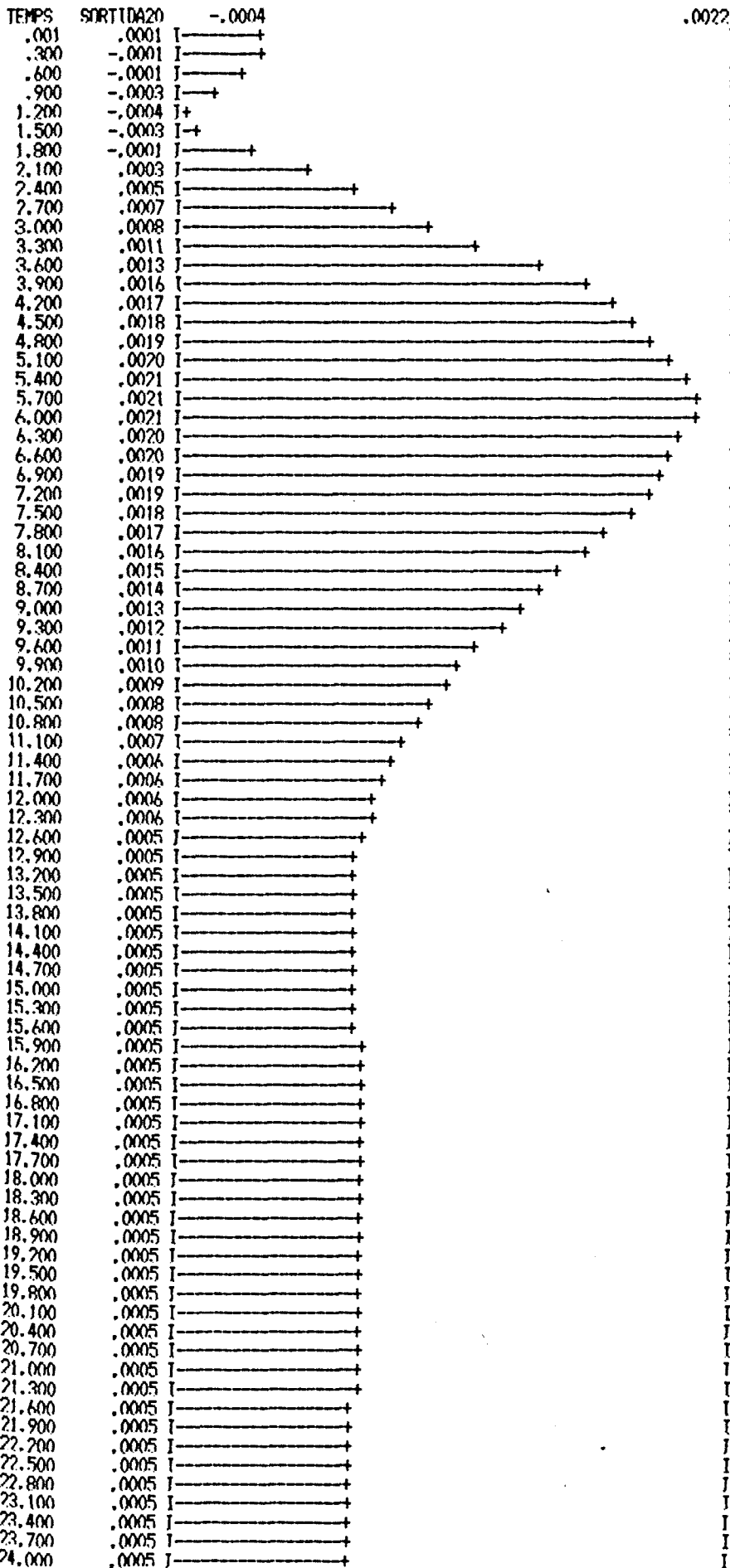
R S - 52

BLOC FIX Y (27) MINIM (-.0010) MAXIM (.0070)



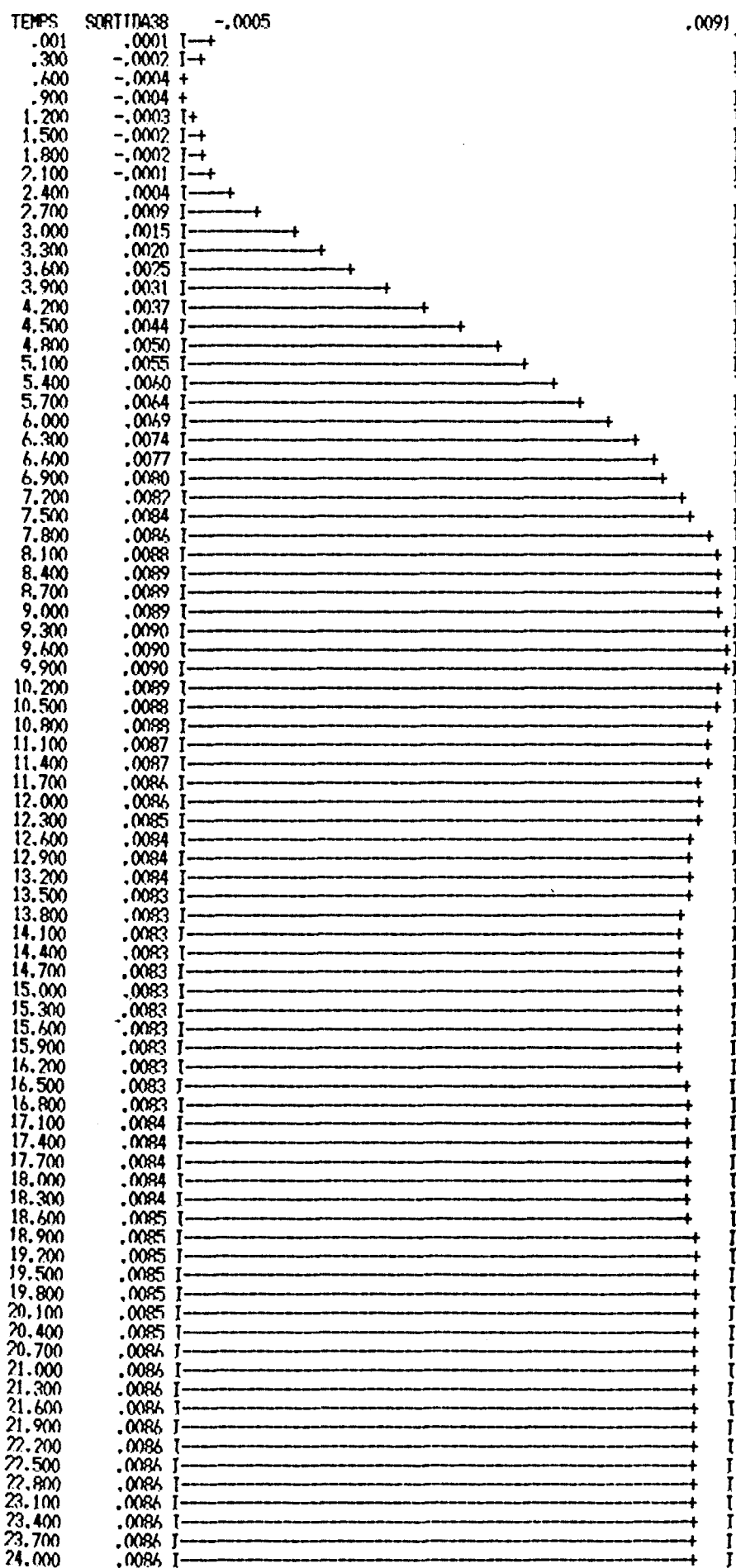
R S - 53

BLOC FIX Y (20) MINIM (-.0004) MAXIM (.0022)



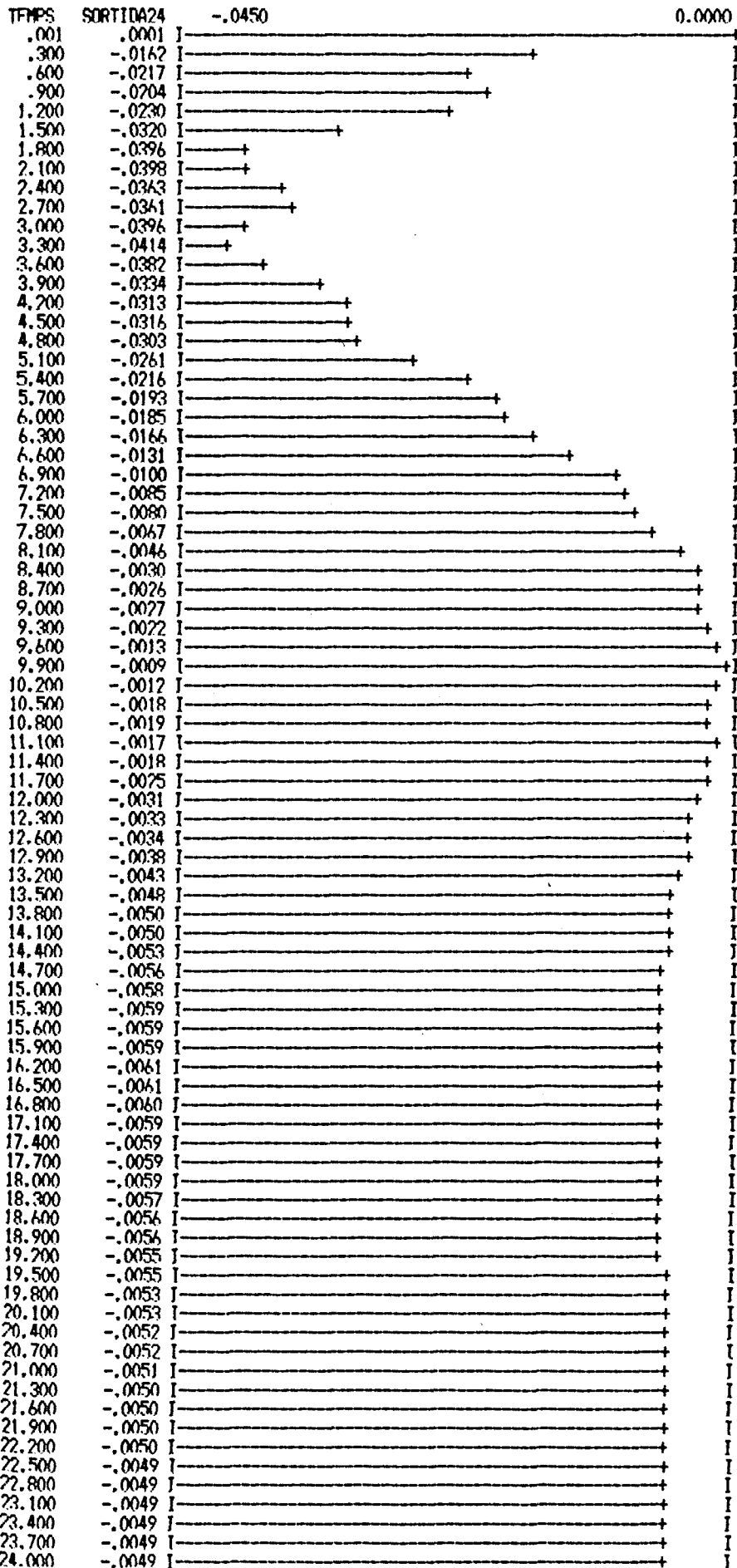
RS - 54

BLOC EIX Y (38) MINIM (-.0005) MAXIM (.0091)



R S - 55

BLOC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



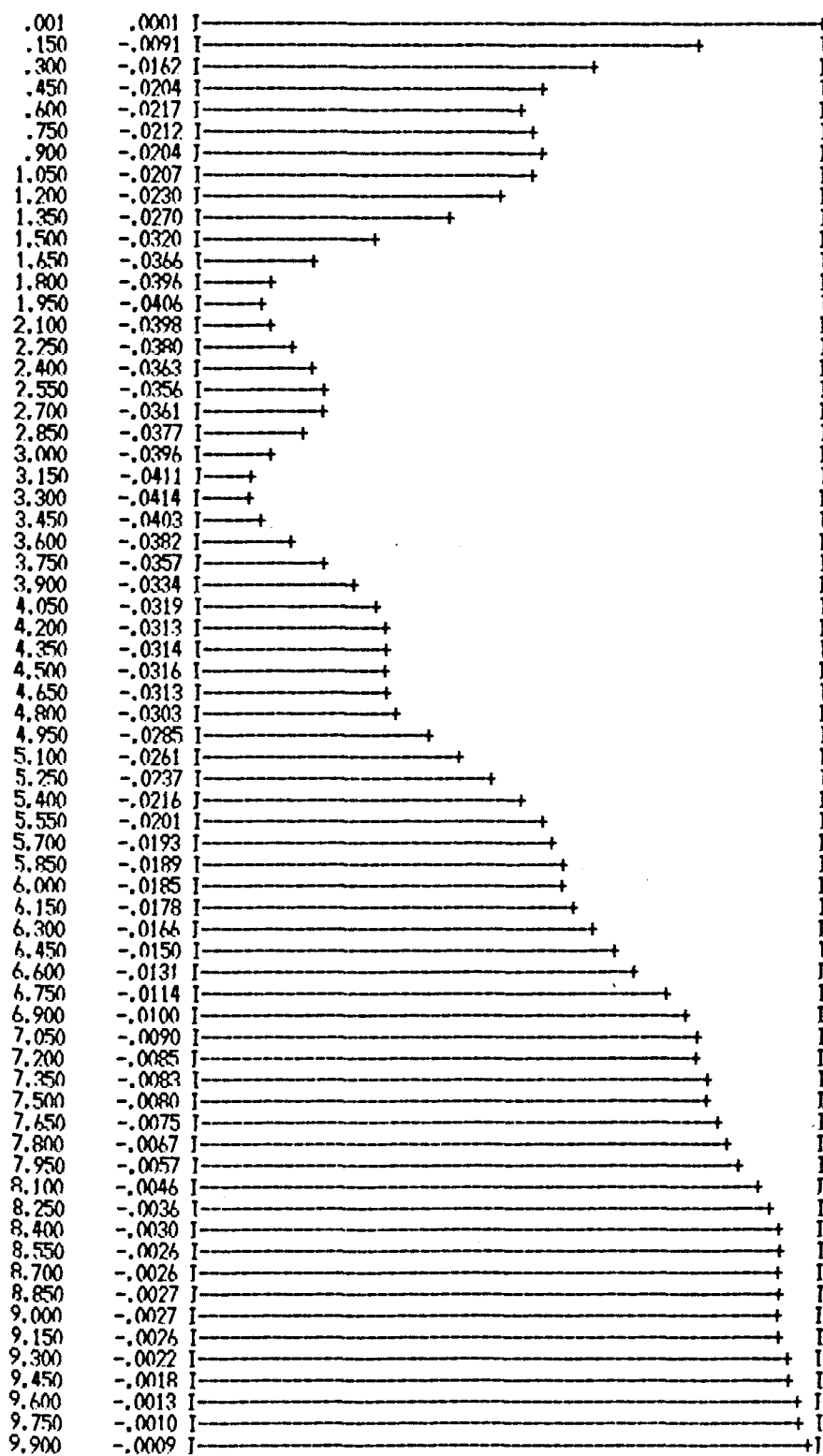
RS - 56

$\Delta P_1 = 0,01 \text{ p.u. Mw}$

$\Delta P_2 = 0$

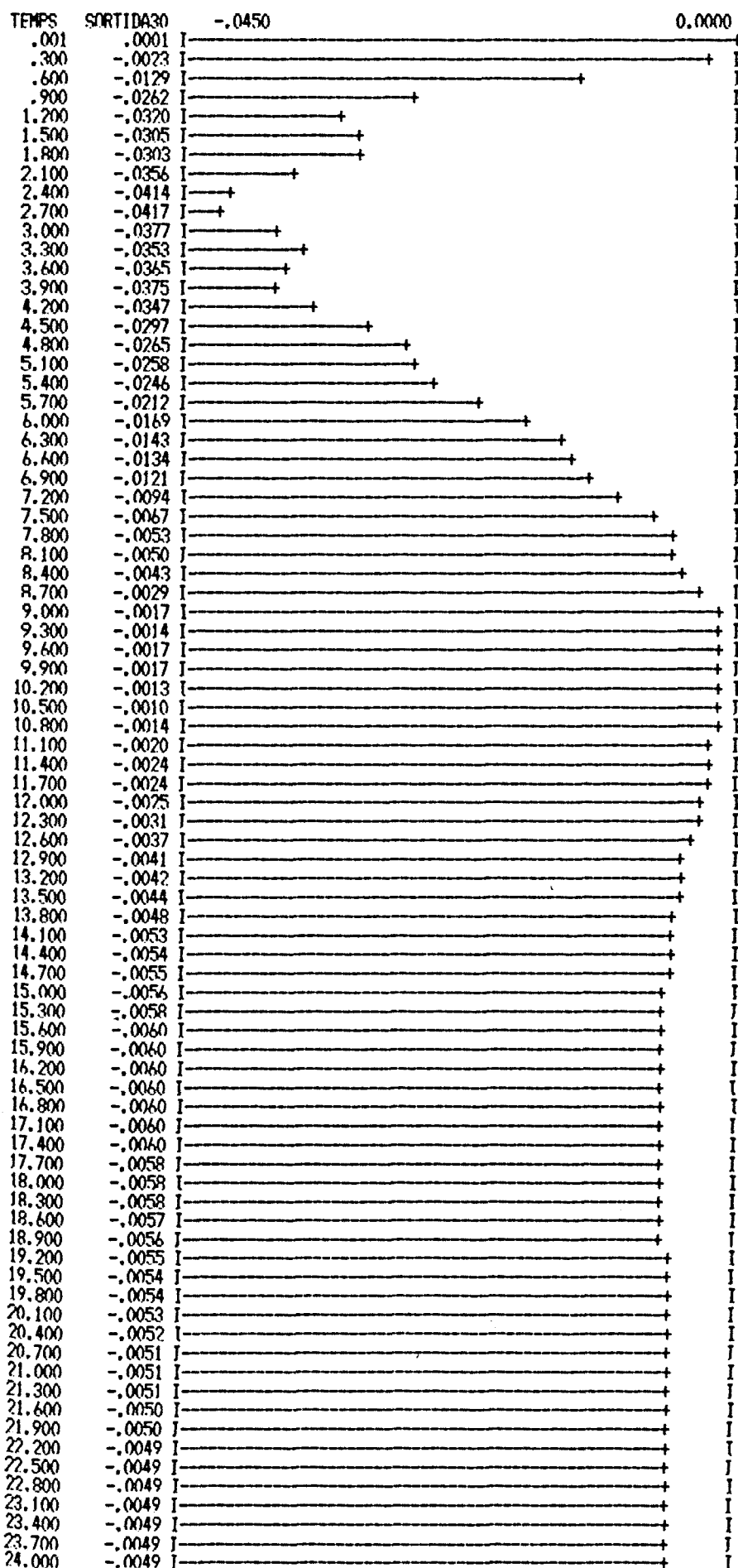
$T_{ie} = 1,53 \text{ p.u.MW} \times \text{seg.} / 1$

BLOC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



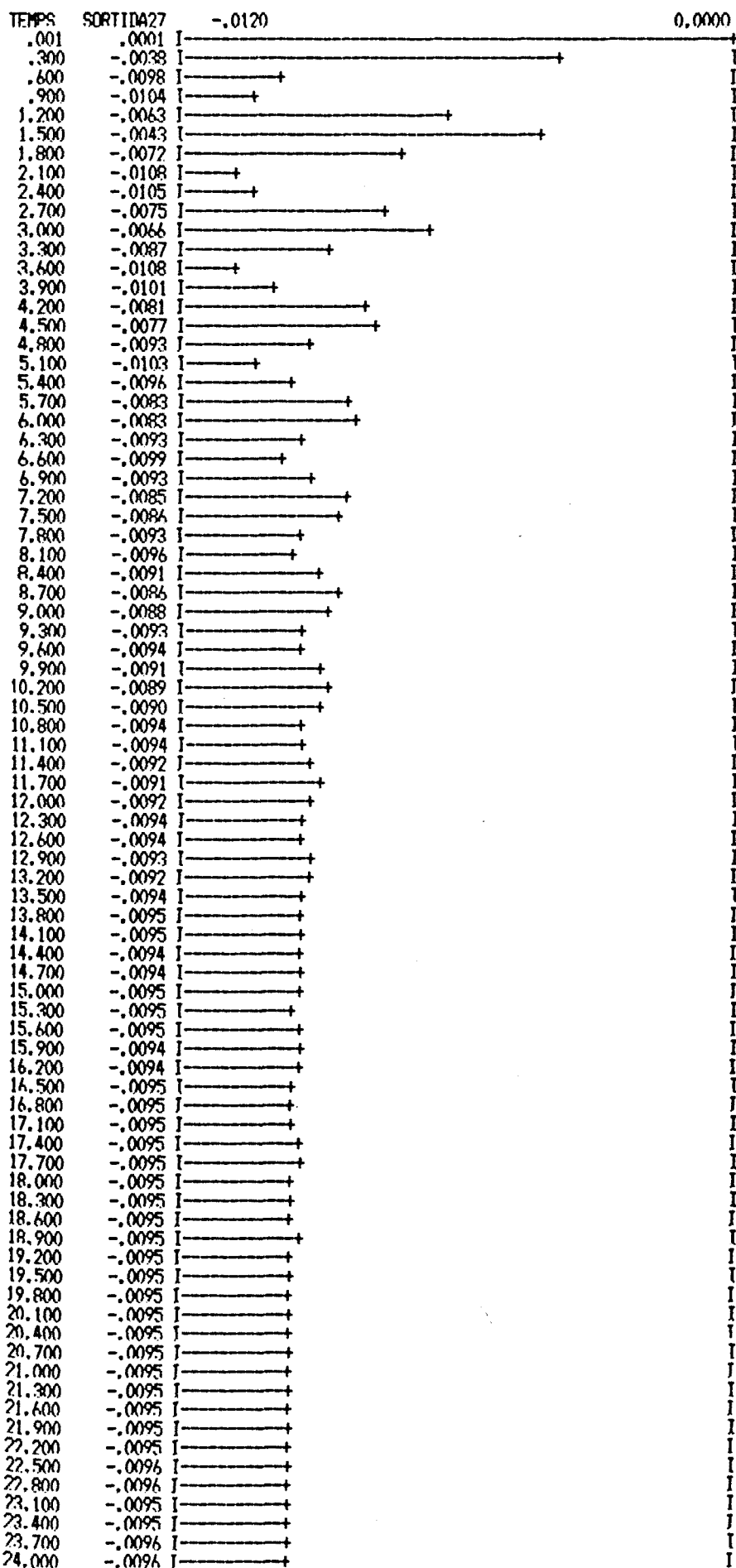
RS - 57

BLOC ETX Y (30) MINIM (-.0450) MAXIM (0.0000)



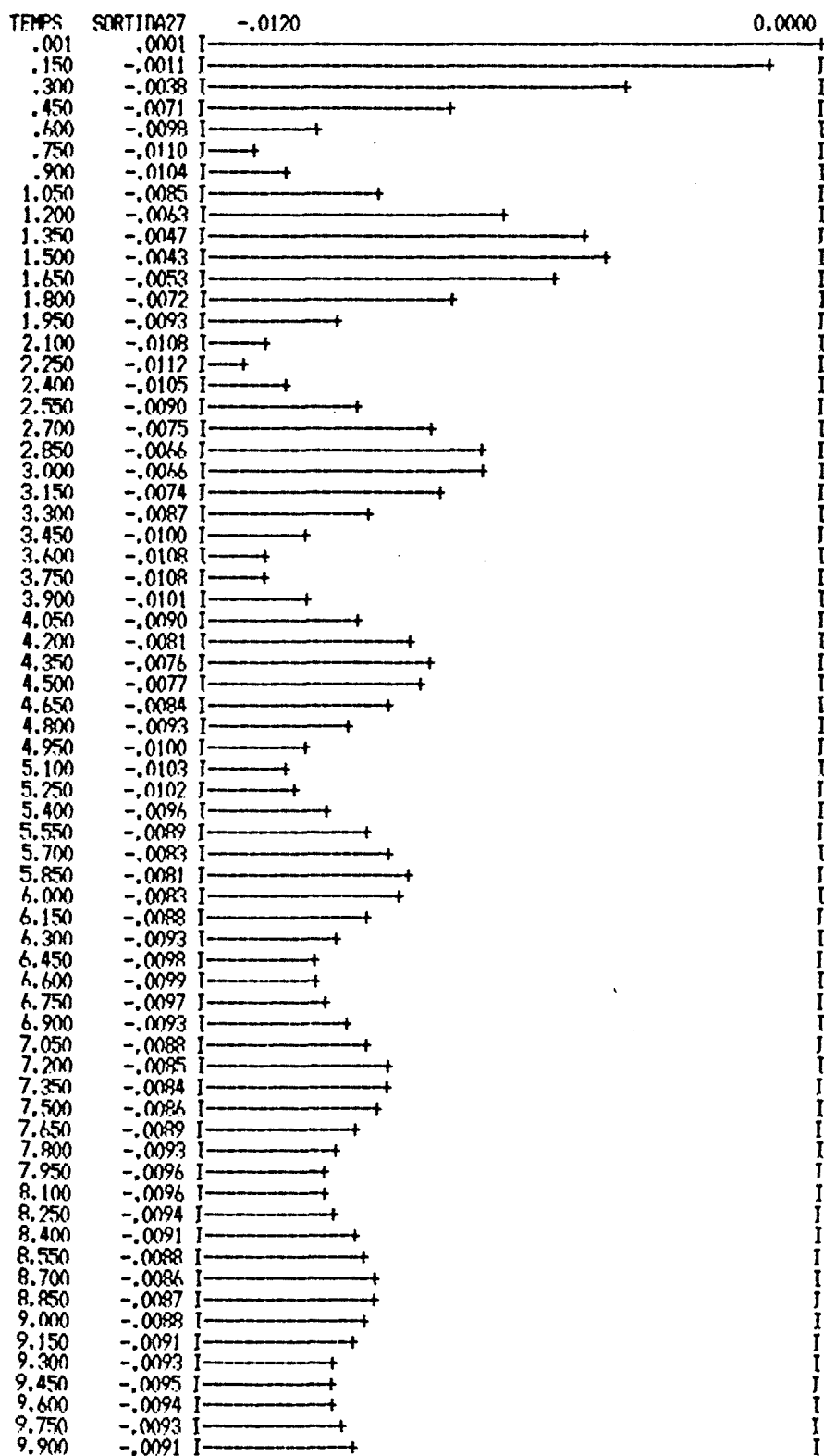
RS - 58

BLOC EIX Y (27) MINIM (-.0120) MAXIM (0.0000)



R S - 59

BLOC FIX Y (27) MINIM (-.0120) MAXIM (0.0000)



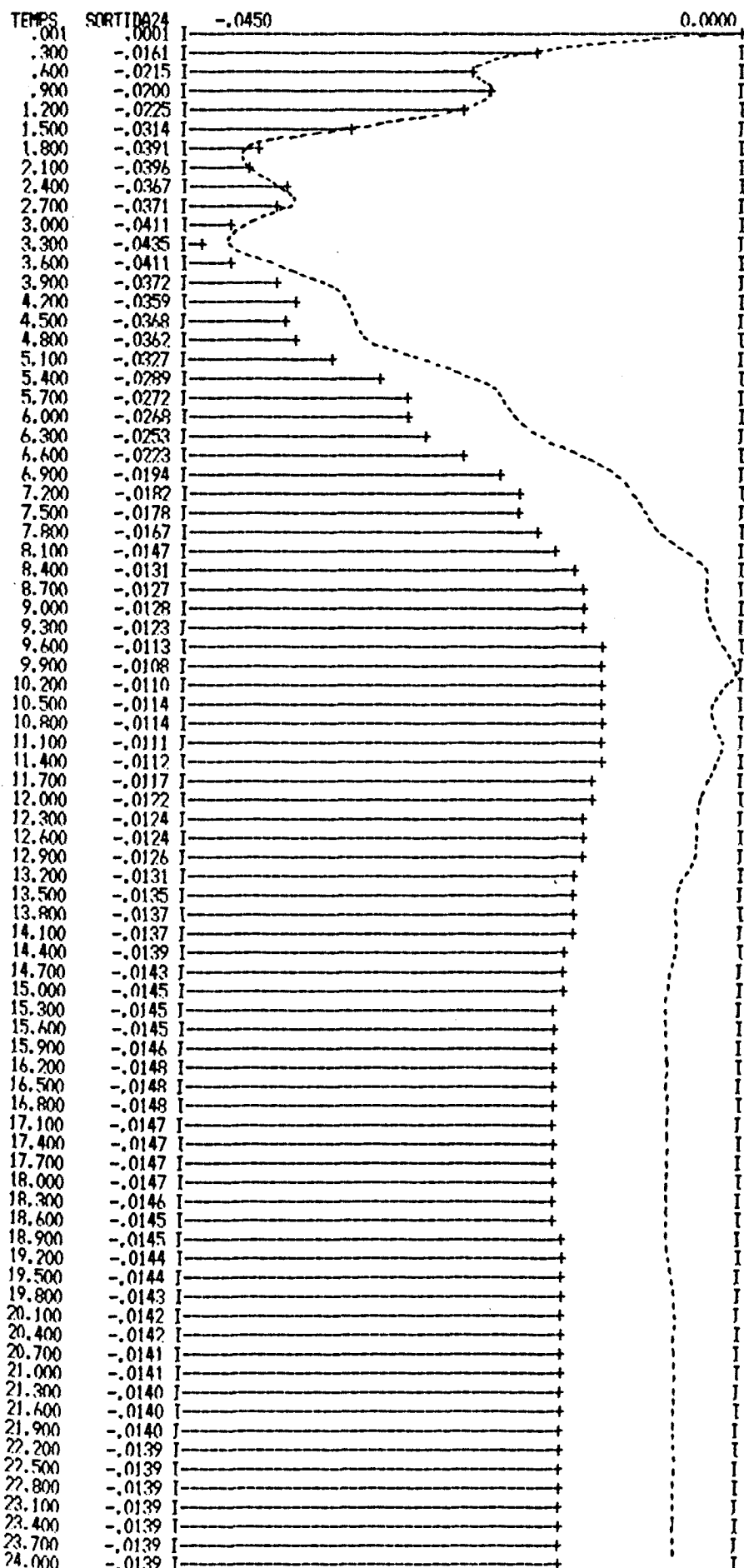
R S - 60

CONDICIONS INICIALS I PARAMETRES

RLOC	CI/PAR 1	PAR 2	PAR 3
4	.0377	0.0000	0.0000
6	.0247	-.0738	0.0000
7	12.9700	0.0000	0.0000
9	5.3518	0.0000	0.0000
10	.0509	0.0000	0.0000
13	2000.0000	0.0000	0.0000
15	.0100	0.0000	0.0000
16	2.0746	0.0000	0.0000
18	.9640	0.0000	0.0000
21	2.0746	0.0000	0.0000
22	-1.0000	1.0000	-1.0000
23	6.2500	0.0000	0.0000
24	0.0000	-.0937	0.0000
26	1.5300	0.0000	0.0000
28	1.0000	1.0000	-1.0000
29	6.2490	0.0000	0.0000
30	0.0000	-1.2343	0.0000
31	.0575	0.0000	0.0000
32	0.0000	-.0295	0.0000
33	2.0000	0.0000	0.0000
35	1.0000	0.0000	0.0000
37	2.0000	0.0000	0.0000
41	.1243	0.0000	0.0000
44	.8500	0.0000	0.0000
47	.1000	0.0000	0.0000
49	.5000	0.0000	0.0000
60	.0142	0.0000	0.0000
66	1.7770	-2.6666	0.0000
71	20000.0000	0.0000	0.0000
75	10.0000	0.0000	0.0000

RS - 62

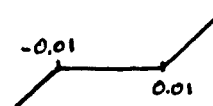
BLOC EIX Y (24) MINIM (-.0450) MAXIM (0.0000)



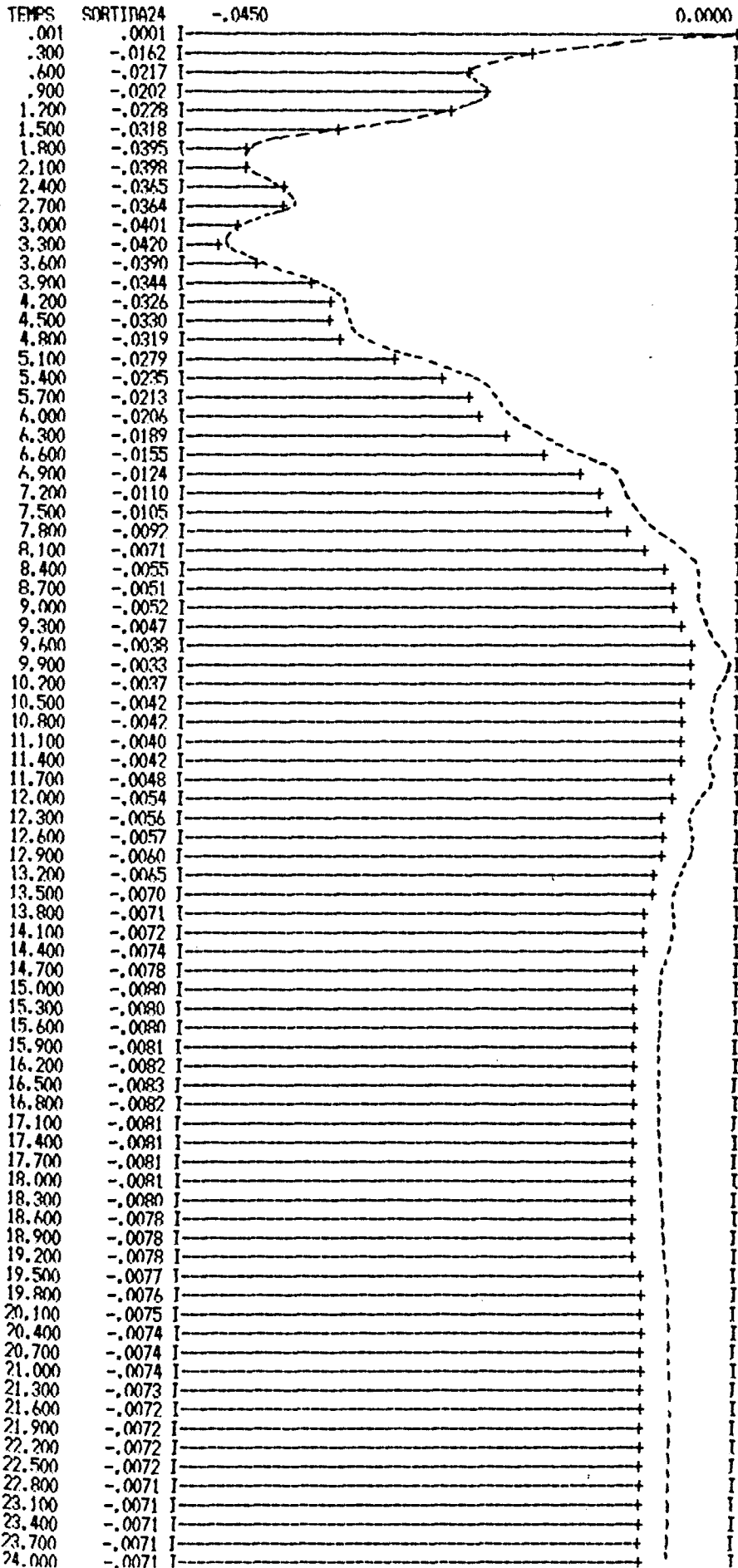
RS - 63

ZONA MUERTA CONVENCIONAL
A ± 0,01 Hz.

----- Simulación sin zona muerta



BLOC EIX Y (24) MNIM (-.0450) MAXIM (0.0000)

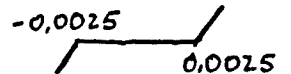


RS - 64

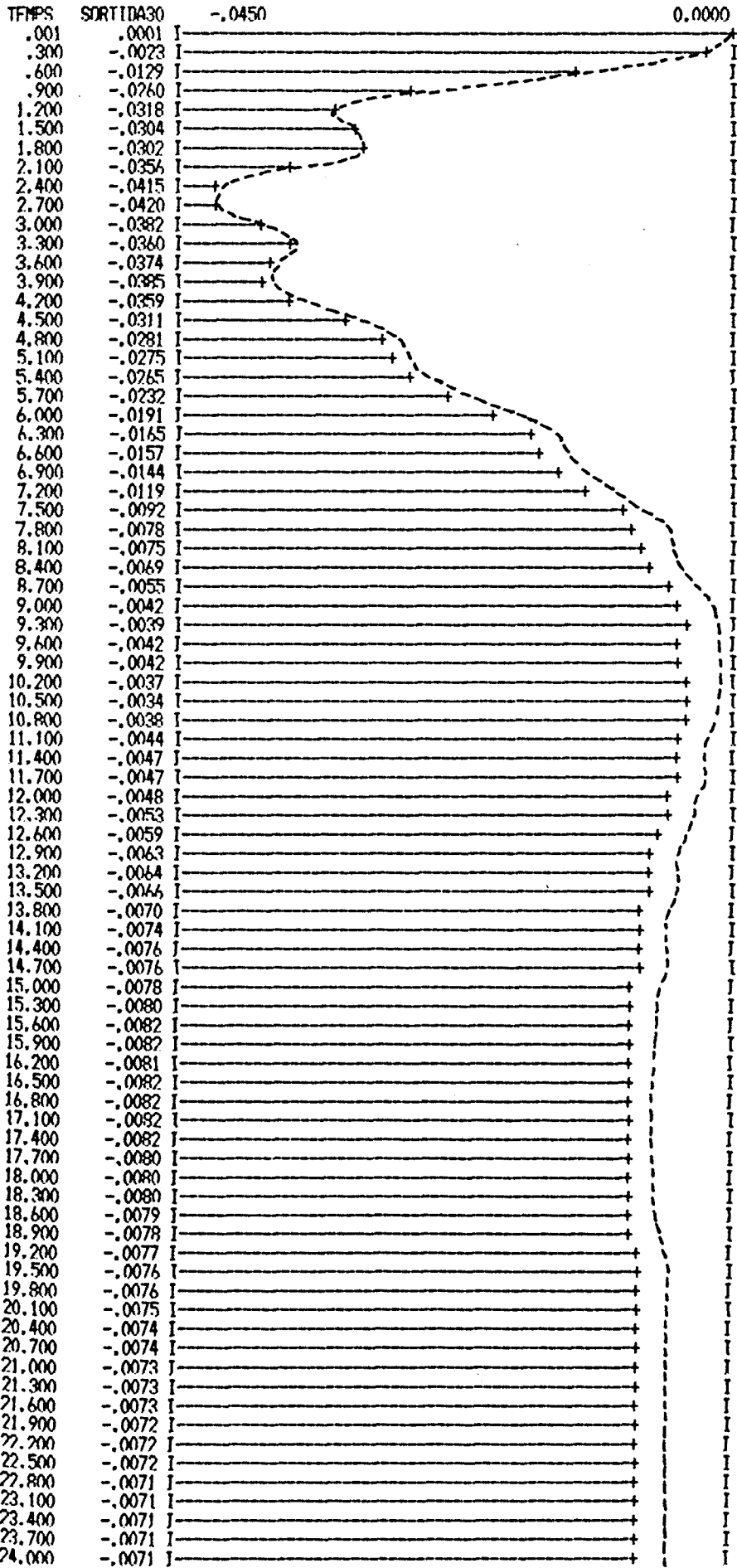
ZONA MUERTA CONVENCIONAL

A ± 0,0025 Hz

----- Simulación sin zona muerta

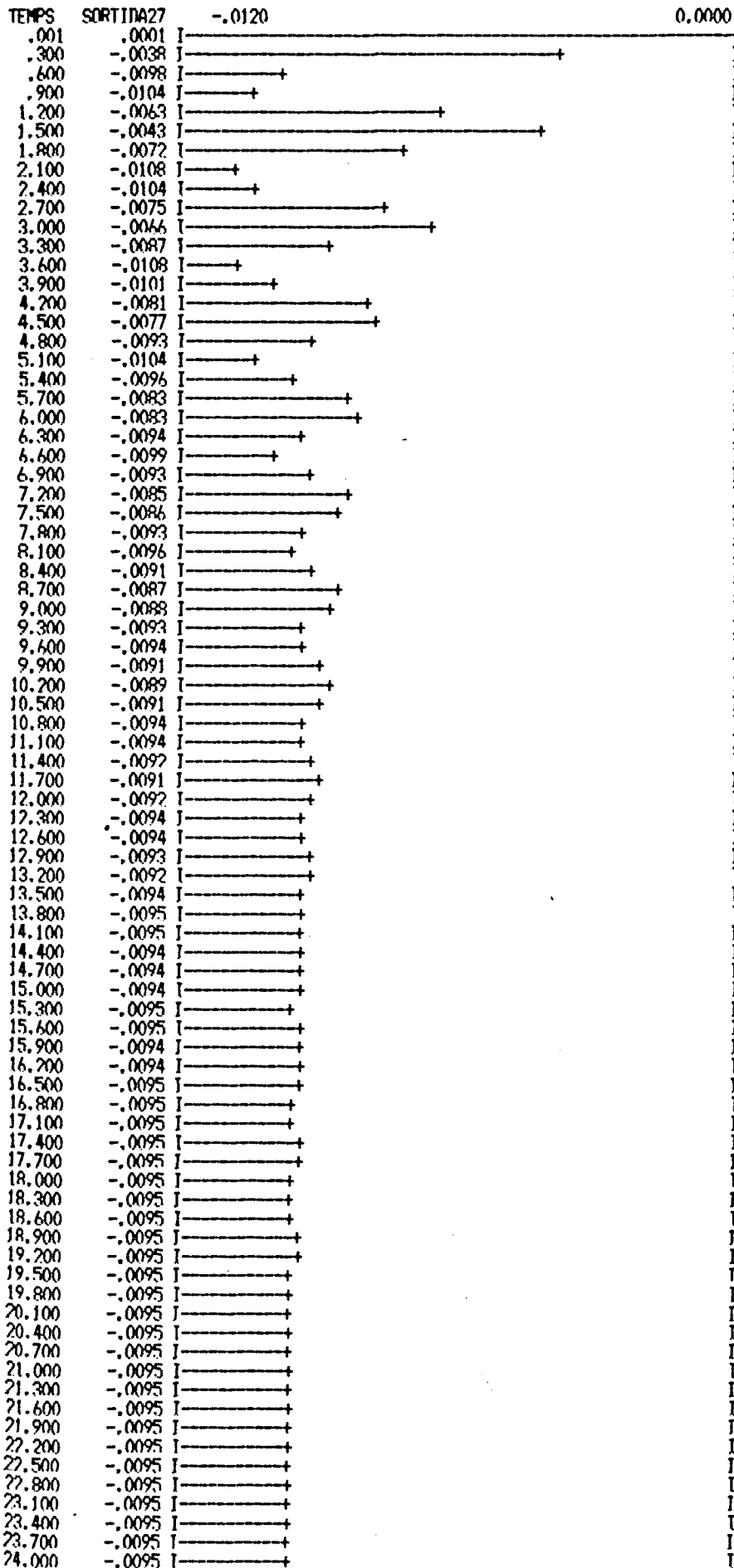


BLOC EIX Y (30) MINIM (-.0450) MAXIM (0.0000)



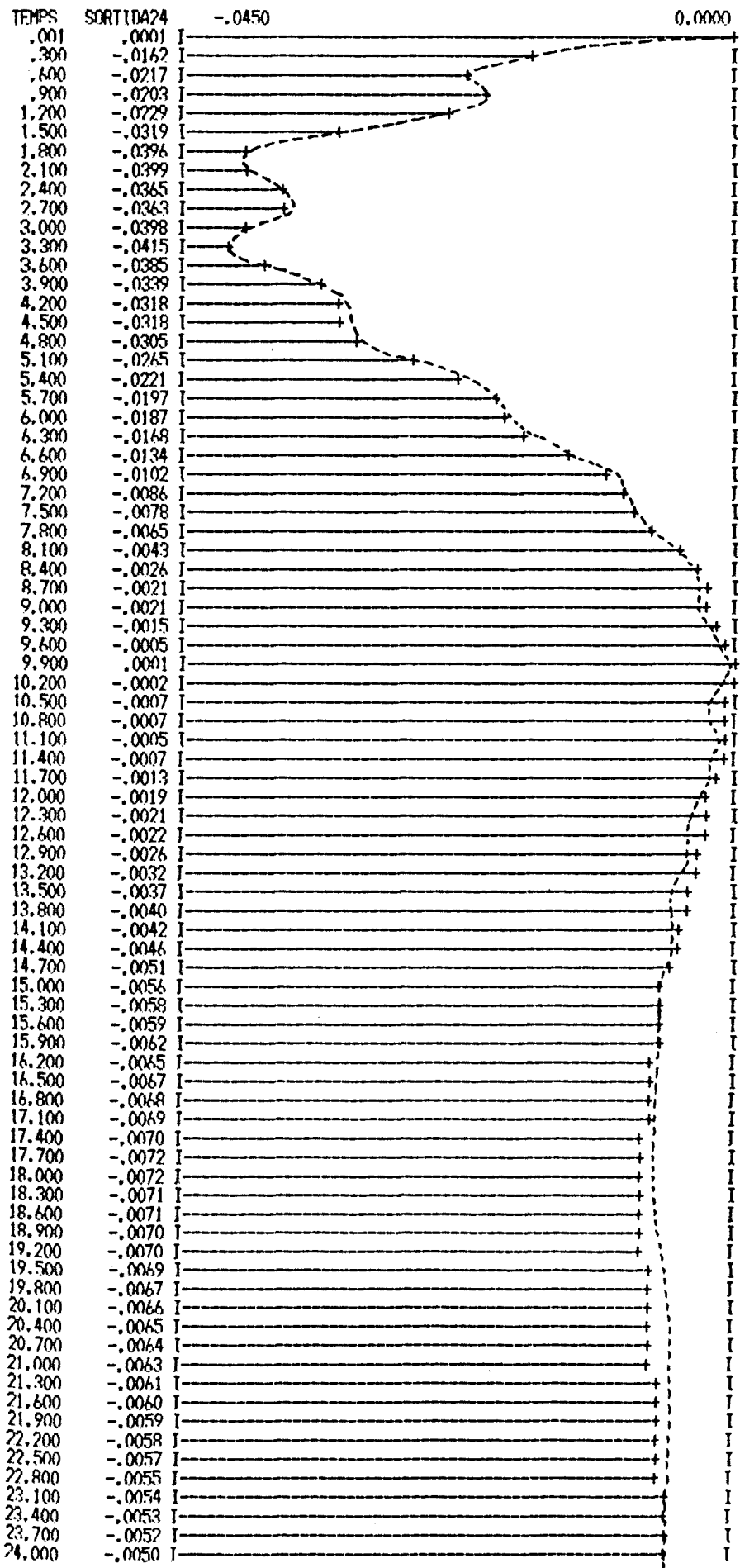
RS - 65

BLOC EIX Y (27) MINIM (-.0120) MAXIM (0.0000)



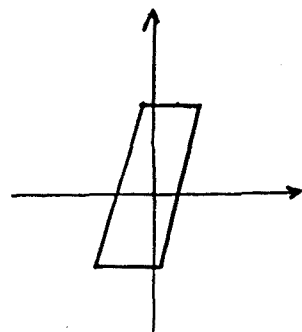
R S - 66

BLOC FIX Y (24) MINIM (-.0450) MAXIM (0.0000)



RS - 67

SIMULACION CON "BACKLASH".



24.000	-.0050	I	-----+	I
24.050	-.0050	I	-----+	I
24.300	-.0049	I	-----+	I
24.600	-.0048	I	-----+	I
24.900	-.0047	I	-----+	I
25.200	-.0046	I	-----+	I
25.500	-.0044	I	-----+	I
25.800	-.0043	I	-----+	I
26.100	-.0042	I	-----+	I
26.400	-.0041	I	-----+	I
26.700	-.0040	I	-----+	I
27.000	-.0039	I	-----+	I
27.300	-.0037	I	-----+	I
27.600	-.0035	I	-----+	I
27.900	-.0033	I	-----+	I
28.200	-.0032	I	-----+	I
28.500	-.0032	I	-----+	I
28.800	-.0032	I	-----+	I
29.100	-.0032	I	-----+	I
29.400	-.0032	I	-----+	I
29.700	-.0033	I	-----+	I
30.000	-.0034	I	-----+	I
30.300	-.0035	I	-----+	I
30.600	-.0035	I	-----+	I
30.900	-.0036	I	-----+	I
31.200	-.0037	I	-----+	I
31.500	-.0038	I	-----+	I
31.800	-.0039	I	-----+	I
32.100	-.0040	I	-----+	I
32.400	-.0041	I	-----+	I
32.700	-.0042	I	-----+	I
33.000	-.0043	I	-----+	I
33.300	-.0044	I	-----+	I
33.600	-.0045	I	-----+	I
33.900	-.0046	I	-----+	I
34.200	-.0047	I	-----+	I
34.500	-.0048	I	-----+	I
34.800	-.0049	I	-----+	I
35.100	-.0049	I	-----+	I
35.400	-.0050	I	-----+	I
35.700	-.0051	I	-----+	I
36.000	-.0052	I	-----+	I
36.300	-.0053	I	-----+	I
36.600	-.0053	I	-----+	I
36.900	-.0054	I	-----+	I
37.200	-.0055	I	-----+	I
37.500	-.0056	I	-----+	I
37.800	-.0056	I	-----+	I
38.100	-.0057	I	-----+	I
38.400	-.0058	I	-----+	I
38.700	-.0058	I	-----+	I
39.000	-.0059	I	-----+	I
39.300	-.0060	I	-----+	I
39.600	-.0061	I	-----+	I
39.900	-.0061	I	-----+	I
40.200	-.0062	I	-----+	I
40.500	-.0063	I	-----+	I
40.800	-.0064	I	-----+	I
41.100	-.0064	I	-----+	I
41.400	-.0065	I	-----+	I
41.700	-.0065	I	-----+	I
42.000	-.0067	I	-----+	I
42.300	-.0067	I	-----+	I
42.600	-.0067	I	-----+	I
42.900	-.0066	I	-----+	I
43.200	-.0066	I	-----+	I
43.500	-.0065	I	-----+	I
43.800	-.0065	I	-----+	I
44.100	-.0063	I	-----+	I
44.400	-.0062	I	-----+	I
44.700	-.0061	I	-----+	I
45.000	-.0060	I	-----+	I
45.300	-.0059	I	-----+	I
45.600	-.0057	I	-----+	I
45.900	-.0056	I	-----+	I
46.200	-.0055	I	-----+	I
46.500	-.0053	I	-----+	I
46.800	-.0052	I	-----+	I
47.100	-.0051	I	-----+	I
47.400	-.0049	I	-----+	I
47.700	-.0048	I	-----+	I
48.000	-.0047	I	-----+	I

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continuación del
listado anterior.

48.000	-.0047	I	-----	+	I
48.050	-.0047	I	-----	+	I
48.300	-.0046	I	-----	+	I
48.600	-.0044	I	-----	+	I
48.900	-.0043	I	-----	+	I
49.200	-.0042	I	-----	+	I
49.500	-.0041	I	-----	+	I
49.800	-.0040	I	-----	+	I
50.100	-.0038	I	-----	+	I
50.400	-.0037	I	-----	+	I
50.700	-.0035	I	-----	+	I
51.000	-.0033	I	-----	+	I
51.300	-.0032	I	-----	+	I
51.600	-.0032	I	-----	+	I
51.900	-.0032	I	-----	+	I
52.200	-.0031	I	-----	+	I
52.500	-.0032	I	-----	+	I
52.800	-.0032	I	-----	+	I
53.100	-.0033	I	-----	+	I
53.400	-.0034	I	-----	+	I
53.700	-.0035	I	-----	+	I
54.000	-.0036	I	-----	+	I
54.300	-.0037	I	-----	+	I
54.600	-.0038	I	-----	+	I
54.900	-.0039	I	-----	+	I
55.200	-.0040	I	-----	+	I
55.500	-.0040	I	-----	+	I
55.800	-.0042	I	-----	+	I
56.100	-.0043	I	-----	+	I
56.400	-.0043	I	-----	+	I
56.700	-.0044	I	-----	+	I
57.000	-.0045	I	-----	+	I
57.300	-.0046	I	-----	+	I
57.600	-.0047	I	-----	+	I
57.900	-.0048	I	-----	+	I
58.200	-.0049	I	-----	+	I
58.500	-.0049	I	-----	+	I
58.800	-.0050	I	-----	+	I
59.100	-.0051	I	-----	+	I
59.400	-.0052	I	-----	+	I
59.700	-.0053	I	-----	+	I
60.000	-.0053	I	-----	+	I
60.300	-.0054	I	-----	+	I
60.600	-.0055	I	-----	+	I
60.900	-.0056	I	-----	+	I
61.200	-.0056	I	-----	+	I
61.500	-.0057	I	-----	+	I
61.800	-.0058	I	-----	+	I
62.100	-.0059	I	-----	+	I
62.400	-.0059	I	-----	+	I
62.700	-.0060	I	-----	+	I
63.000	-.0061	I	-----	+	I
63.300	-.0061	I	-----	+	I
63.600	-.0062	I	-----	+	I
63.900	-.0063	I	-----	+	I
64.200	-.0064	I	-----	+	I
64.500	-.0064	I	-----	+	I
64.800	-.0065	I	-----	+	I
65.100	-.0066	I	-----	+	I
65.400	-.0067	I	-----	+	I
65.700	-.0067	I	-----	+	I
66.000	-.0067	I	-----	+	I
66.300	-.0066	I	-----	+	I
66.600	-.0065	I	-----	+	I
66.900	-.0065	I	-----	+	I
67.200	-.0064	I	-----	+	I
67.500	-.0063	I	-----	+	I
67.800	-.0061	I	-----	+	I
68.100	-.0060	I	-----	+	I
68.400	-.0059	I	-----	+	I
68.700	-.0058	I	-----	+	I
69.000	-.0057	I	-----	+	I
69.300	-.0055	I	-----	+	I
69.600	-.0054	I	-----	+	I
69.900	-.0053	I	-----	+	I
70.200	-.0052	I	-----	+	I
70.500	-.0050	I	-----	+	I
70.800	-.0049	I	-----	+	I
71.100	-.0048	I	-----	+	I
71.400	-.0047	I	-----	+	I
71.700	-.0045	I	-----	+	I
72.000	-.0044	I	-----	+	I

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continuación del listado anterior

$f_0 = 0,043 \text{ Hz.}$

APENDICE D :Determinación del vector de control óptimo: ecuación de Riccati.

El cálculo de la ley de control óptimo \underline{u}° puede enfocarse de diversas formas. En este Apéndice se seleccionará la basada en el Principio del Máximo de Pointryagin, por su interés en el desarrollo de la formulación del Capítulo 6.

Partiendo de la ecuación de estado [52.2], (Apartado 5.2), reescrita aquí como

$$\frac{dx_i}{dt} = f_i(x_1, \dots, x_n, u_1, \dots, u_n), \quad i=1, 2, \dots, n \quad [D.1]$$

y del criterio integral [52.1], escrito ahora de la forma general,

$$J = \int_0^{\infty} f_0(\underline{x}, \underline{u}) dt, \quad \underline{x}_0 \in \underline{x} \quad [D.2]$$

definimos una ecuación de estado ampliada con los términos f_0 y \underline{x}_0 del criterio integral,

$$\frac{d\underline{X}}{dt} = \underline{F}(\underline{x}, \underline{u}), \quad \underline{F} = (f_0, \dots, f_n) \quad [D.3]$$

Introduciendo un vector adjunto (ó covariante) $\underline{\psi}$, que cumpla la siguiente ecuación lineal y homogénea,

$$\frac{d\underline{\psi}}{dt} = - \begin{bmatrix} \frac{\partial f_0}{\partial x_0} & \dots & \frac{\partial f_n}{\partial x_0} \\ \vdots & & \vdots \\ \frac{\partial f_0}{\partial x_n} & \dots & \frac{\partial f_n}{\partial x_n} \end{bmatrix} \underline{\psi} \quad [D.4]$$

podemos definir al Hamiltoniano,

$$H = \underline{\psi}^T \underline{F} = \underline{\psi}^T \frac{d\underline{X}}{dt} = \sum_{i=0}^n \psi_i f_i(\underline{x}, \underline{u}) \quad [D.5]$$

$$(\underline{\psi} = (\psi_0, \dots, \psi_n))$$

Según el Principio del Máximo de Pointryagin, para que una determinada ley de control $\underline{u}^\circ(t)$ desplace al sistema desde un estado inicial $\underline{x}(0)$ a un estado final $\underline{x}(t_1)$ según una trayectoria óptima en el sentido de [D.2], $\underline{x}^\circ(t)$, es necesaria la existencia de un vector continuo $\underline{\psi}^\circ(t)$, correspondiente a $\underline{x}^\circ(t)$ y a $\underline{u}^\circ(t)$, para el cual:

1/ La función H alcanza un máximo en $\underline{u}=\underline{u}^\circ$,

$$H(\underline{\psi}^\circ(t), \underline{x}^\circ(t), \underline{u}^\circ(t)) = M(\underline{\psi}^\circ(t), \underline{x}^\circ(t)) \quad [D.6]$$

2/ El máximo de M es cero si el valor de Ψ_0 no es positivo,

$$M(\underline{\psi}^\circ(t), \underline{x}^\circ(t)) = 0, \quad 0 \leq t \leq t_1 \quad [D.7]$$

Dado el carácter homogéneo de la ecuación 52.9, se escoge el valor

$$\Psi_0 = -1 \quad [D.8]$$

Según la condición [D.8] el Hamiltoniano de la expresión [D.5] se convierte en:

$$H = -f_0(\underline{x}, \underline{u}) + \sum_{i=1}^n \Psi_i f_i(\underline{x}, \underline{u}) \quad [D.9]$$

y, comparando a [52.1] (Apartado 5.2) con [D.2] y a [52.2] con [D.1],

$$H = -\underline{x}^T \underline{Q} \underline{x} - \underline{u}^T \underline{R} \underline{u} + \underline{\psi}_a^T (\underline{A} \underline{x} + \underline{B} \underline{u}) \quad [D.10]$$

siendo $\underline{\psi}_a$ un vector de dimensión n formado por los elementos (Ψ_1, \dots, Ψ_n)

La condición del máximo obliga a que:

$$\left. \frac{\partial H}{\partial \underline{u}} \right|_{\underline{u}=\underline{u}^\circ} = 0 \quad \Rightarrow \quad \underline{R}^T \underline{u} + \underline{R} \underline{u} + \underline{\psi}_a^T \underline{B} = 0 \quad [D.11]$$

y, siendo \underline{R} una matriz simétrica,

$$2 \underline{R} \underline{u} + \underline{\psi}_a^T \underline{B} = 0 \quad \Rightarrow \quad \underline{u}^\circ = -\frac{1}{2} \underline{R}^{-1} \underline{B}^T \underline{\psi}_a^T \quad [D.12]$$

expresión que determina la ley de control óptimo.

Por otro lado, de [D.4] y [D.5], se obtiene,

$$\frac{d\underline{\psi}}{dt} = -\frac{\partial H}{\partial \underline{x}} \quad [D.13]$$

expresión que, particularizada para [D.10], queda:

$$\frac{d \underline{\psi}_a}{dt} = \underline{Q}^T \underline{x} + \underline{Q} \underline{x} - \underline{A}^T \underline{\psi}_a \quad [D.14]$$

y, siendo \underline{Q} otra matriz simétrica,

$$2 \underline{Q} \underline{x} - \underline{A}^T \underline{\psi}_a = \frac{d \underline{\psi}_a}{dt} \quad [D.15]$$

Usando la siguiente transformación, denominada Transformación de Riccati,

$$\frac{1}{2} \underline{\psi}_a = \underline{P} \underline{x} \quad [D.16]$$

la expresión [D.15] pasa a ser:

$$\underline{Q} \underline{x} + \underline{A}^T \underline{P} \underline{x} = - \frac{d \underline{P}}{dt} \underline{x} - \underline{P} \frac{d \underline{x}}{dt} \quad [D.17]$$

y, en vista de [52.2] del Apartado 5.2,

$$- \frac{d \underline{P}}{dt} \underline{x} = \underline{Q} \underline{x} + \underline{A}^T \underline{P} \underline{x} + \underline{P} \underline{A} \underline{x} + \underline{P} \underline{B} \underline{u} \quad [D.18]$$

expresión que, junto con [D.12], lleva a la ecuación algebraica de Riccati:

$$\frac{d \underline{P}}{dt} = - \underline{Q} - \underline{A}^T \underline{P} - \underline{P} \underline{A} + \underline{P} \underline{B} \underline{R}^{-1} \underline{B}^T \underline{P} \quad [D.19]$$

La solución de esta ecuación no es un problema trivial, existiendo diversos algoritmos para la determinación de \underline{P} [120]. Dada la necesidad de un ordenador para ejecutar estos algoritmos, pueden presentarse problemas de convergencia en los resultados debidos a los truncamientos y redondeos, lo que obliga a depurar los programas.

Los algoritmos basados en métodos recursivos suelen partir de una discretización del término $\frac{d \underline{P}}{dt}$ de la ecuación de Riccati,

$$\frac{d \underline{P}}{dt} \approx \frac{\underline{P}(k+1) - \underline{P}(k)}{T} \quad [D.20]$$

con lo que la ecuación [D.19] se convierte en

$$\underline{P}(k+1) = \underline{P}(k) + T (- \underline{Q} - \underline{A}^T \underline{P}(k) - \underline{P}(k) \underline{B} \underline{R}^{-1} \underline{B}^T \underline{P}(k) - \underline{P}(k) \underline{A}) \quad [D.21]$$

expresión que permite una fácil programación (determinación de $\tilde{P}(k+1)$ a partir del valor de $\tilde{P}(k)$ en la iteración anterior), la cual termina cuando

$$|\tilde{P}(k+1) - \tilde{P}(k)| < \varepsilon \quad [\text{D.22}]$$

(ε = precisión deseada; idealmente $\varepsilon = 0$)

es decir, cuando se anule la derivada $\frac{d\tilde{P}}{dt}$,

$$0 = \tilde{Q} + \tilde{A}^T \tilde{P} + \tilde{P} \tilde{A} - \tilde{P} \tilde{B} \tilde{R}^{-1} \tilde{B}^T \tilde{P} \quad [\text{D.23}]$$

Obviamente, cuanto menor sea el periodo de muestreo T , menor será la distorsión derivada de pasar del dominio continuo al discreto. Pero, dado que en cada iteración se avanzan T seg del transitorio de $\tilde{P}(t)$, un valor pequeño de T dilata el tiempo de cálculo necesario para obtener la solución (valor de $\tilde{P}(t)$ en régimen permanente). Por ello, en la práctica, estos algoritmos recursivos de resolución de la ecuación de Riccati precisan de un primer tanteo en el ordenador para estimar un valor de T que conjugue satisfactoriamente los requisitos de precisión en los resultados y de rapidez en la ejecución de los programas.

Los métodos no recursivos, como es el del "autovalor-autovector", requieren una mayor complejidad en los algoritmos (por ejemplo el método citado encuentra la matriz \tilde{P} de Riccati determinando previamente los autovalores de unas matrices auxiliares [120]), pero, en contrapartida, reducen el periodo de cálculo (según resultados experimentales propios el método del "autovalor-autovector" es unas 10 veces más rápido que el método recursivo de la ref. [126]).